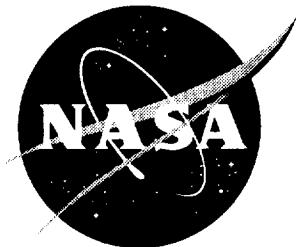


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Catalogue of X-Ray Texture Data for Al-Cu-Li Alloy 1460, 2090, 2096 and 2195 Near-Net-Shape Extrusions, Sheet and Plate

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Catalogue of X-Ray Texture Data for Al-Cu-Li Alloy 1460, 2090, 2096 and 2195 Near-Net-Shape Extrusions, Sheet and Plate

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Abstract

The effect of crystallographic texture on the mechanical properties of near-net-shape extrusions is of major interest if these products are to find application in launch vehicle or aircraft structures. The objective of this research was to produce a catalogue containing quantitative texture information for extruded product, sheet and plate. The material characterized was extracted from wide, integrally stiffened panels fabricated from the Al-Cu-Li alloys 1460, 2090, 2096 and 2195. The textural characteristics of sheet and plate products of the same alloys were determined for comparison purposes. The approach involved using x-ray diffraction to generate pole figures in combination with crystallite orientation distribution function analysis. The data were compiled as a function of location in the extruded and wrought product cross-sections and the variation in the major deformation- and recrystallization-related texture components was identified.

* This research was conducted in the Materials Division at NASA Langley Research Center under Contract # NAS1-19708 with Mr. Keith Bird as technical monitor.

Symbols and Abbreviations

OD :	Outside diameter
ID :	Inside diameter
R :	Specimen plane perpendicular to the original radial axis of the stovepipe extrusion
C :	Specimen plane perpendicular to the original circumferential axis of the stovepipe extrusion
ED :	Extrusion direction
RD :	Rolling direction in sheet and plate
S :	Specimen plane perpendicular to the short-transverse axis of sheet and plate
TD :	Transverse direction
t :	Thickness (e.g. t/2 corresponds to mid-plane of cross-section)
CODF :	Crystallite orientation distribution function
ϕ_1, ϕ, ϕ_2 :	Euler angles using Bunge notation

1. Introduction

A variety of Al-Cu-Li alloy products are candidates for future launch vehicle and aircraft structures. The improved specific properties of these alloys compared to conventional Al alloys can be translated into structural weight savings and reduced operational costs. Because Al-Cu-Li alloys are more expensive than conventional alloys, fabrication methods which reduce manufacturing costs are also being considered. The current Space Shuttle External Tank is fabricated from integrally machined plate and the use of near-net-shape extrusions creates the potential to reduce material expenses by lowering the scrap rate. When considering different product forms for service, the relationship between crystallographic texture and mechanical properties is an important issue. Although this relationship is not addressed here, there is a need to develop a database of texture information on extruded product. The objective of this research was to document the variation in texture of near-net-shape extrusions as a function of location through the cross-section.

In parallel, data outlining the textural characteristics of sheet and plate were compiled for comparison.

2. Materials

The compositions of the Al-Cu-Li alloys studied in this investigation are listed in Table 1. The sequence of events leading to production of the near-net-shape extrusions is as follows. The alloys were cast into rectangular ingots which were then machined to circular cross-section and forged into hollow cylindrical billets with dimensions 16.5in OD, 12in ID and 25in long. Subsequently, "stove pipe" extrusions 157in long were produced using an extrusion temperature of 680-825°F at a rate of 16-24in/min. The extruded cross-section comprised a 15 in diameter cylinder, 0.18in thick, with 8 equi-spaced integral "J" stiffeners on the outer surface. These cylinders were then split lengthwise and processed into flat panels 32in wide and 118in long using a combination of mechanical unfolding and rolling. Finally, the extrusions were cold stretched to the T3 temper condition. The dimensions of a typical section of the extruded product are shown in Figure 1(a). The sheet and plate product obtained for comparison were rolled by conventional means to the various gages specified and examined in either a T3 or T8 temper.

3. Procedures

The locations for extraction of specimens from the extruded cross-sections suitable for x-ray diffraction analysis are outlined in Figure 1(b). The nomenclature used to describe the principal regions in the cross-section comprise the skin, base, web and cap of the integrally "J" stiffened extrusion. Square coupons, 0.75in x 0.75in, were extracted and metallographically prepared to the appropriate depth location for analysis. In order to confine analysis in the base to the region of interest, multiple sections were extracted and laminated together to produce the desired coupon dimensions. Initial specimen preparation involved rough mechanical polishing down to the desired depth followed by final polishing through 0.05µm colloidal silica, macroetching with a 10% caustic solution for 15 secs at 150°F and de-smutting with concentrated nitric acid.

The x-ray diffraction data were collected using the Schultz backward reflection technique with the specimen mounted in a computer-driven Eulerian cradle and a sample oscillation of 10mm. The data were collected in accordance with the matrix outlined in Table 2 using x-ray diffraction equipment with software suitable for quantitative texture analysis. The data were collected using Cu K α radiation with tube settings of 40kV/30mA and a slit width of 1.8mm. The raw data were corrected with respect to background intensity and defocussing errors using data collected from a randomly-textured, pure Al powder specimen using the same equipment settings. The data were reduced to {111}, {200} and {220} partial pole figures, CODF's calculated and represented graphically in Euler space using the Bunge notation.

4. Results

Quantitative texture data for the alloys and product forms described above are shown in Figures 2-41 for 1460, Figures 42-81 for 2090, Figures 82-114 for 2096 and Figures 115-147 for 2195. The information presented comprises pole figures, CODF data and plots showing the variation in the intensities of the prominent deformation- and recrystallization-related texture components as a function of depth through the product cross-section. This latter analysis, which is only valid when the extrusion/rolling direction is contained within the specimen plane, was only performed on data collected with the specimen plane normal to the radial axis of the extrusion and the plate and sheet.

Alloy	Composition, wt %							
	Element	Cu	Li	Mg	Ag	Zr	Sc	Al
1460	Range	2.6/3.3	2.0/2.5	< 0.05	--	0.06/0.15	0.04/0.14	Bal.
	Nominal	2.9	2.1	--	--	0.11	0.04	Bal.
2090	Range	2.4/3.0	1.9/2.6	< 0.25	--	0.08/0.15	--	Bal.
	Nominal	2.7	2.0	--	--	0.12	--	Bal.
2096	Range	2.3/3.0	1.3/1.9	0.25/0.8	0.25/0.6	0.04/0.18	--	Bal.
	Nominal	2.8	1.4	0.5	0.3	0.13	--	Bal.
2195	Range	3.7/4.3	0.8/1.2	0.25/0.8	0.25/0.6	0.08/0.16	--	Bal.
	Nominal	4.3	1.0	0.4	0.5	0.12	--	Bal.

Table 1. Nominal and specified range of compositions for 1460, 2090, 2096 and 2195 near-net-shape extrusions, sheet and plate.

Alloy	Product	Location	1/8	1/4	3/8	1/2	5/8	3/4	7/8	Plane*
1460-T3	Extrusion	Skin		•		•		•		R
		Base				..				R/C
		Web	•		•		•		•	C
		Cap		•		•		•		R
1460-T3	0.060" Sheet		•	•		•				S
1460-T3	0.285" Plate		•	•		•				S
2090-T8	Extrusion	Skin		•		•		•		R
		Base				..				R/C
		Web	•		•		•		•	C
		Cap		•		•		•		R
2090-T8	0.120" Sheet		•	•		•				S
2090-T8	0.750" Plate		•	•		•				S
2096-T3	Extrusion	Skin		•		•		•		R
		Base				..				R/C
		Web	•		•		•		•	C
		Cap		•		•		•		R
2096-T8	0.090" Sheet		•	•		•				S
2195-T3	Extrusion	Skin		•		•		•		R
		Base				..				R/C
		Web	•		•		•		•	C
		Cap		•		•		•		R
2195-T8	0.250" Plate		•	•		•				S

Table 2. Matrix for collection of x-ray diffraction data as a function of alloy, product form and through-thickness location. * = Orientation of specimen plane: R - perpendicular to radial axis; C - perpendicular to circumferential axis of near-net-shape extrusion and S - perpendicular to short-transverse axis of rolled product.

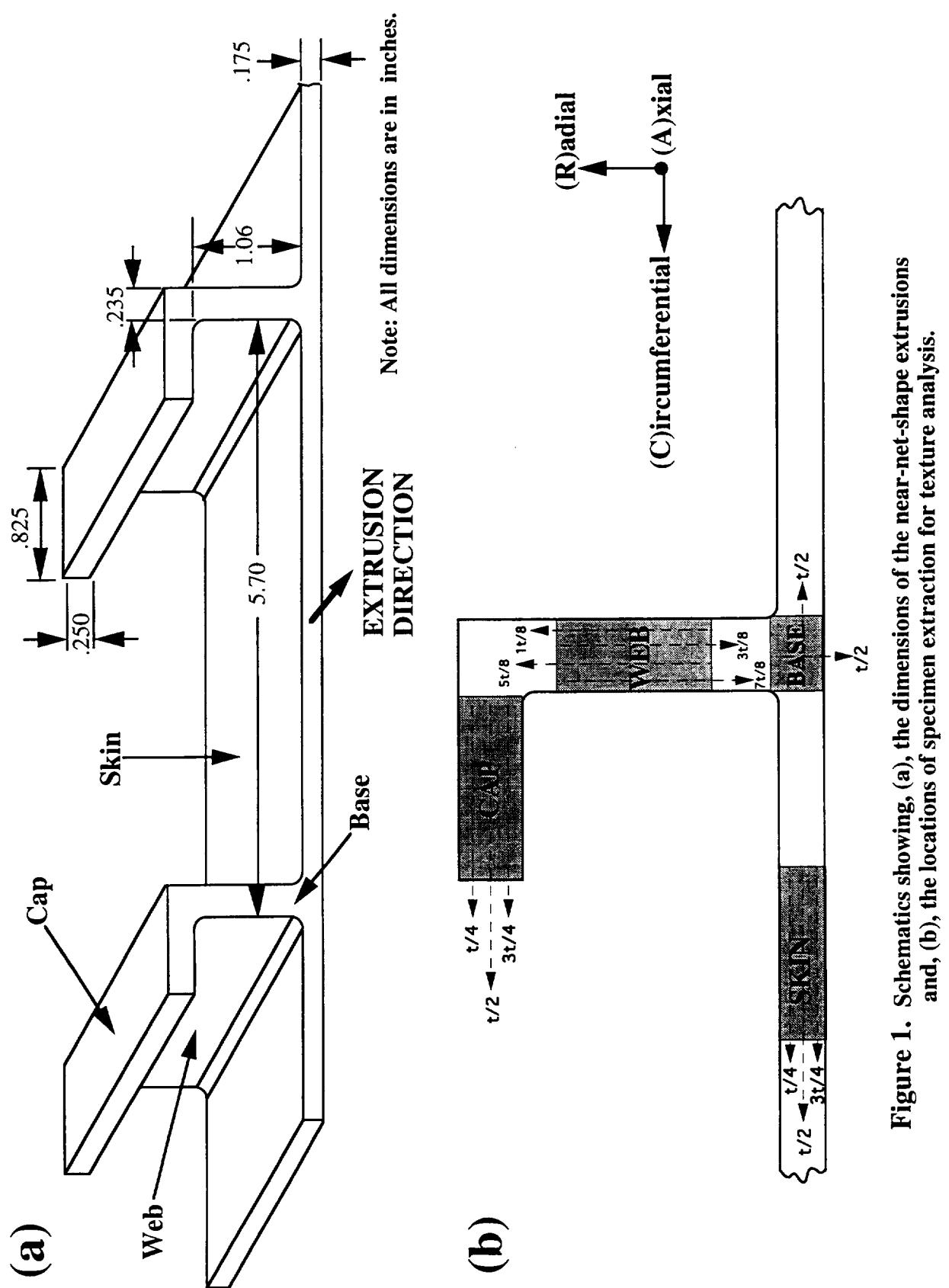


Figure 1. Schematics showing, (a), the dimensions of the near-net-shape extrusions and, (b), the locations of specimen extraction for texture analysis.

4.1 Alloy 1460

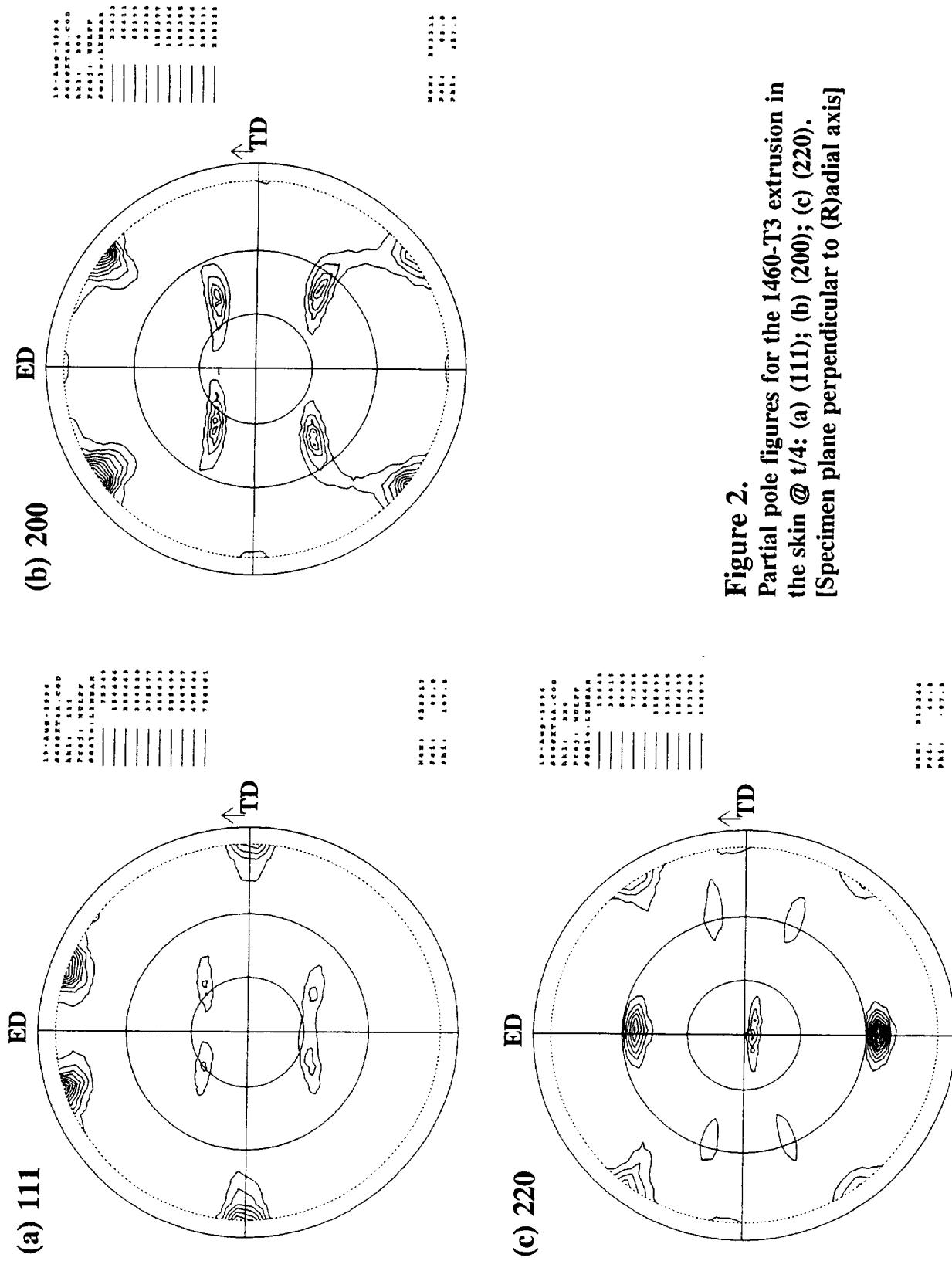
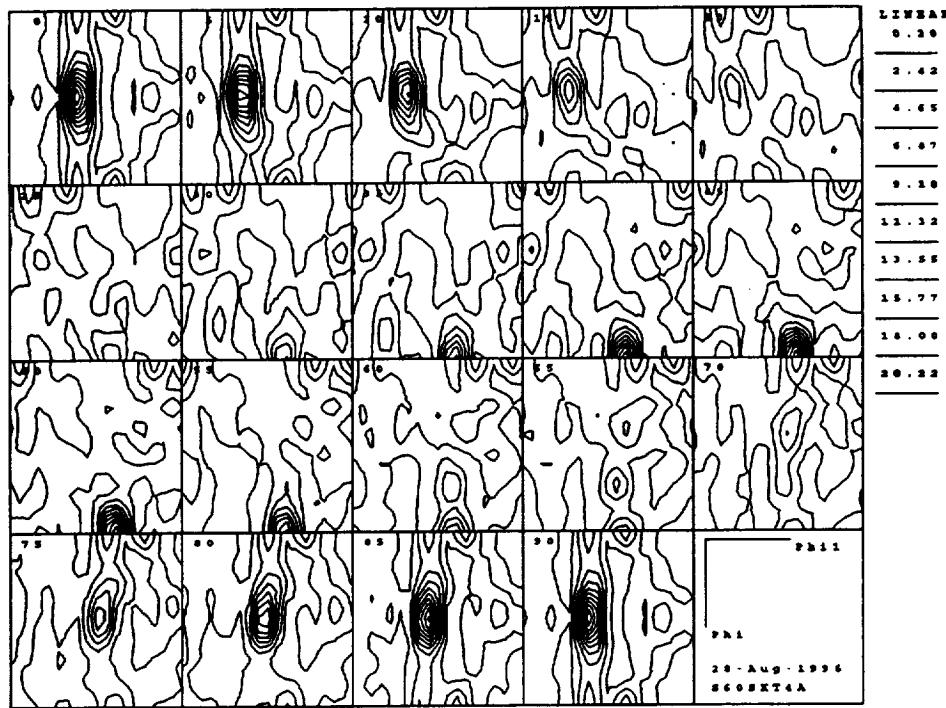


Figure 2.
Partial pole figures for the 1460-T3 extrusion in
the skin @ t/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

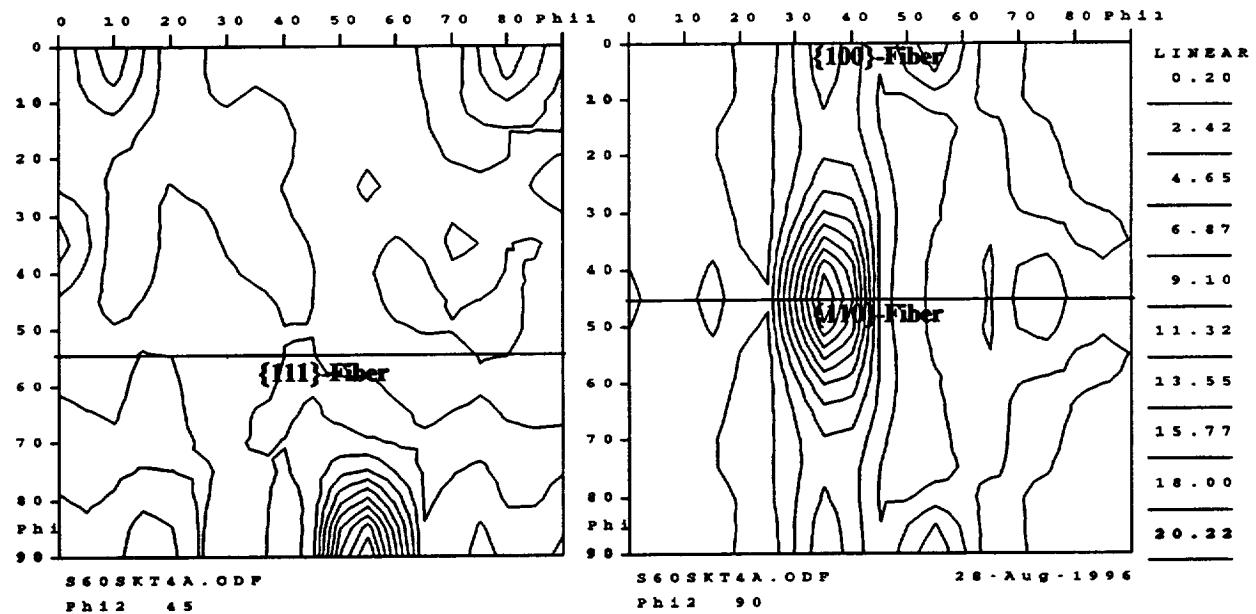


Figure 3. CODF sections for the 1460-T3 extrusion in the skin @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

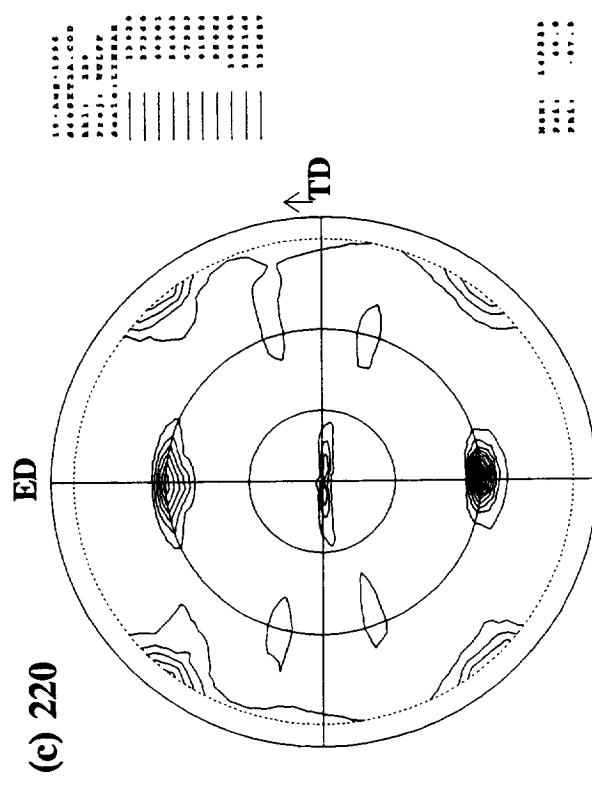
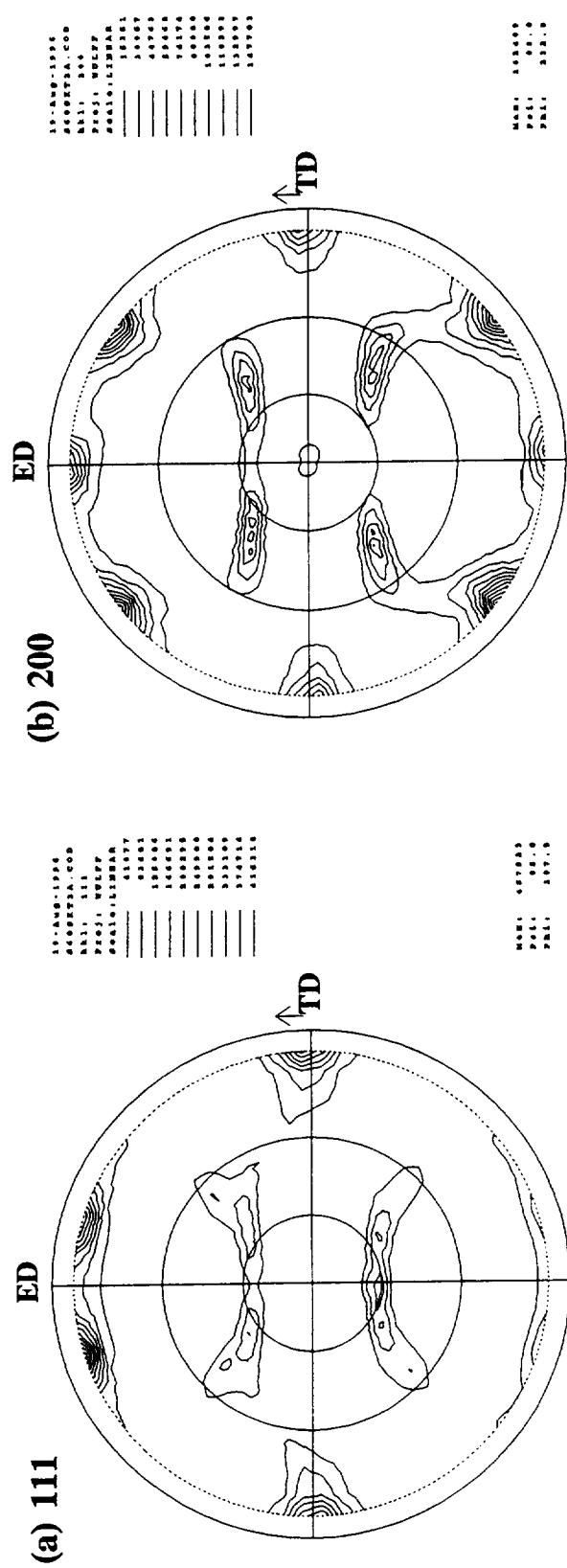
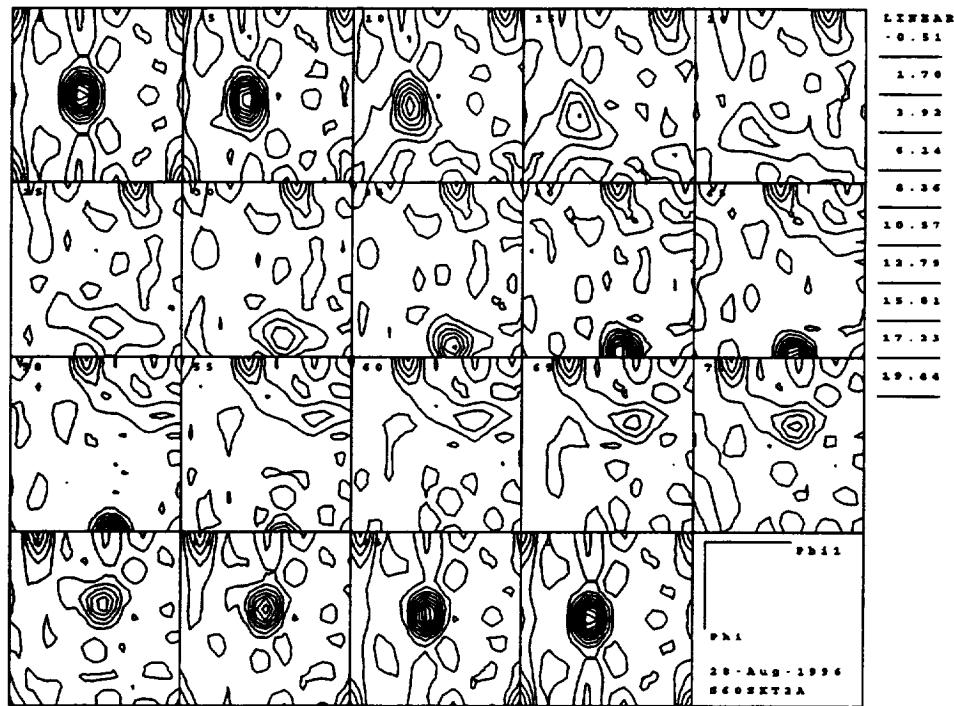


Figure 4.
Partial pole figures for the 1460-T3 extrusion in
the skin @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

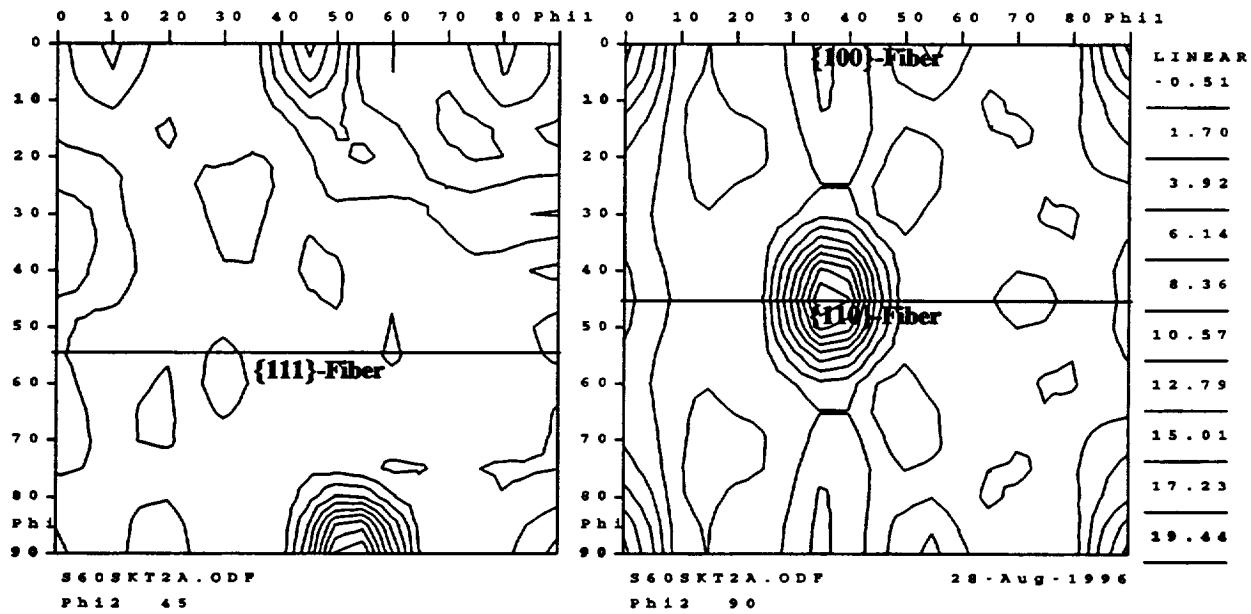


Figure 5. CODF sections for the 1460-T3 extrusion in the skin @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

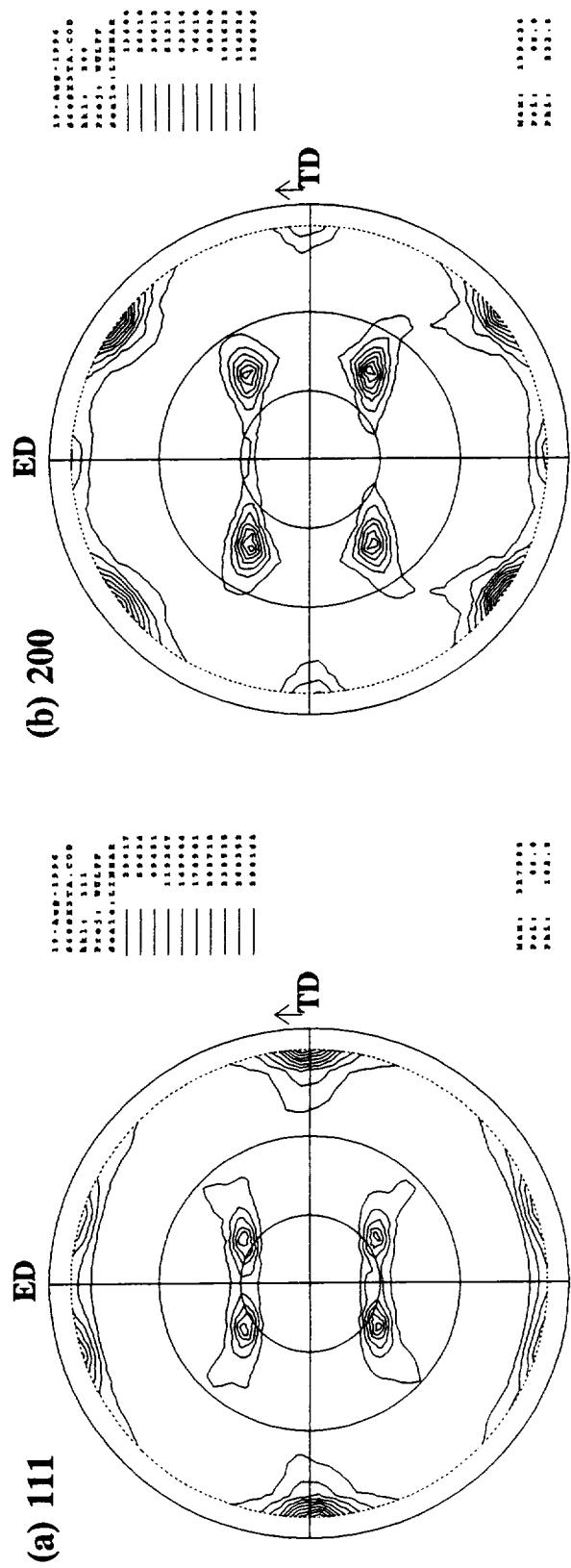
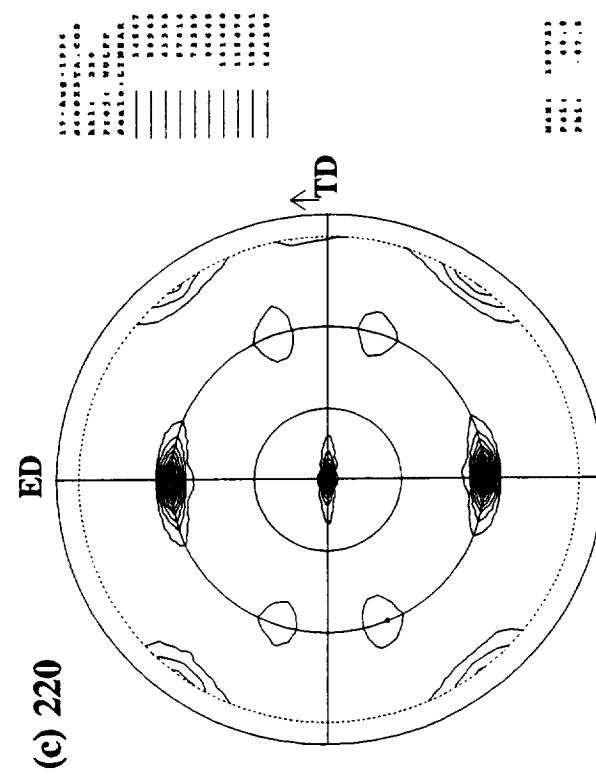
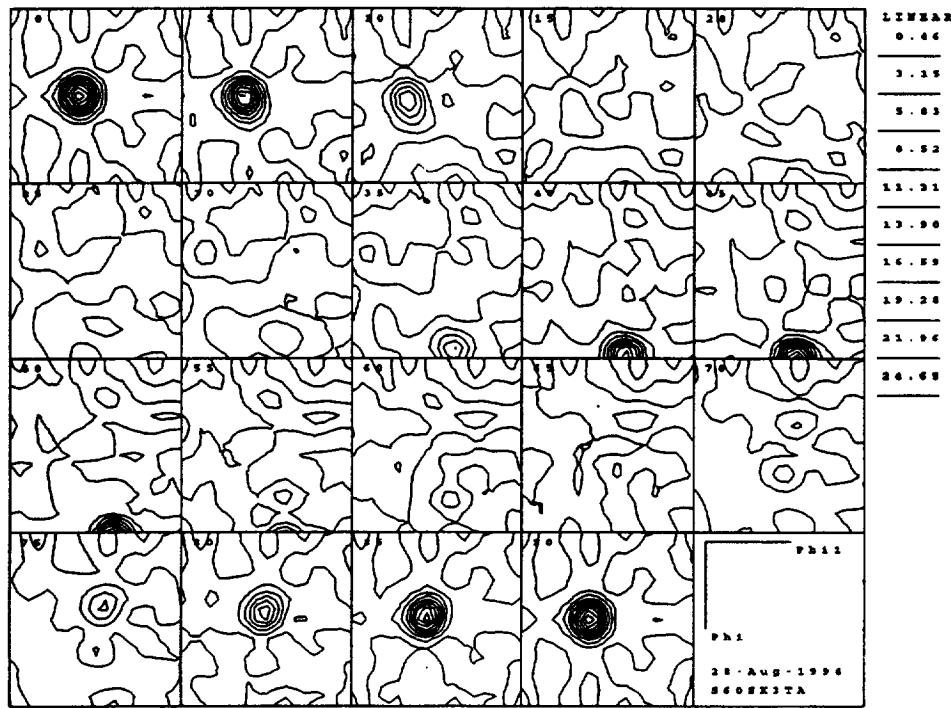


Figure 6.
Partial pole figures for the 1460-T3 extrusion in
the skin @ 3t/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]



(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

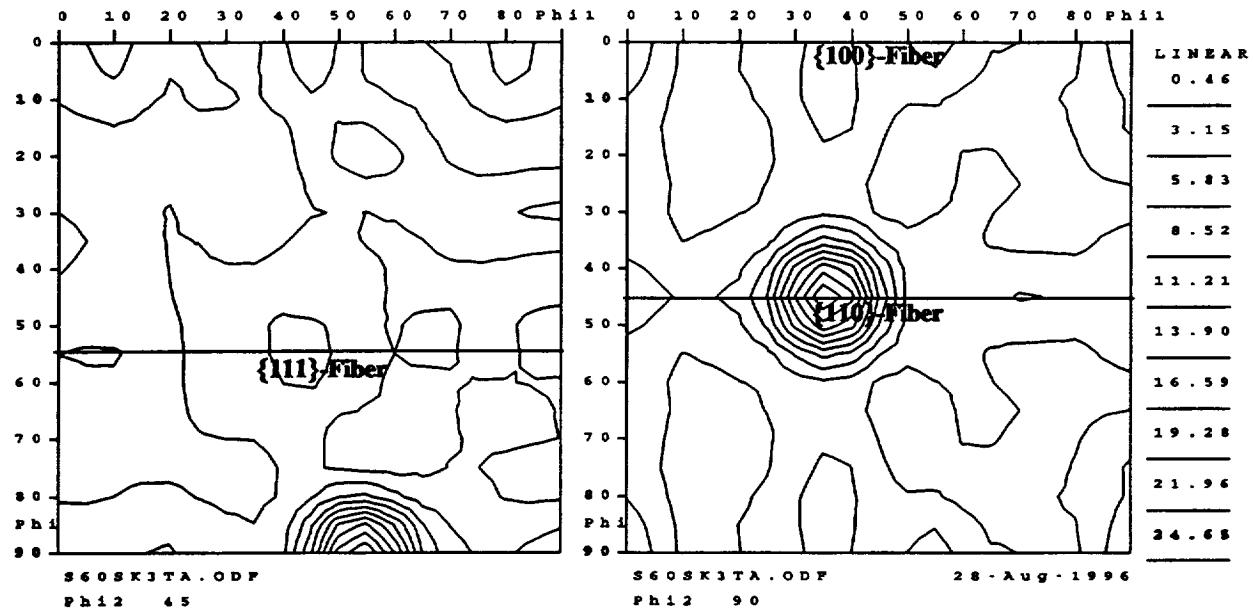


Figure 7. CODF sections for the 1460-T3 extrusion in the skin @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

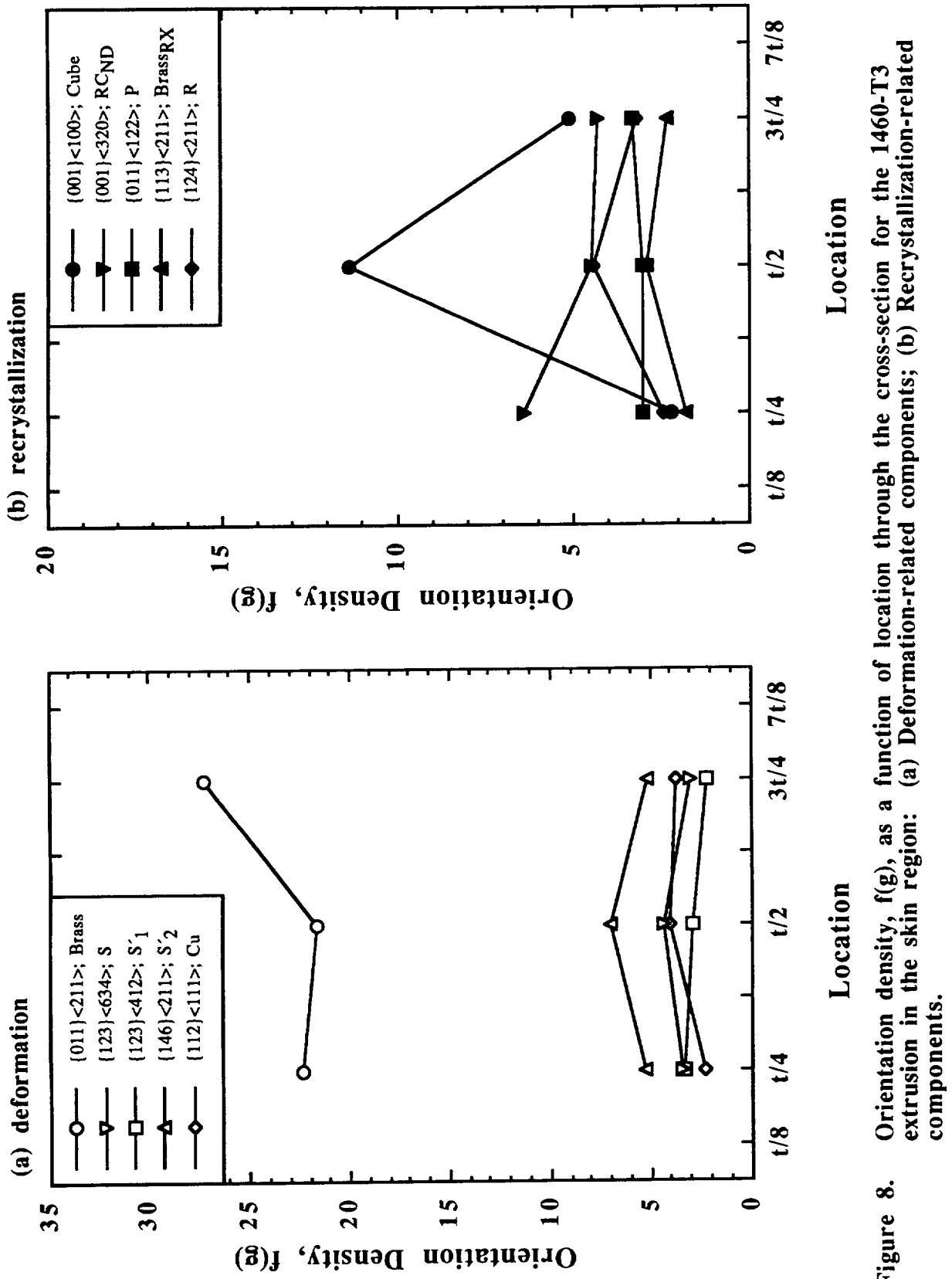


Figure 8. Orientation density, $f(g)$, as a function of location through the cross-section for the 1460-T3 extrusion in the skin region: (a) Deformation-related components; (b) Recrystallization-related components.

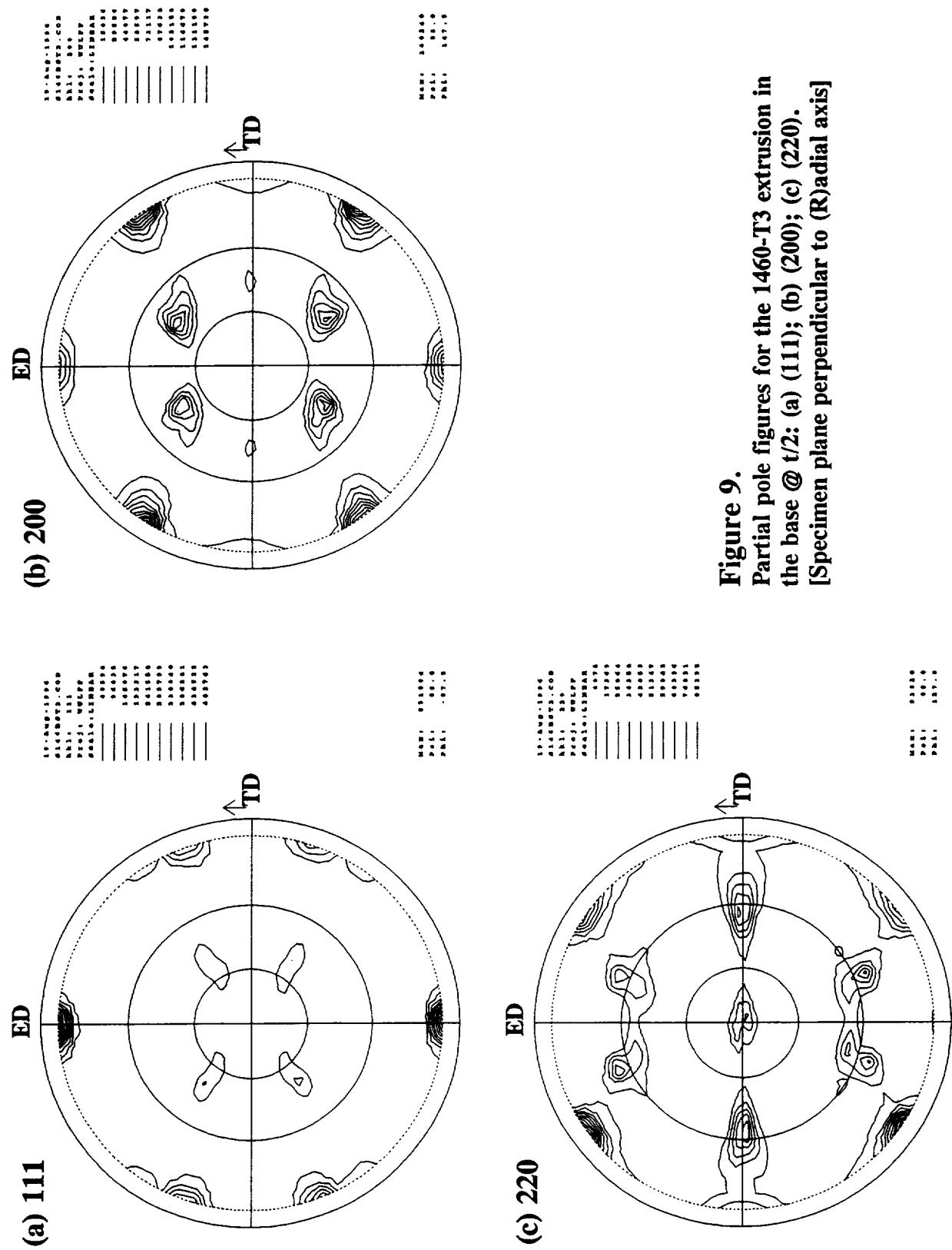
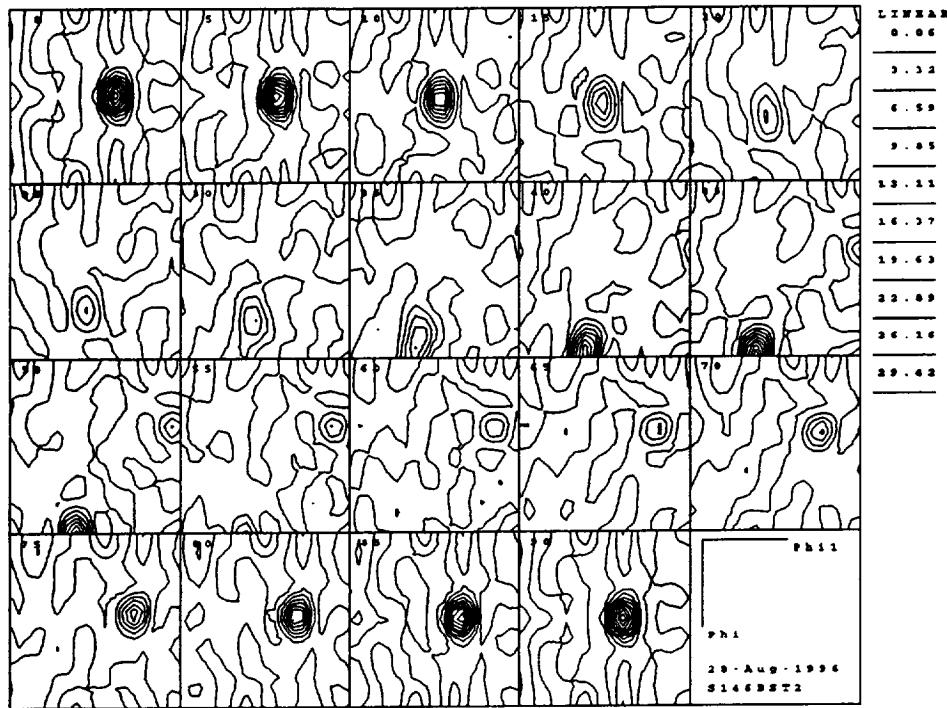


Figure 9.
Partial pole figures for the 1460-T3 extrusion in
the base @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

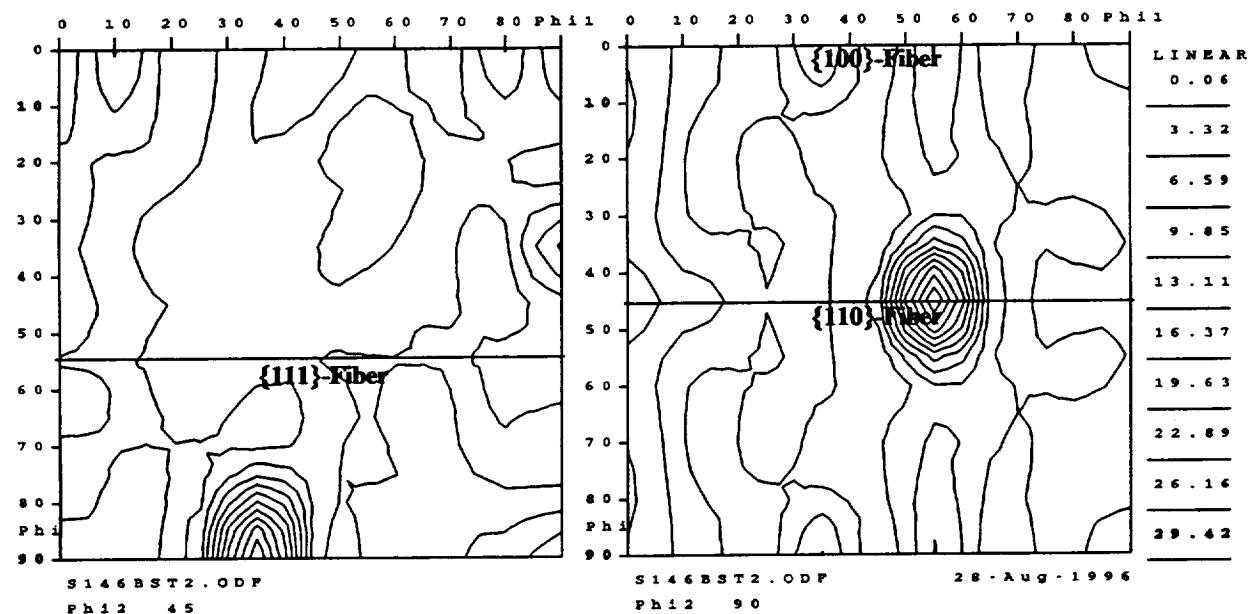


Figure 10. CODF sections for the 1460-T3 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

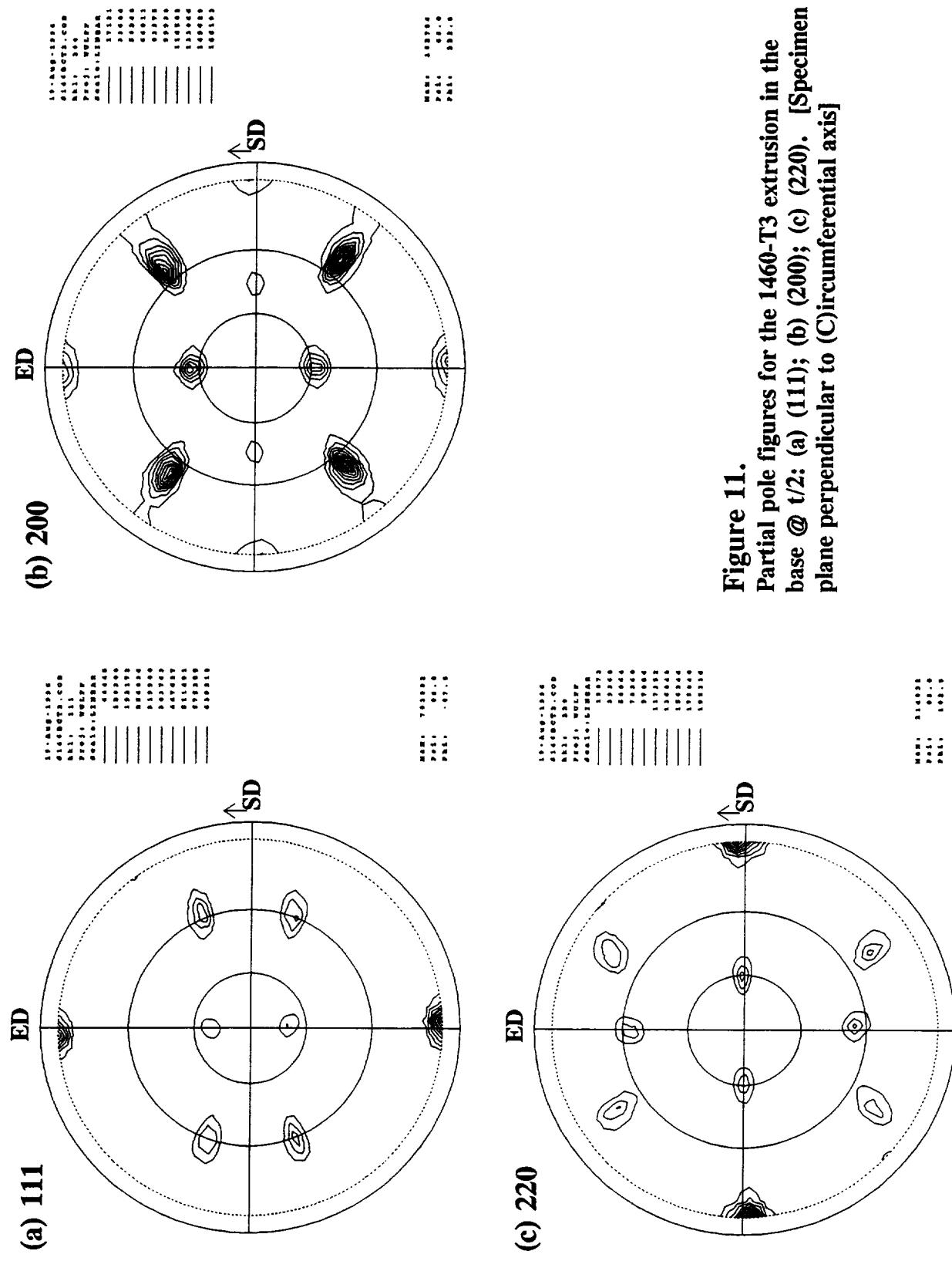
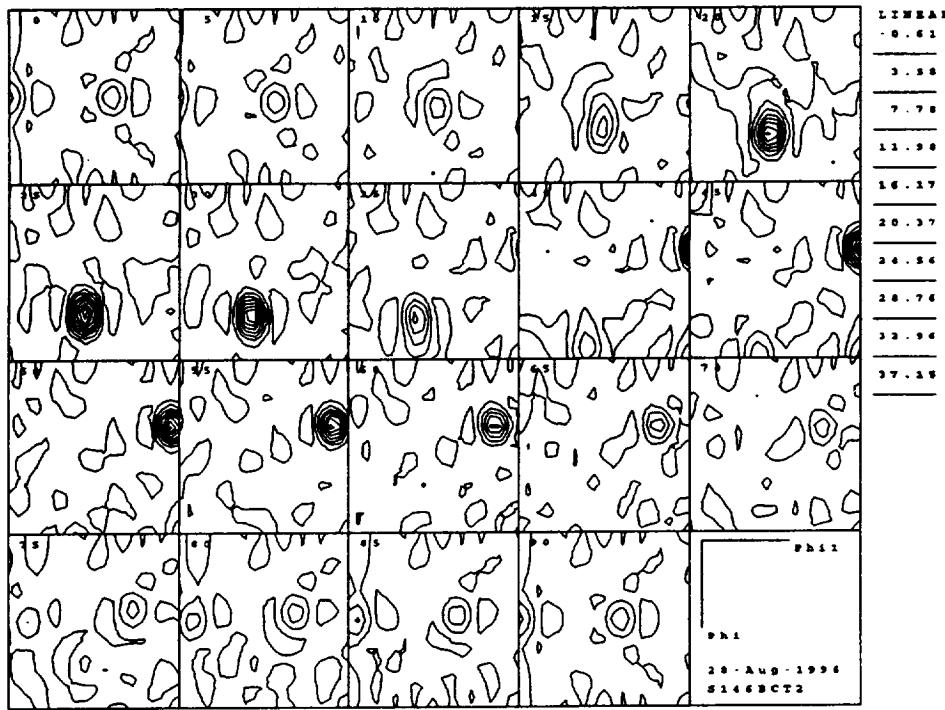


Figure 11.
Partial pole figures for the 1460-T3 extrusion in the
base @ $t/2$: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

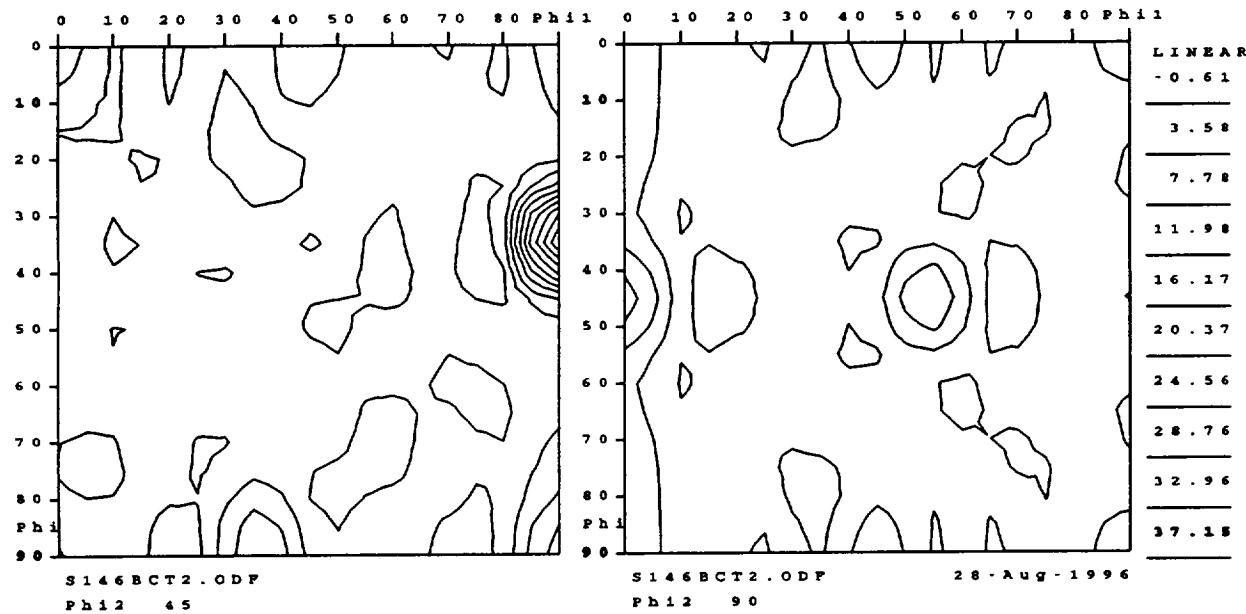


Figure 12. CODF sections for the 1460-T3 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

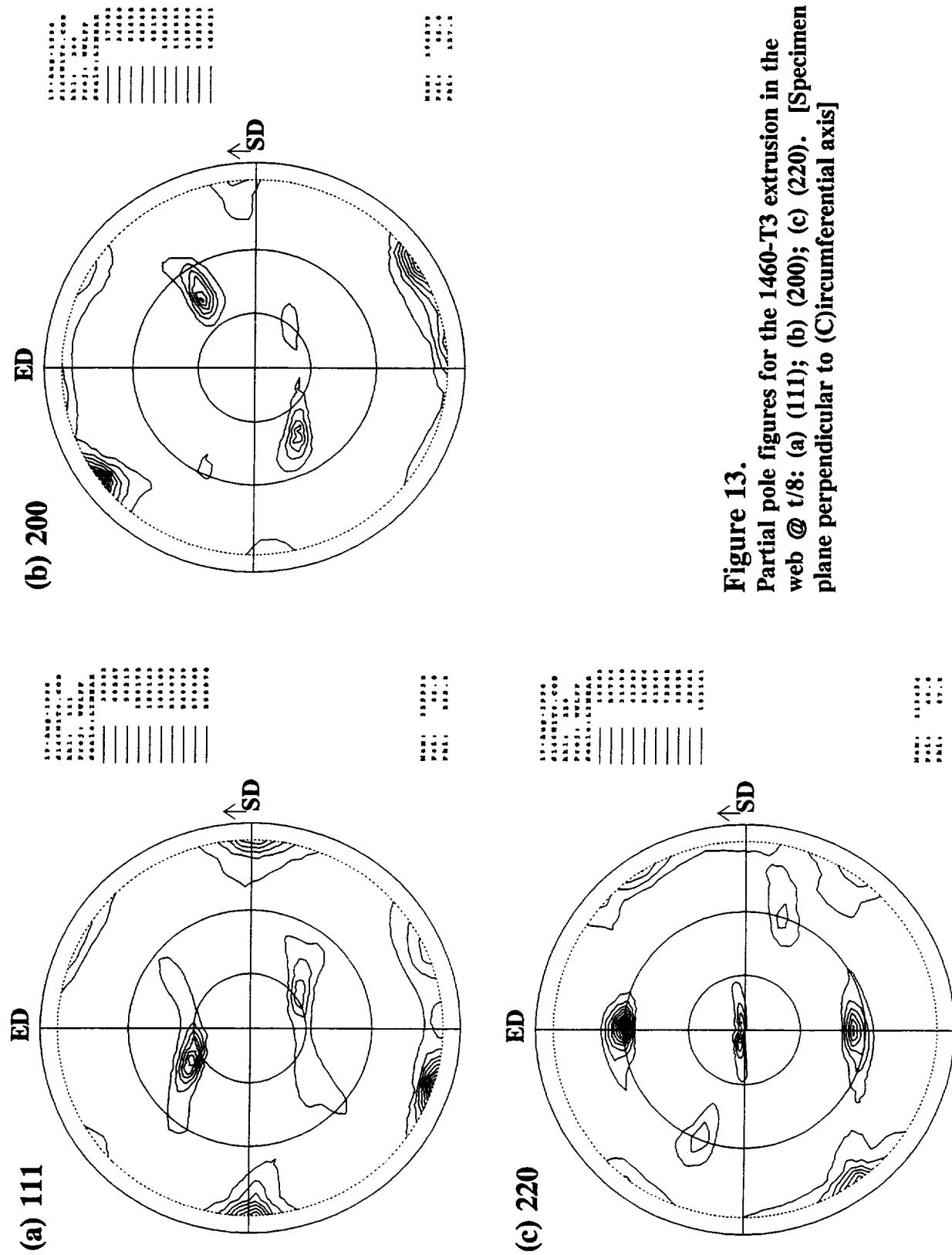
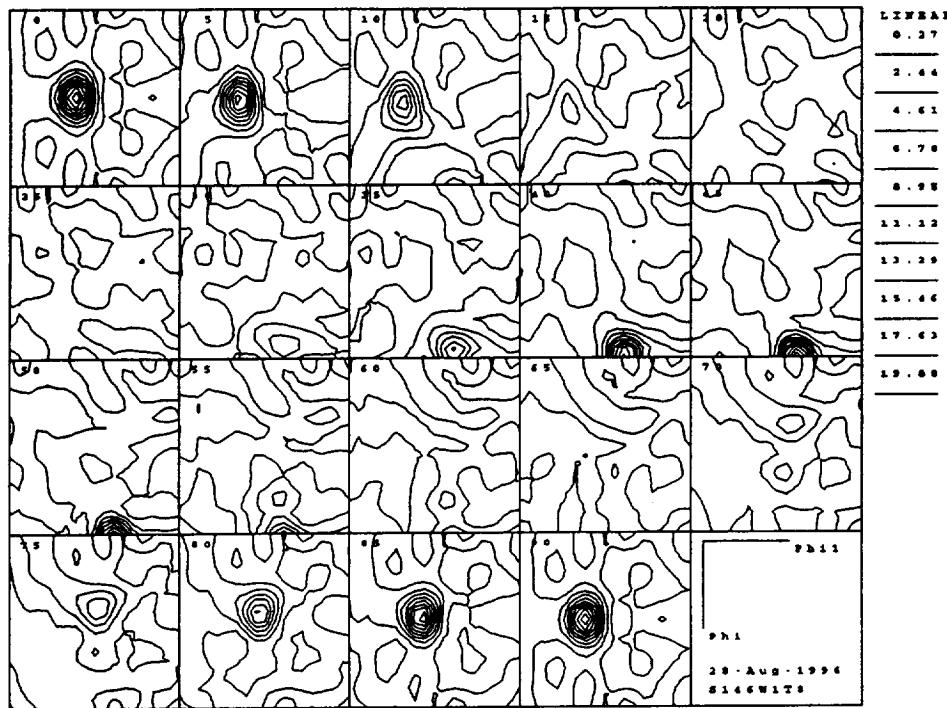


Figure 13.
Partial pole figures for the 1460-T3 extrusion in the
web @ $t/8$: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

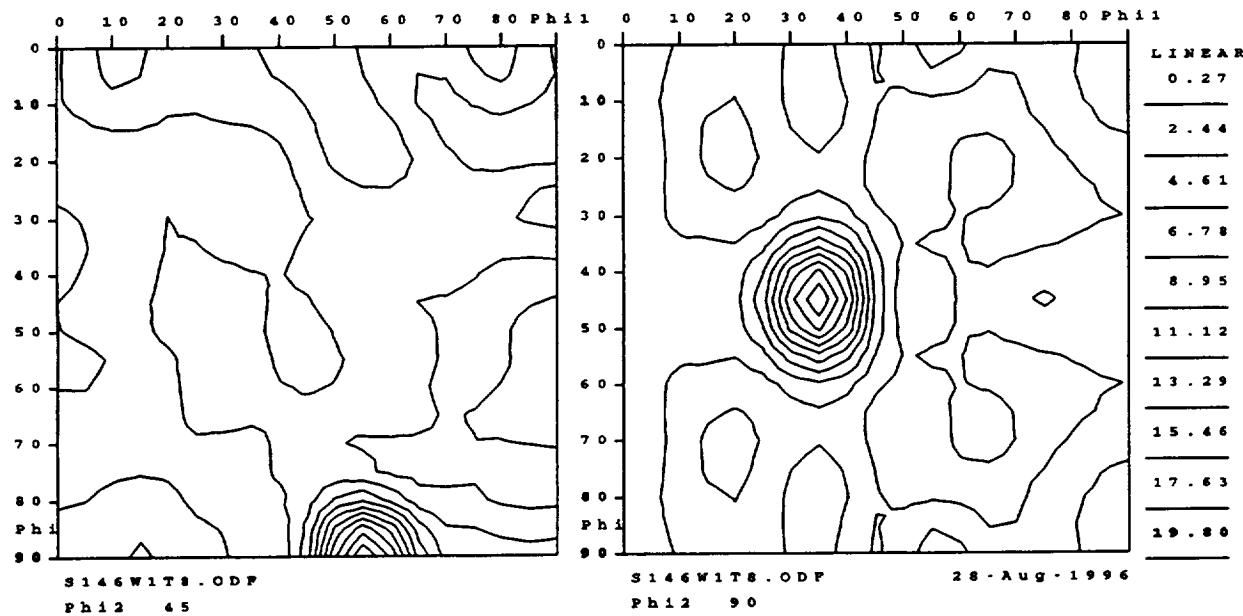


Figure 14. CODF sections for the 1460-T3 extrusion in the web @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

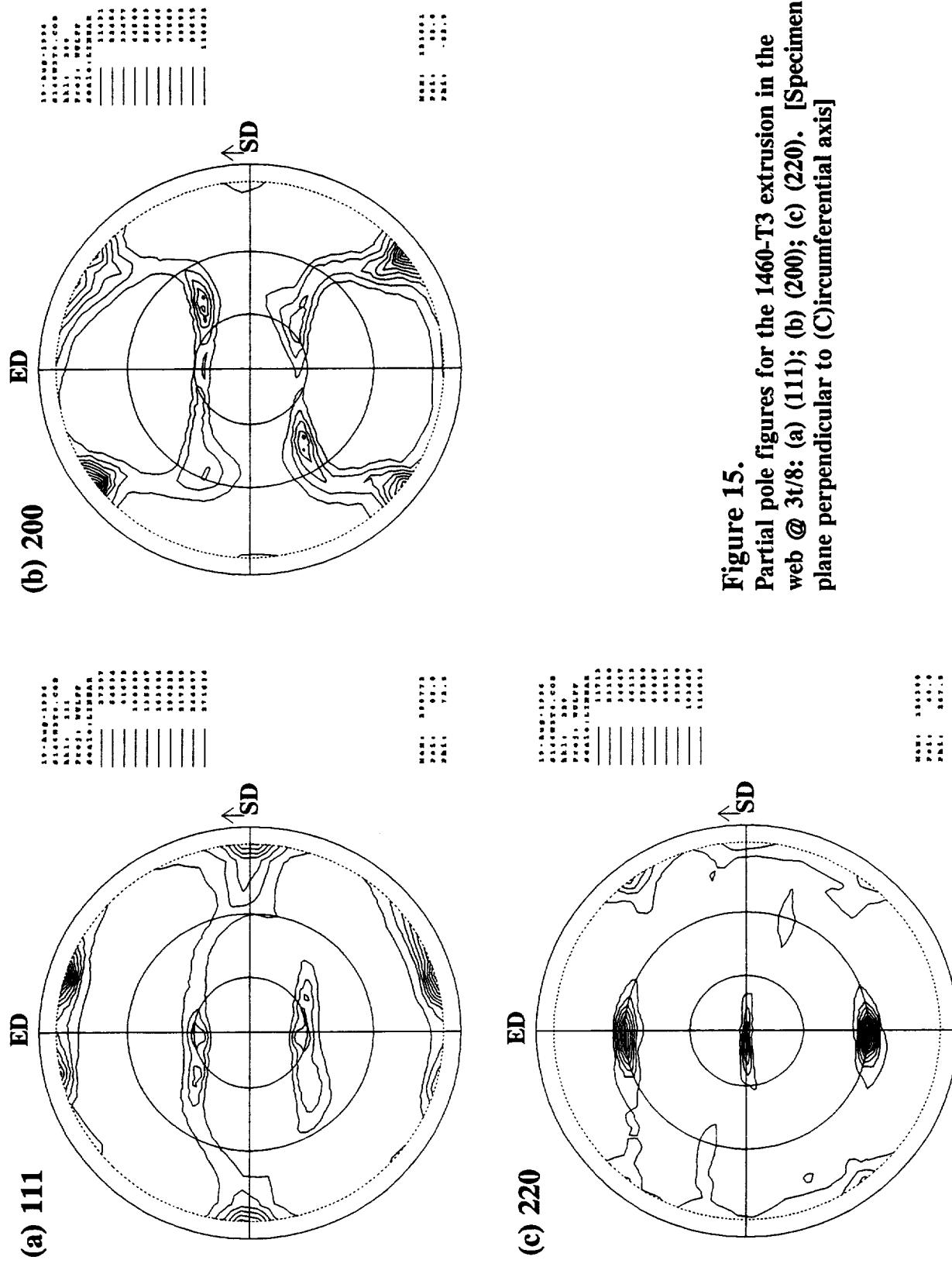
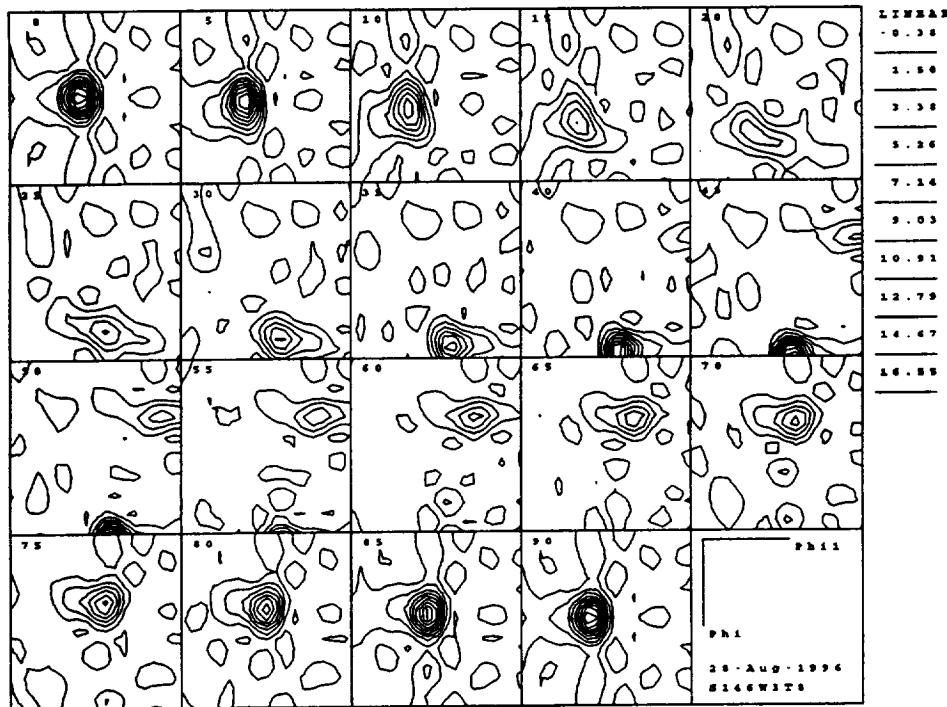


Figure 15.
Partial pole figures for the 1460-T3 extrusion in the
web @ 3t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

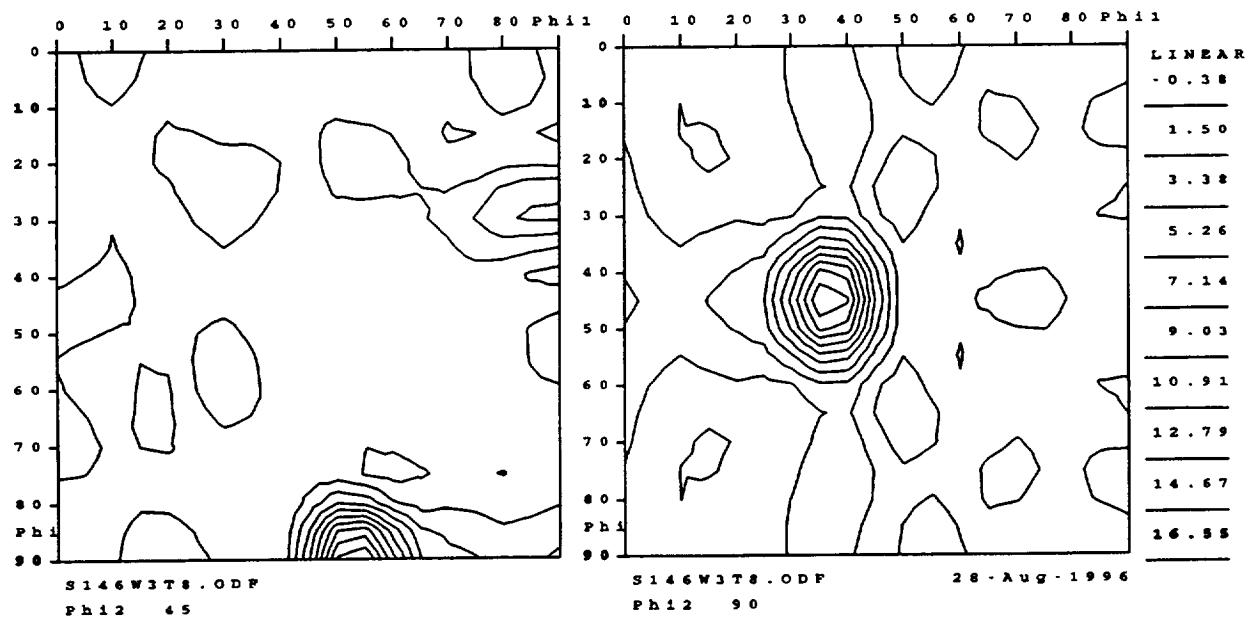


Figure 16. CODF sections for the 1460-T3 extrusion in the web @ 3t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

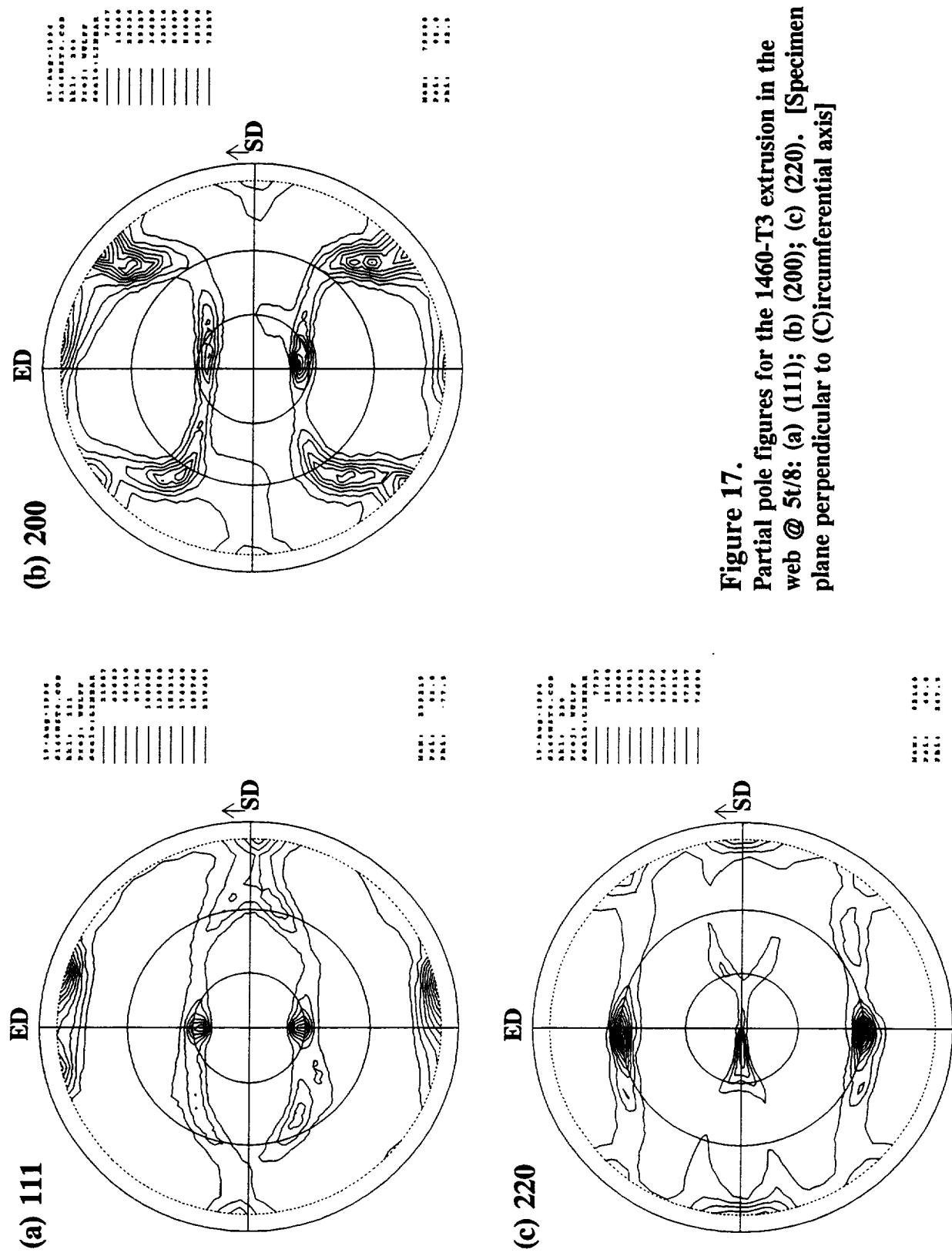
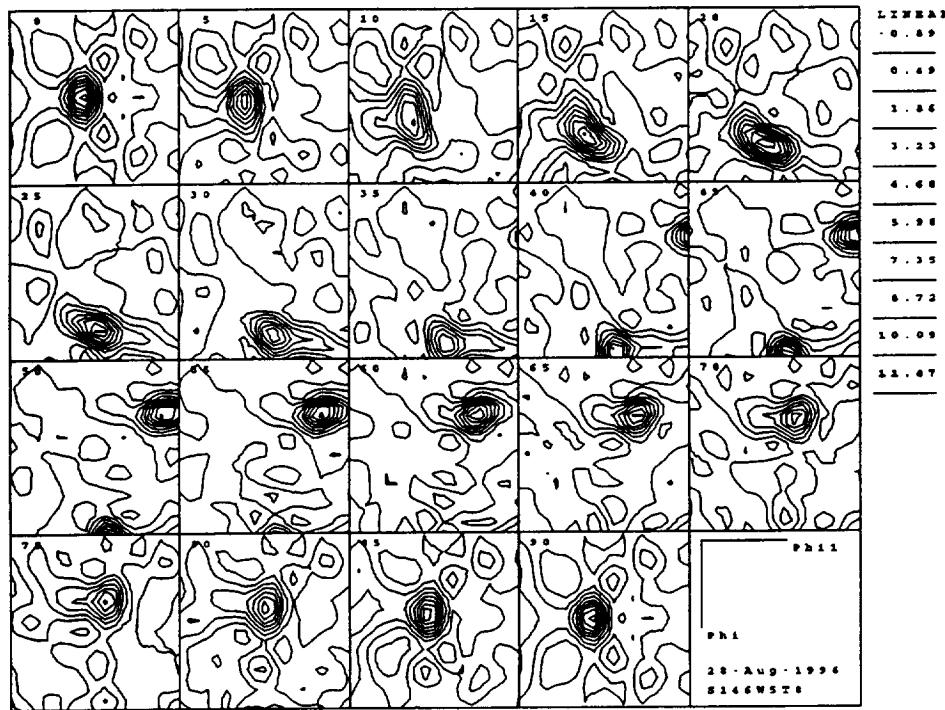


Figure 17.
Partial pole figures for the 1460-T3 extrusion in the
web @ 5t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

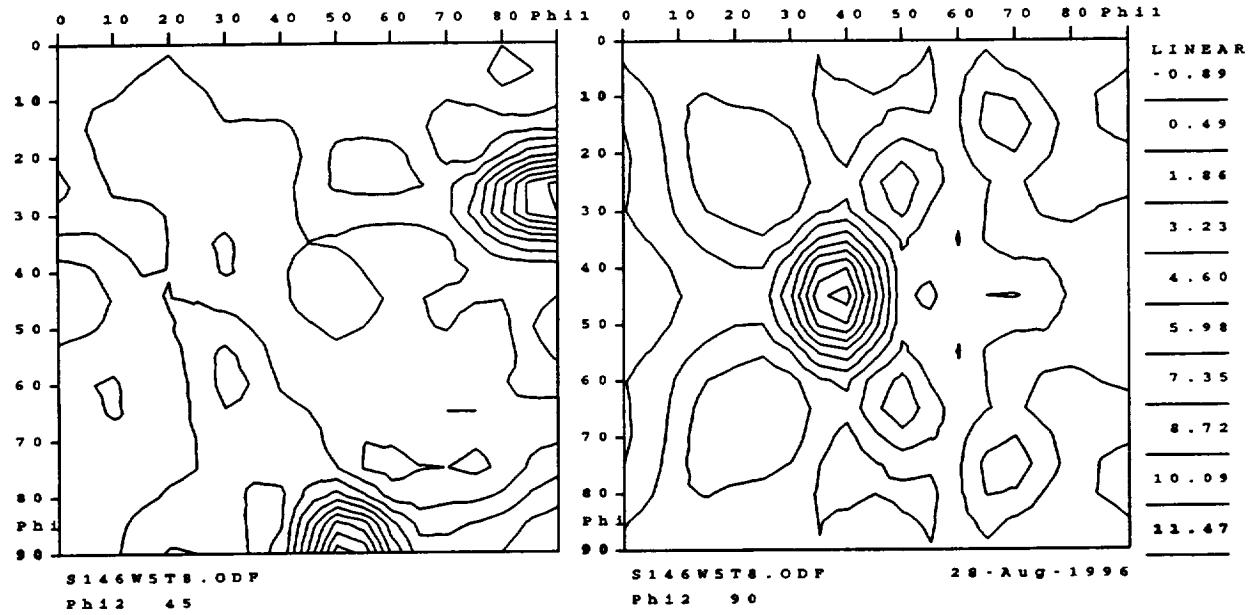


Figure 18. CODF sections for the 1460-T3 extrusion in the web @ 5t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

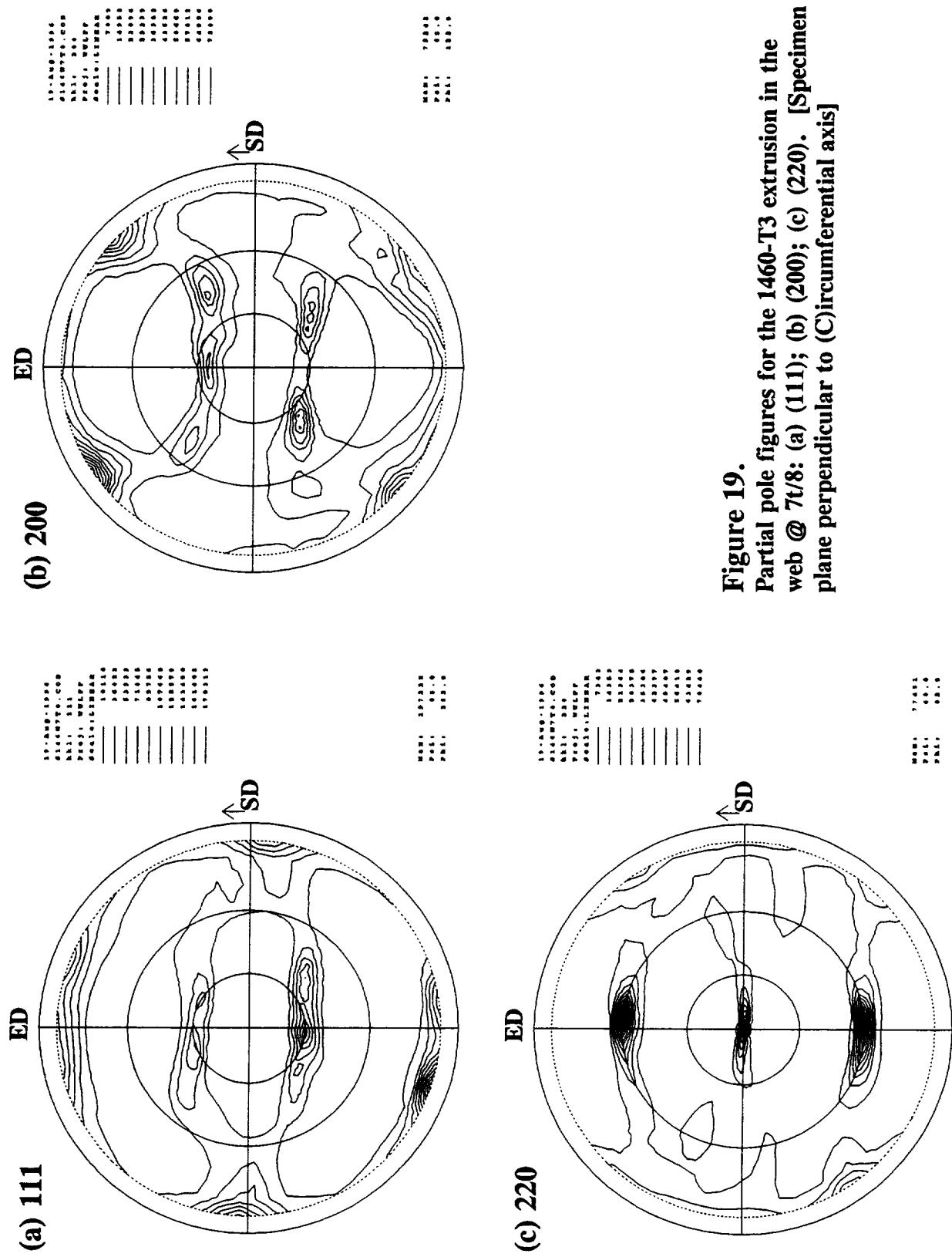
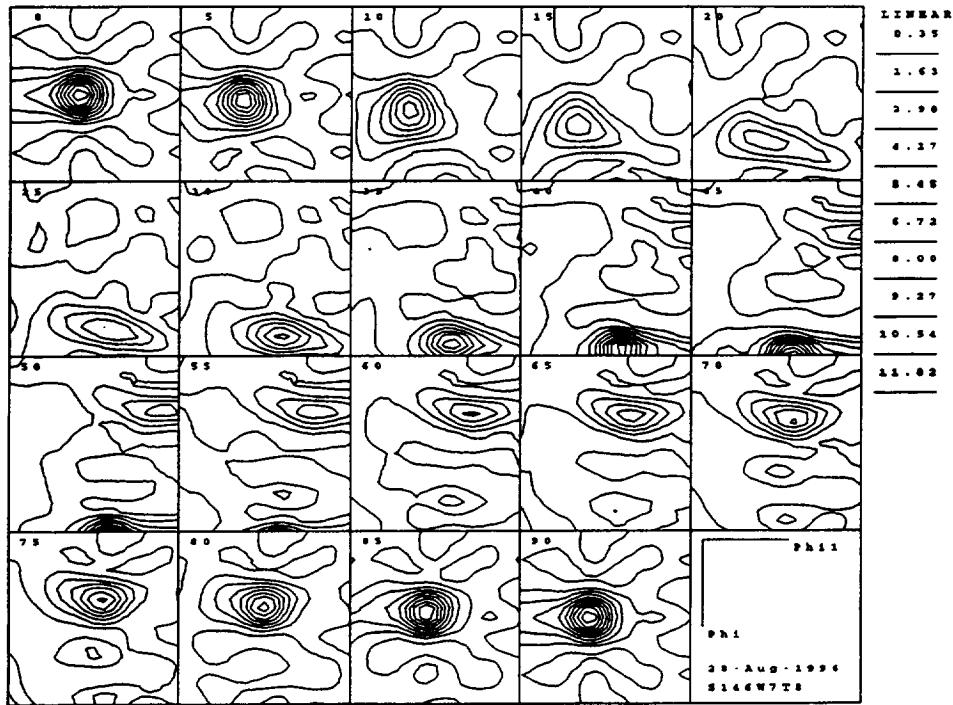


Figure 19.
Partial pole figures for the 1460-T3 extrusion in the
web @ 7/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

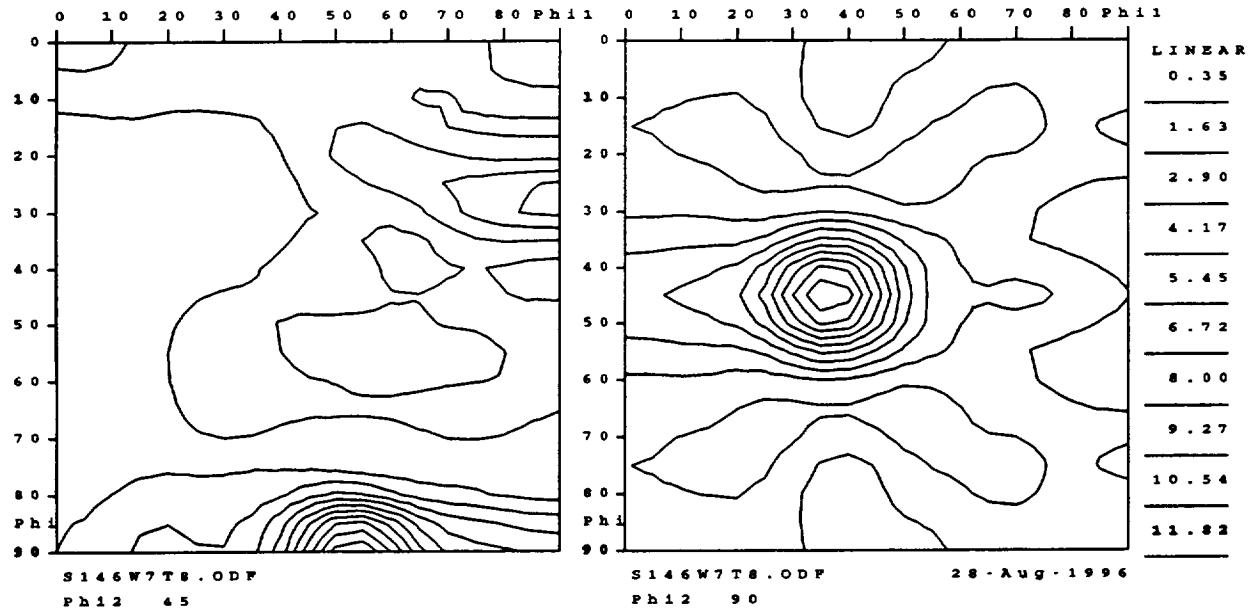


Figure 20. CODF sections for the 1460-T3 extrusion in the web @ 7t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

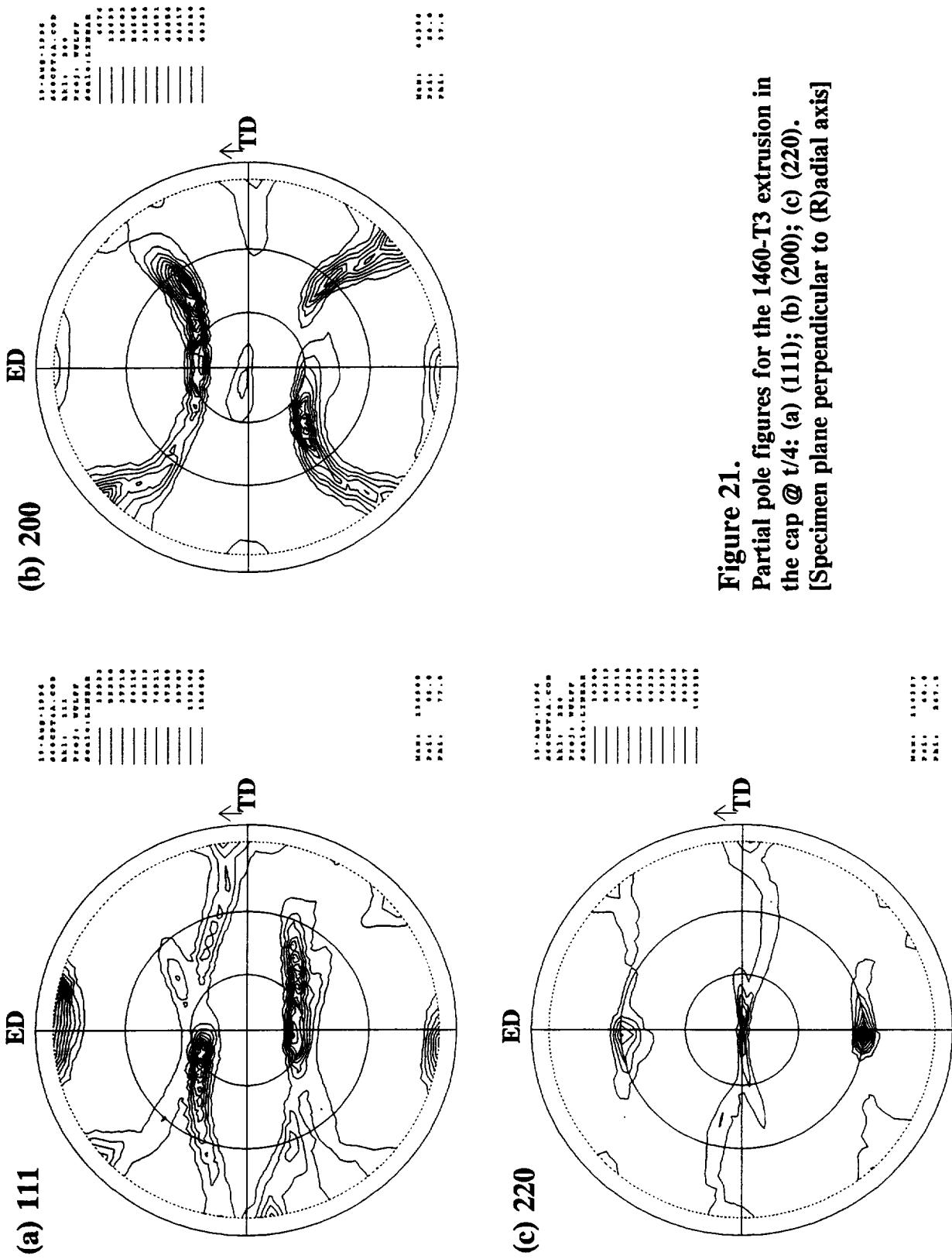
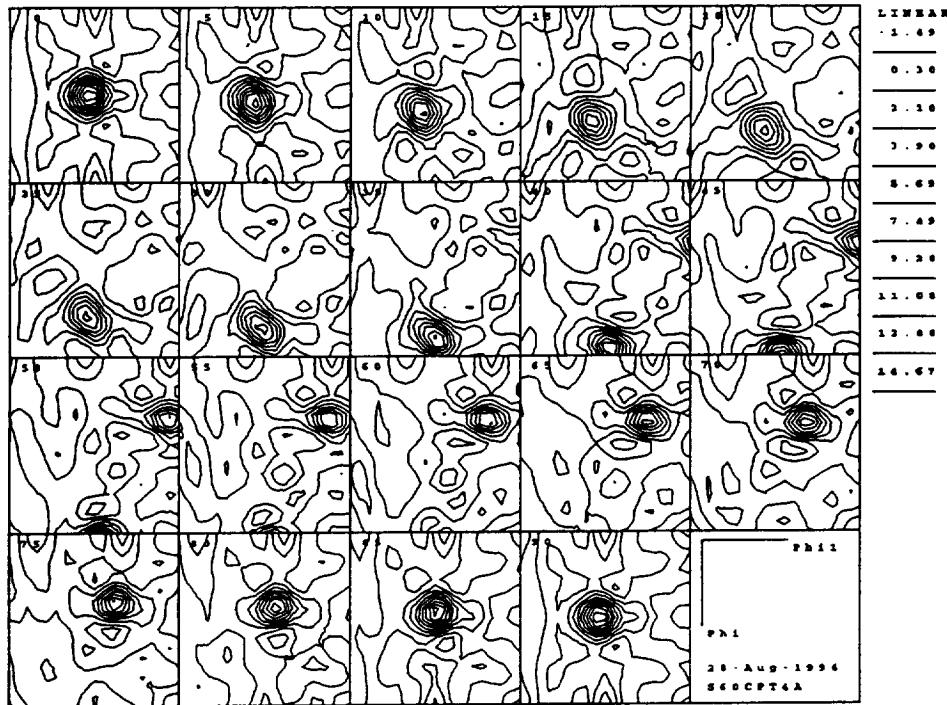


Figure 21.
Partial pole figures for the 1460-T3 extrusion in
the cap @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

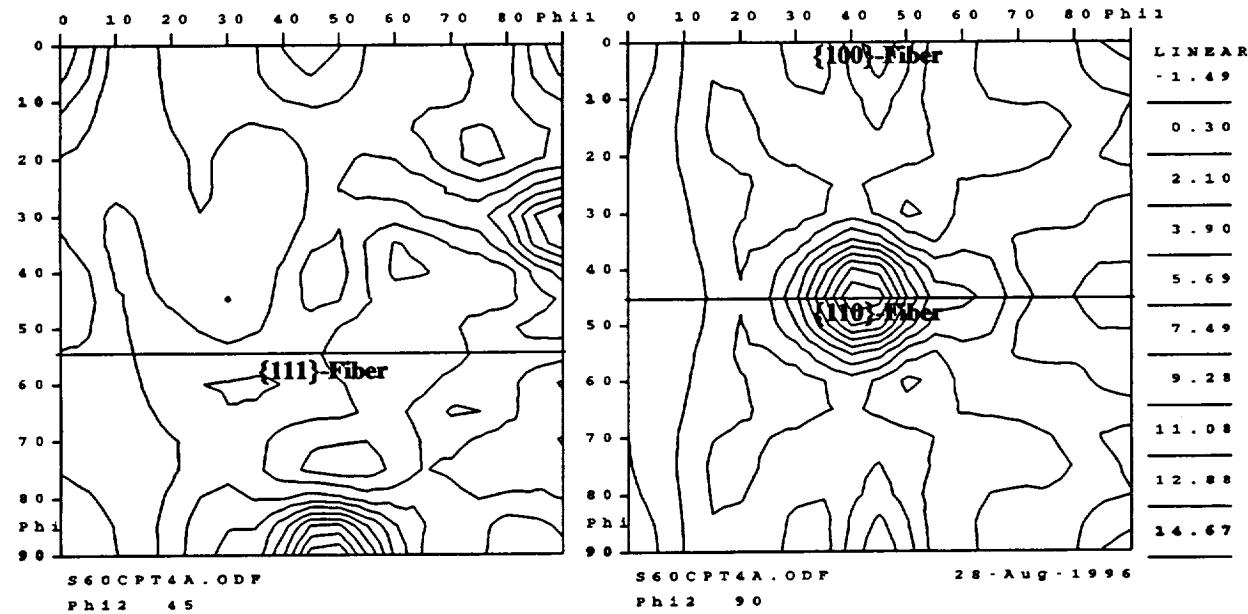


Figure 22. CODF sections for the 1460-T3 extrusion in the cap @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

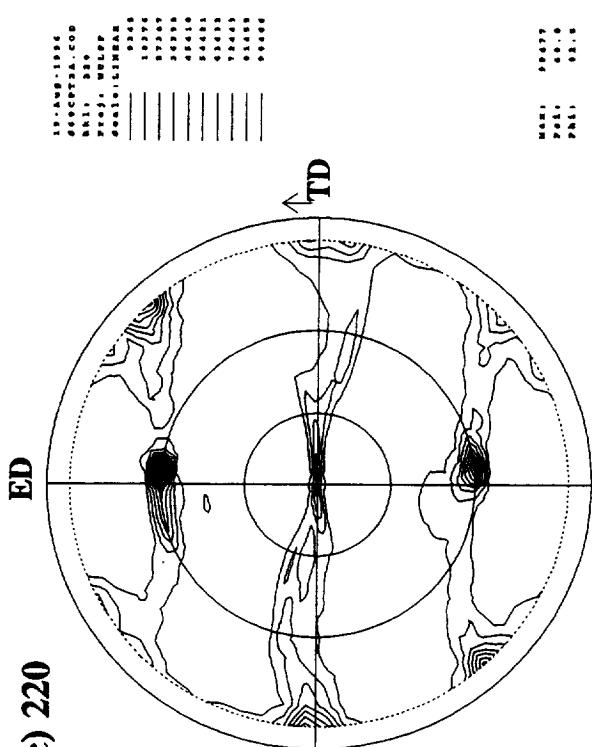
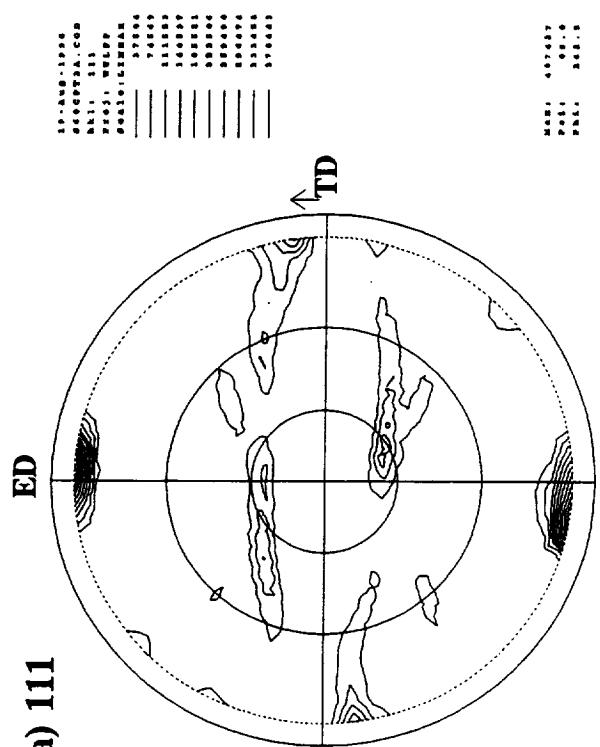
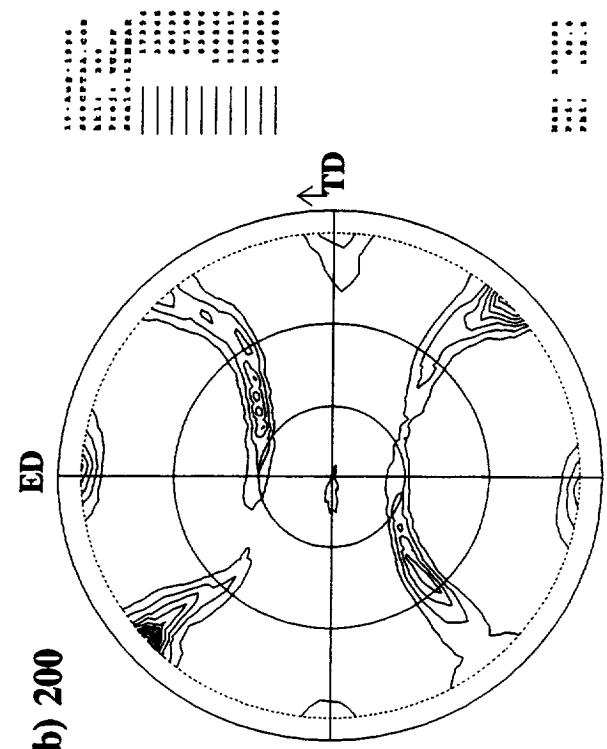
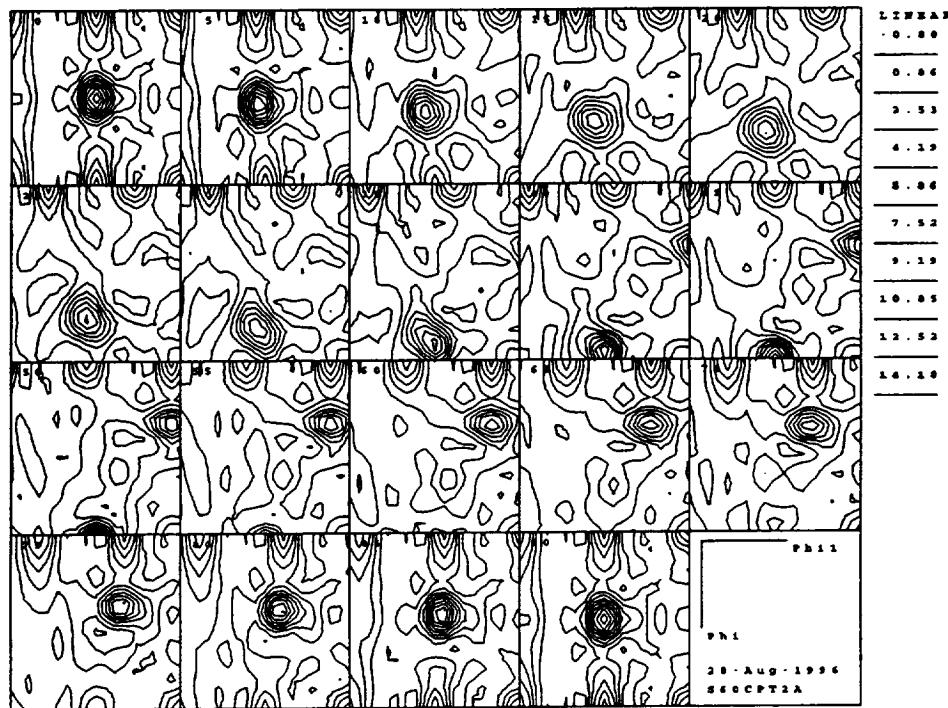


Figure 23.
Partial pole figures for the 1460-T3 extrusion in
the cap @ t/2: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

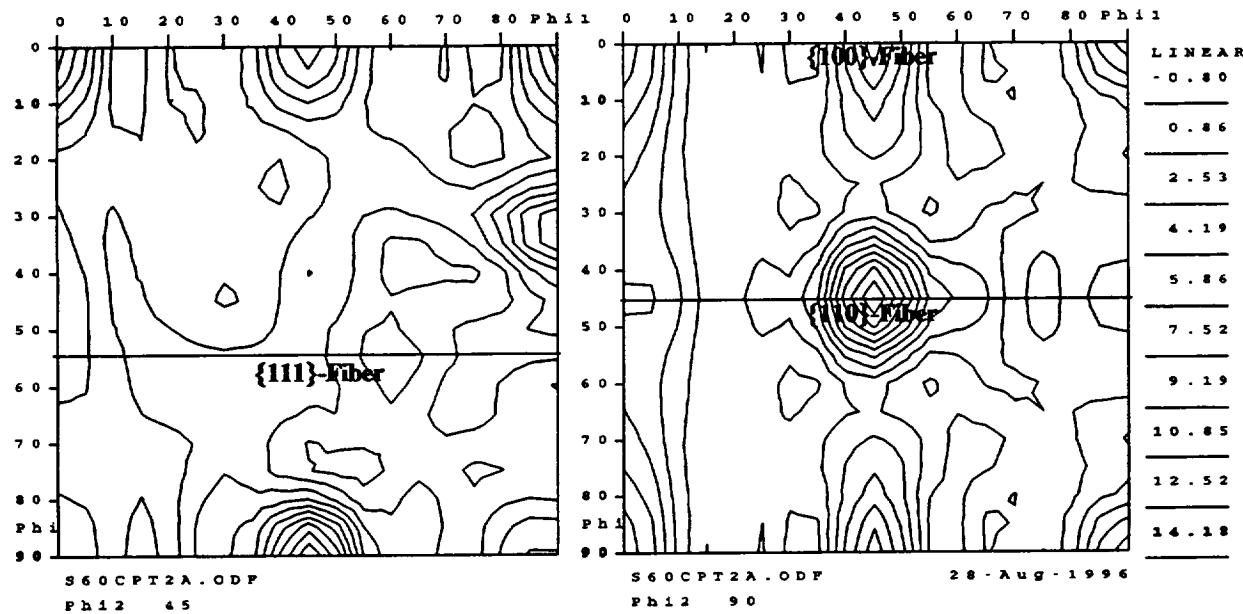


Figure 24. CODF sections for the 1460-T3 extrusion in the cap @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

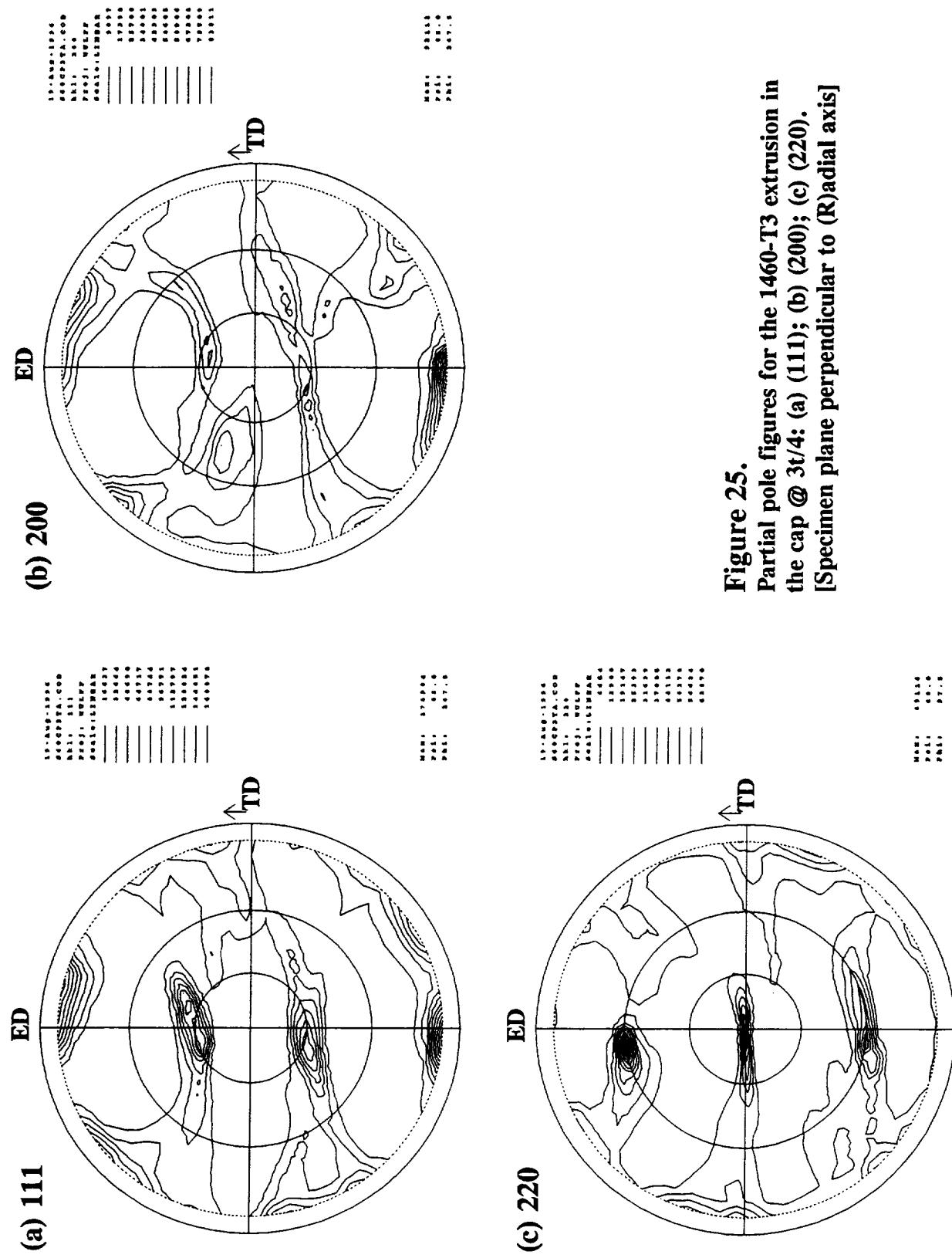
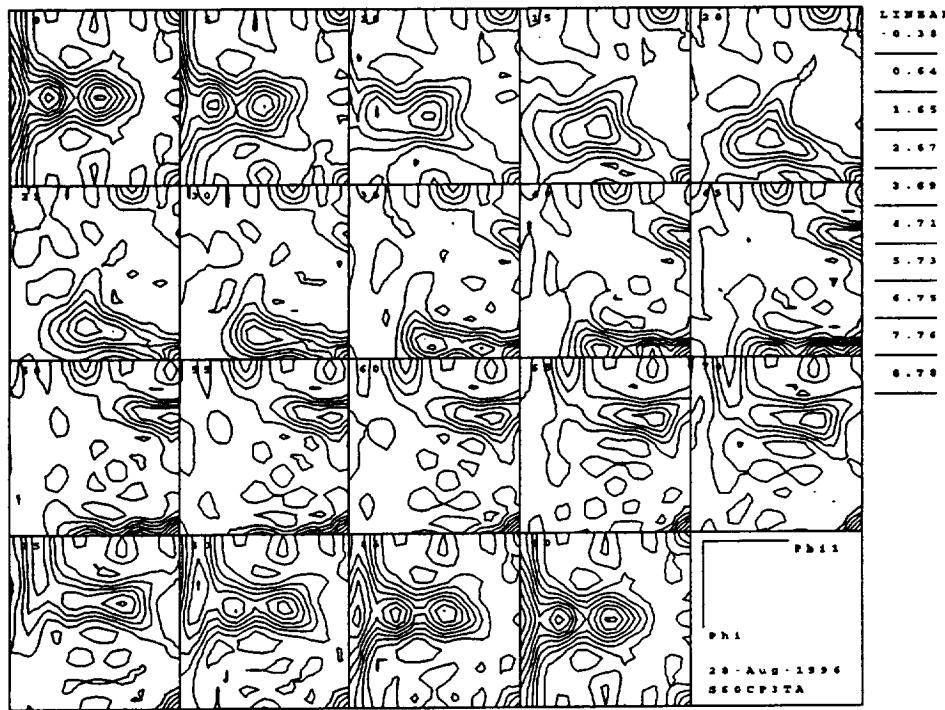


Figure 25.
Partial pole figures for the 1460-T3 extrusion in
the cap @ 3t/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

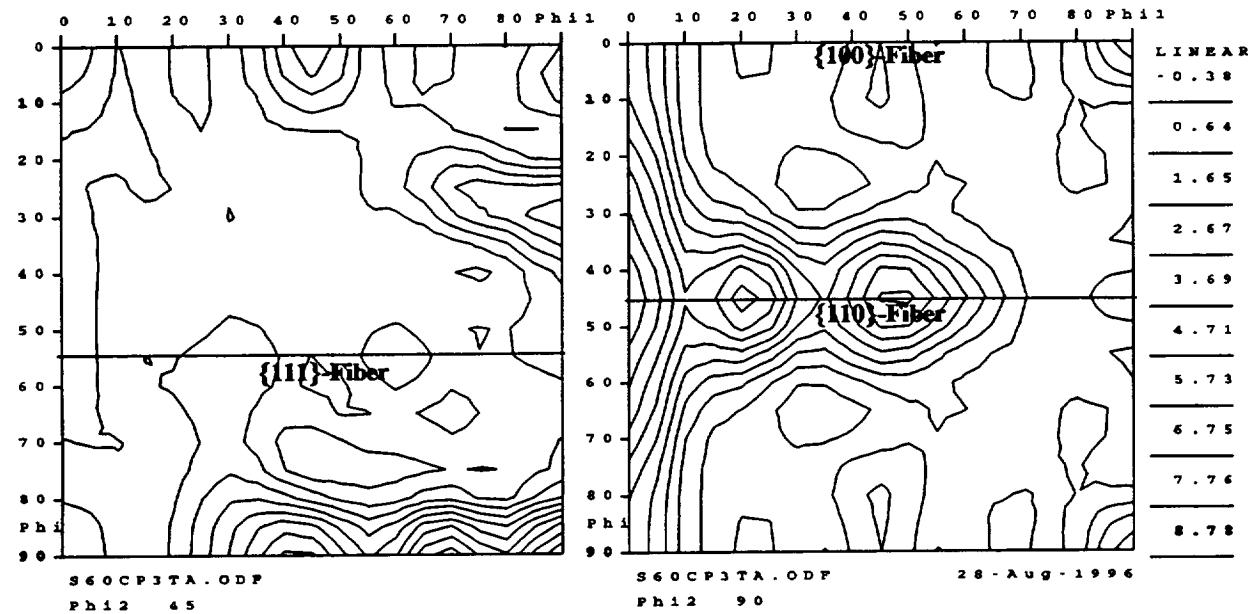


Figure 26. CODF sections for the 1460-T3 extrusion in the cap @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

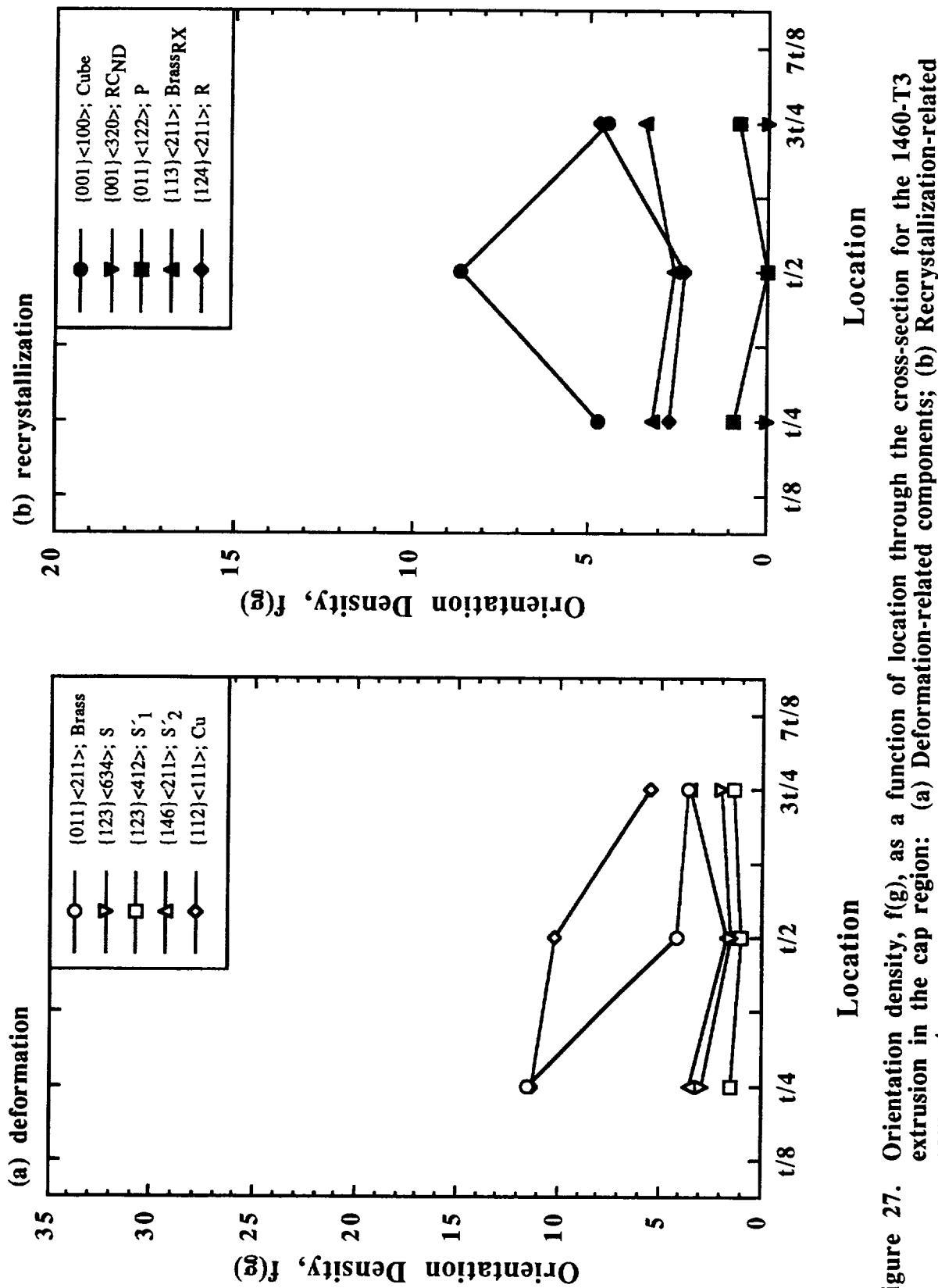


Figure 27. Orientation density, $f(g)$, as a function of location through the cross-section for the 1460-T3 extrusion in the cap region: (a) Deformation-related components; (b) Recrystallization-related components.

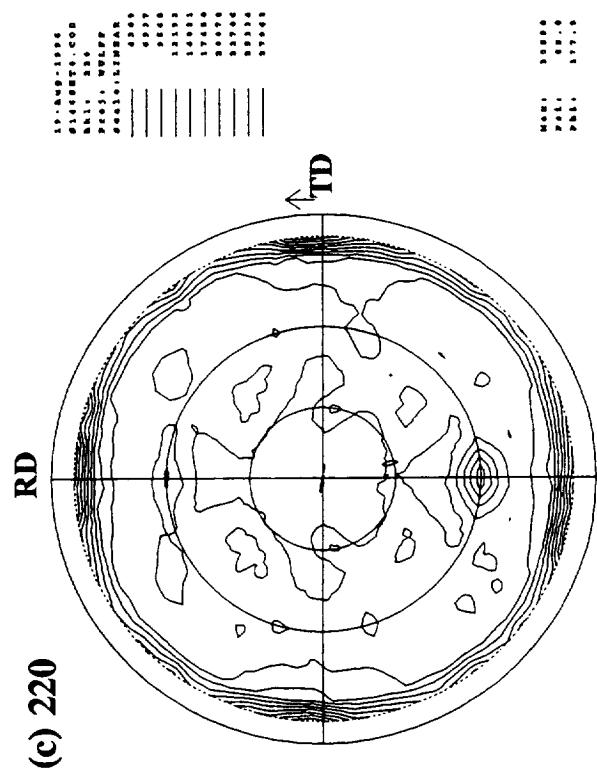
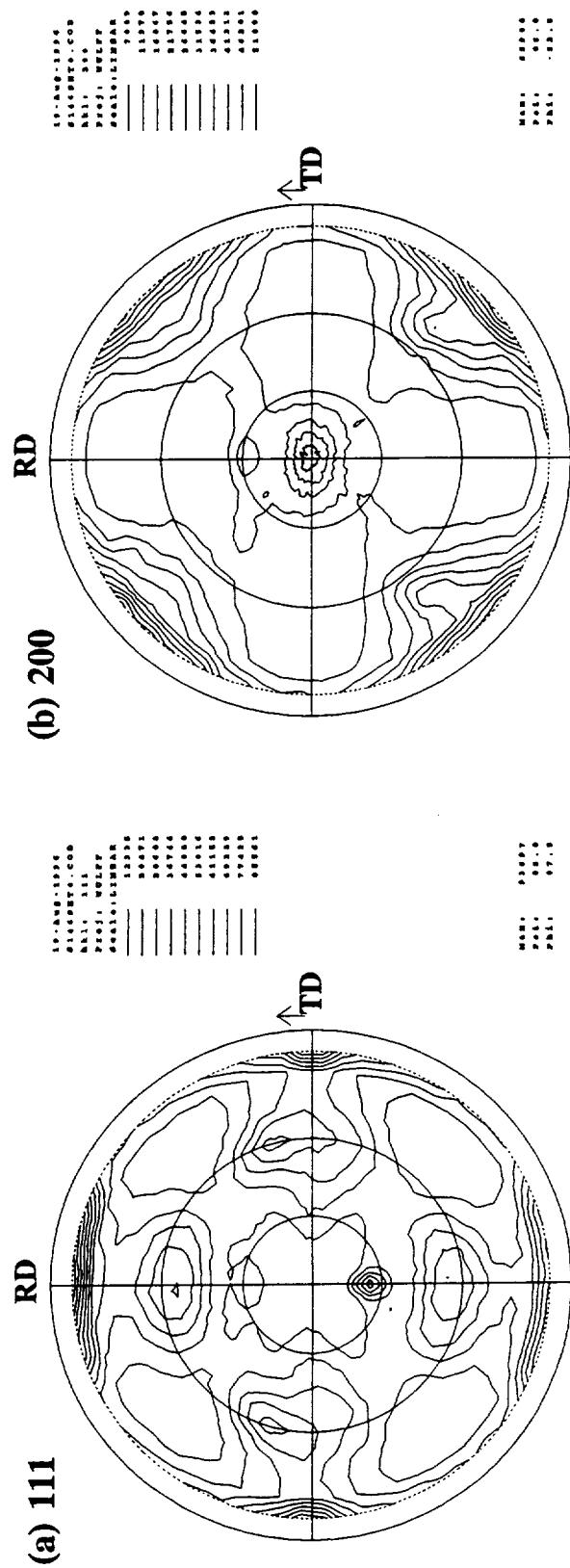
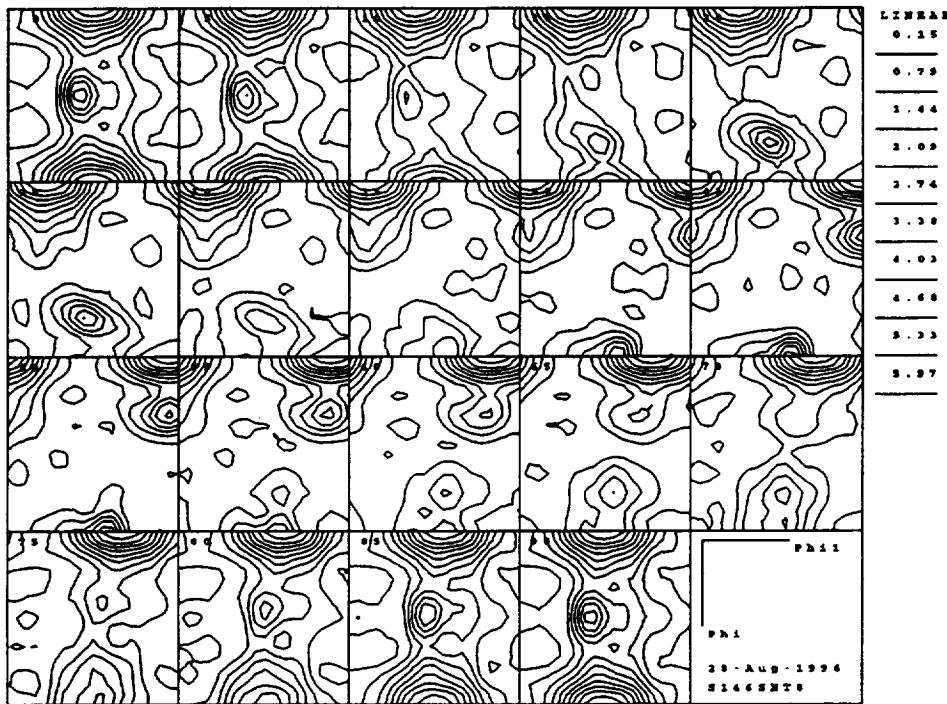


Figure 28.
 Partial pole figures for 1460-T3 sheet @ t/8:
 (a) (111); (b) (200); (c) (220). [Specimen plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

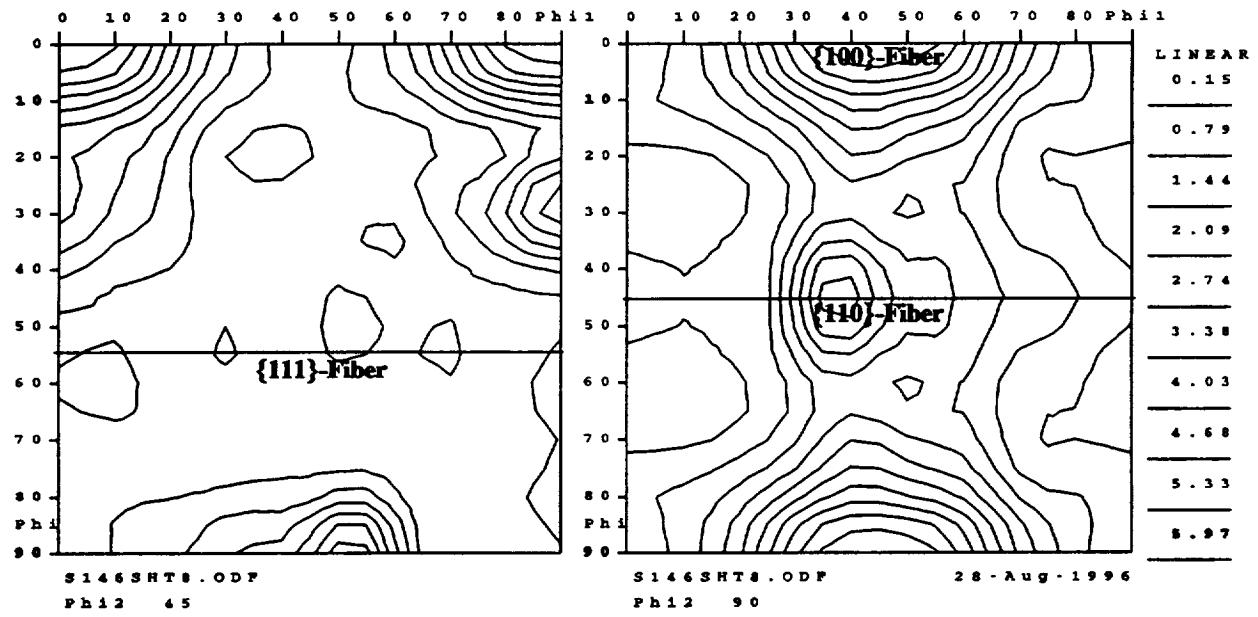


Figure 29. CODF sections for 1460-T3 sheet @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

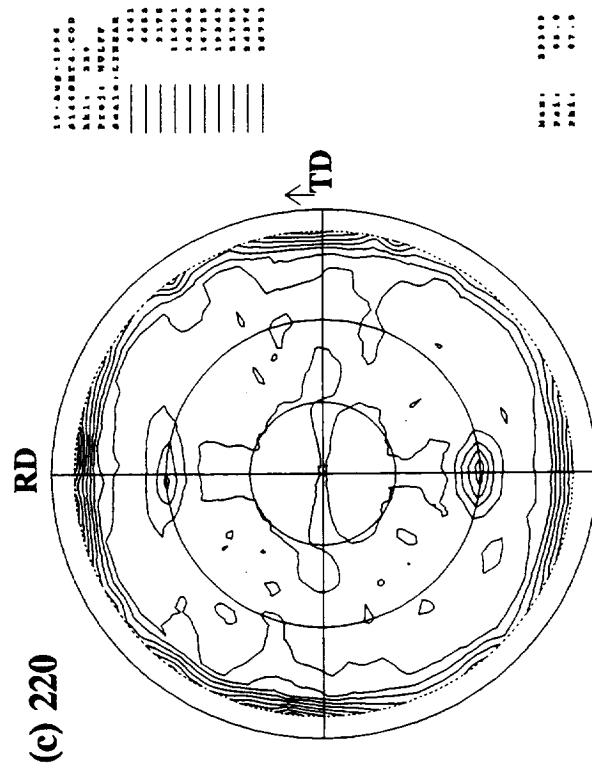
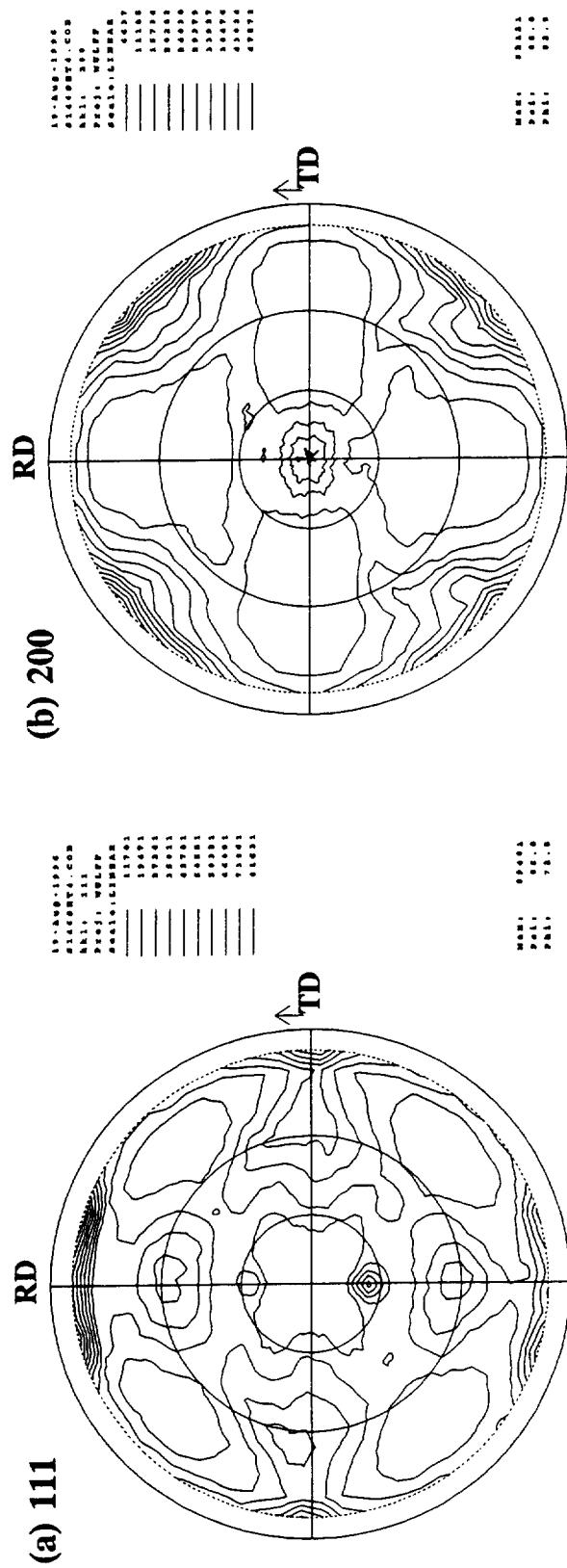
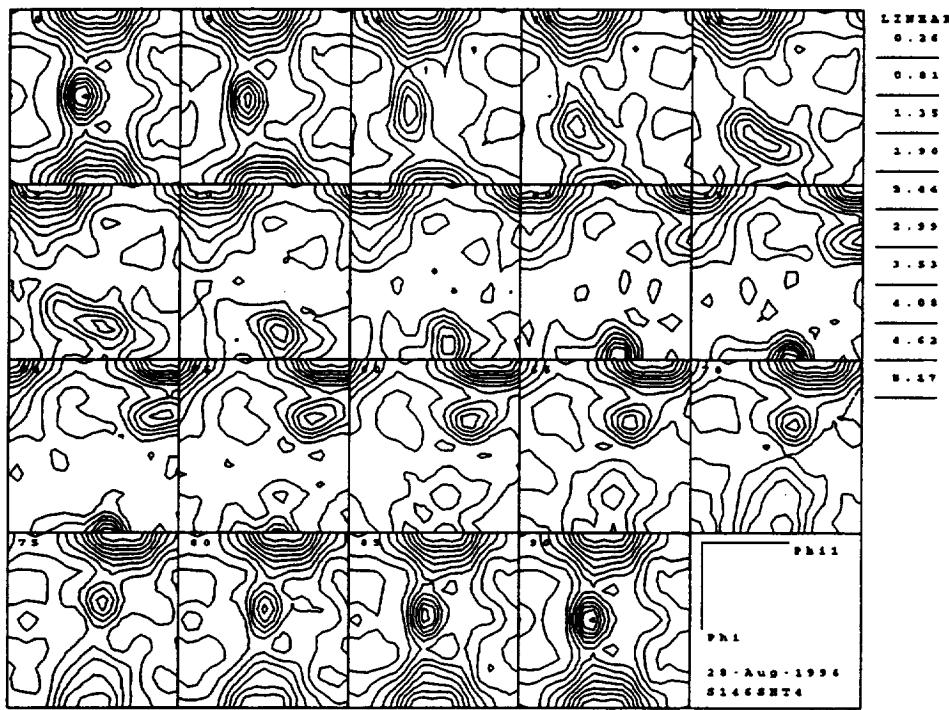


Figure 30.
Partial pole figures for 1460-T3 sheet @ $t/4$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

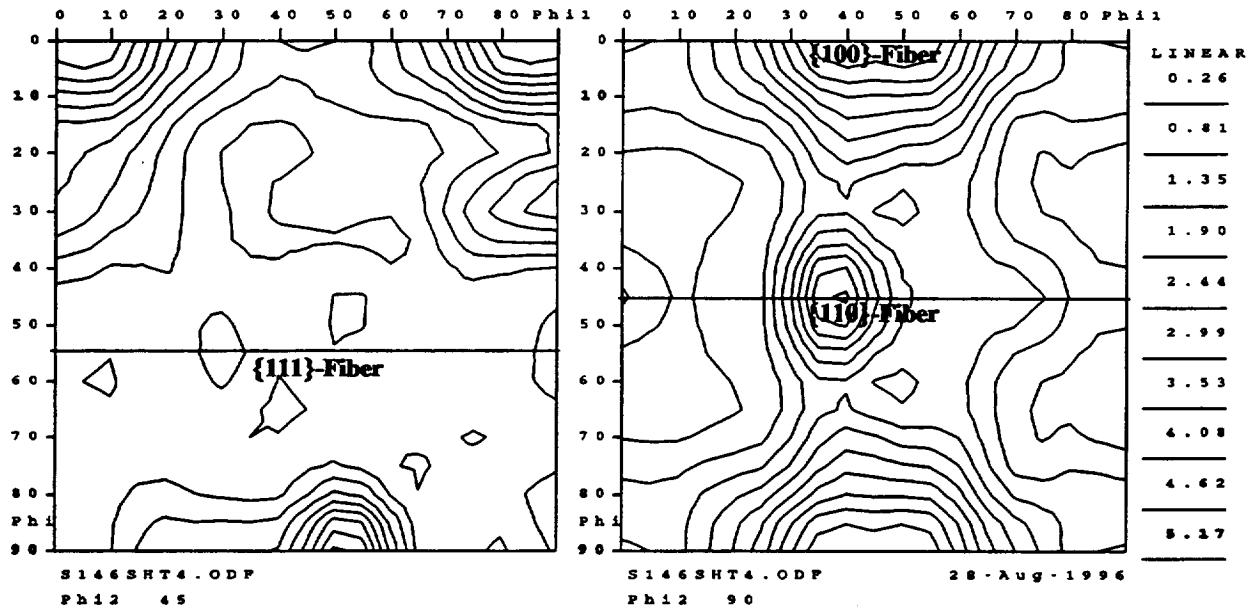


Figure 31. CODF sections for 1460-T3 sheet @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.

[Specimen plane perpendicular to (S)hort-Transverse axis]

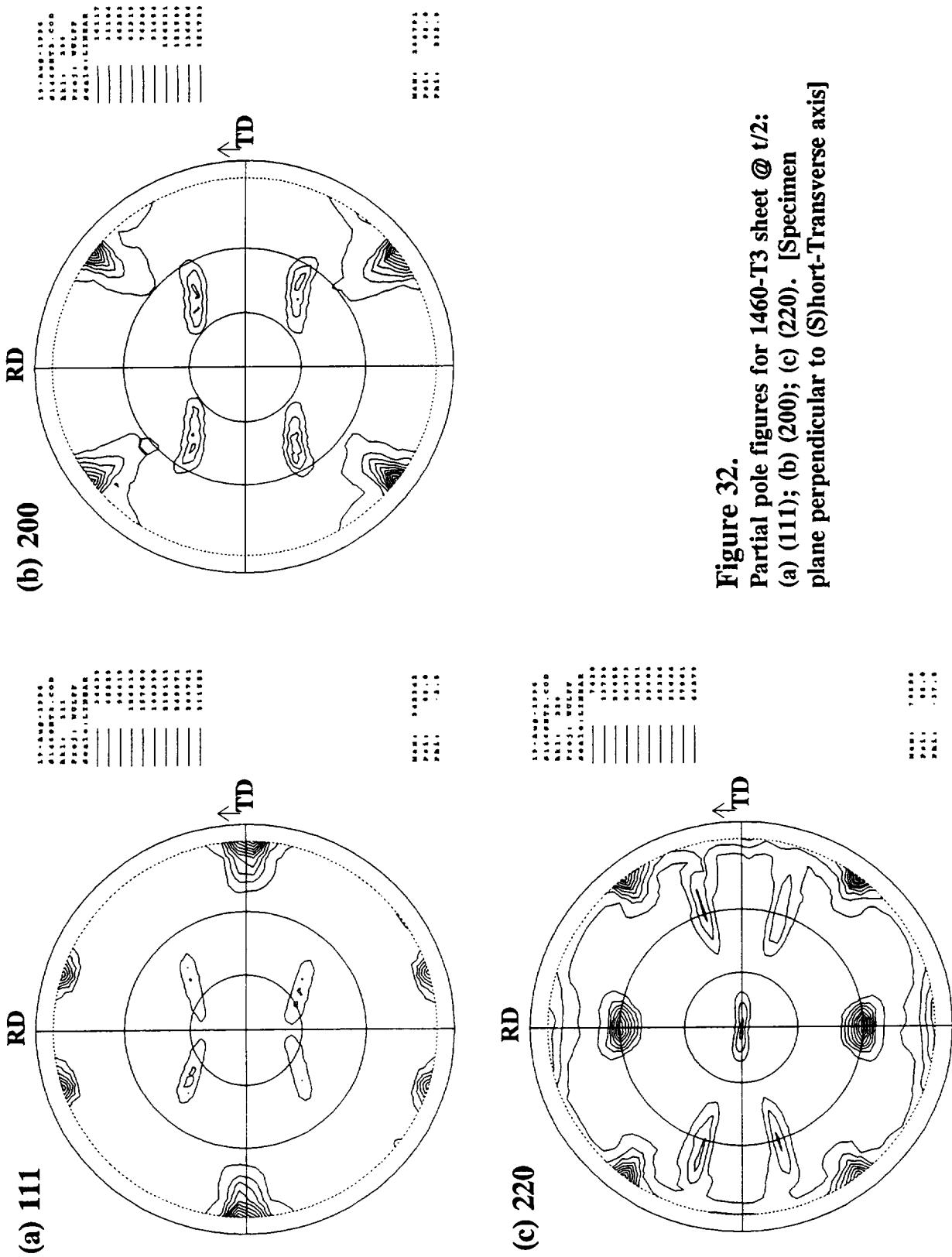
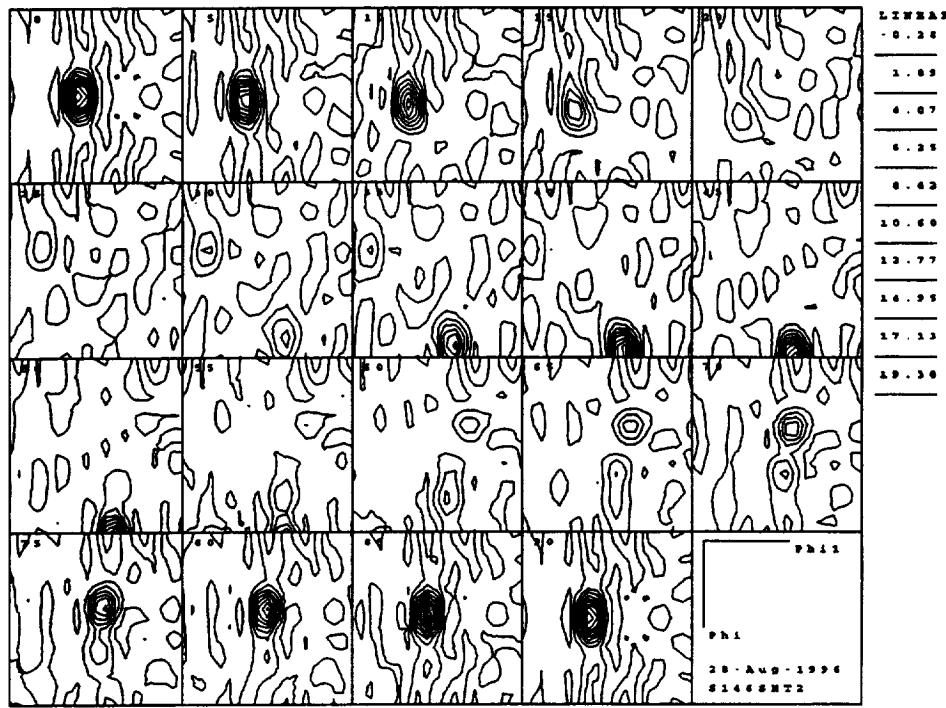


Figure 32.
Partial pole figures for 1460-T3 sheet @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

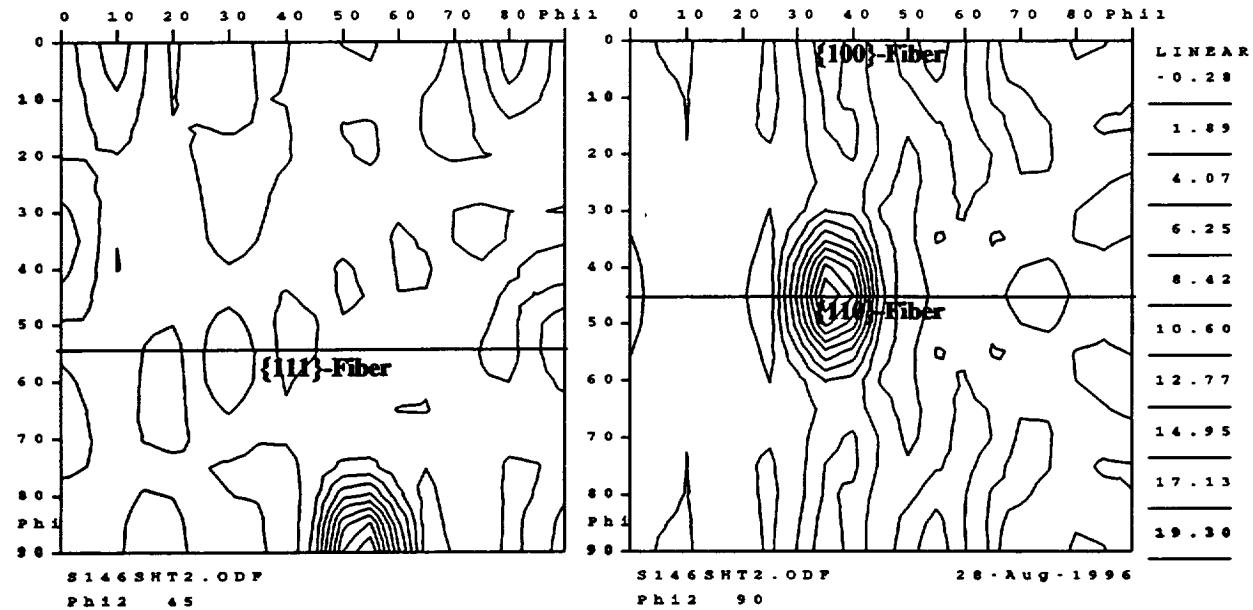


Figure 33. CODF sections for 1460-T3 sheet @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

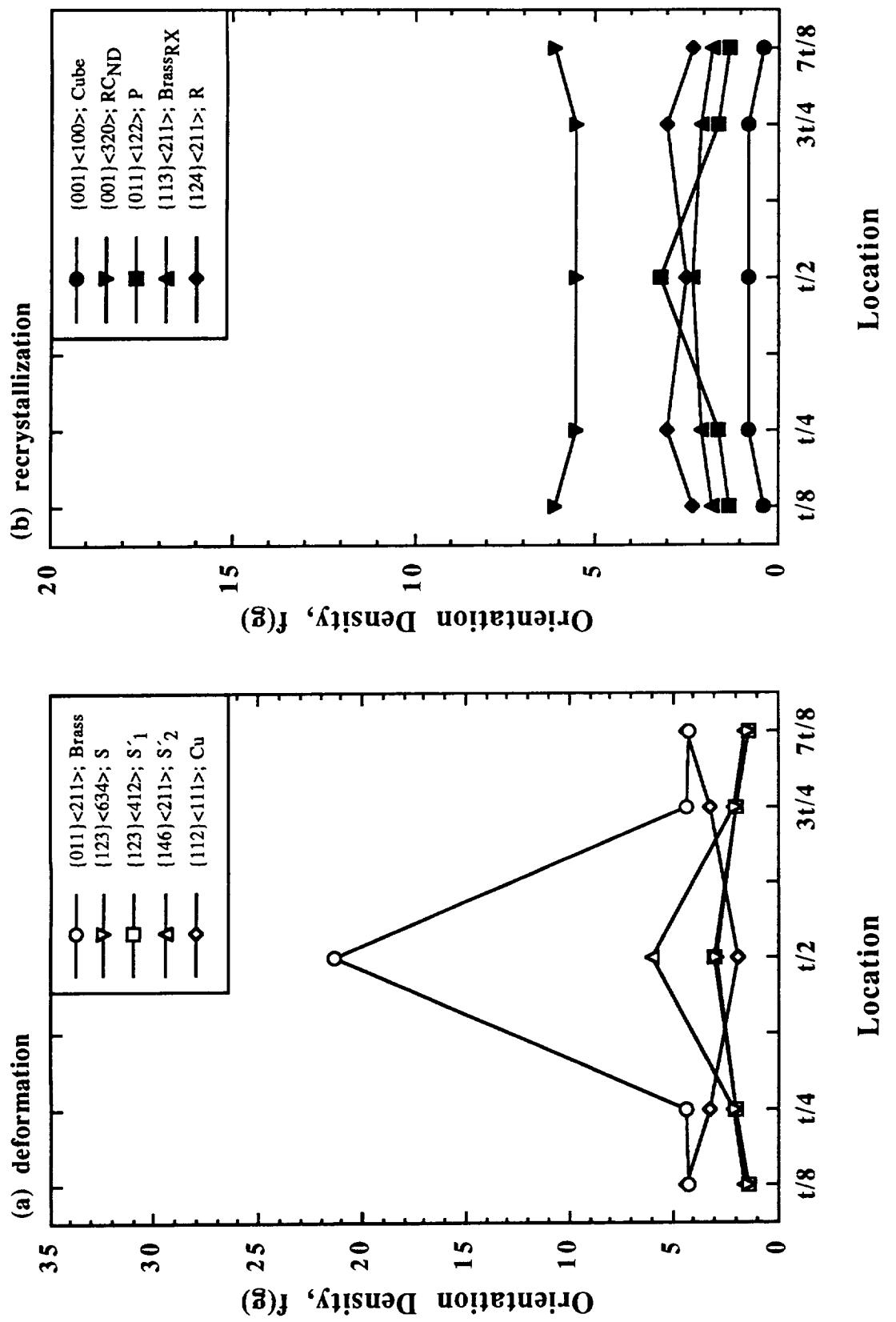


Figure 34. Orientation density, $f(g)$, as a function of location through the cross-section for the 1460-T3 sheet:
(a) Deformation-related components; (b) Recrystallization-related components.

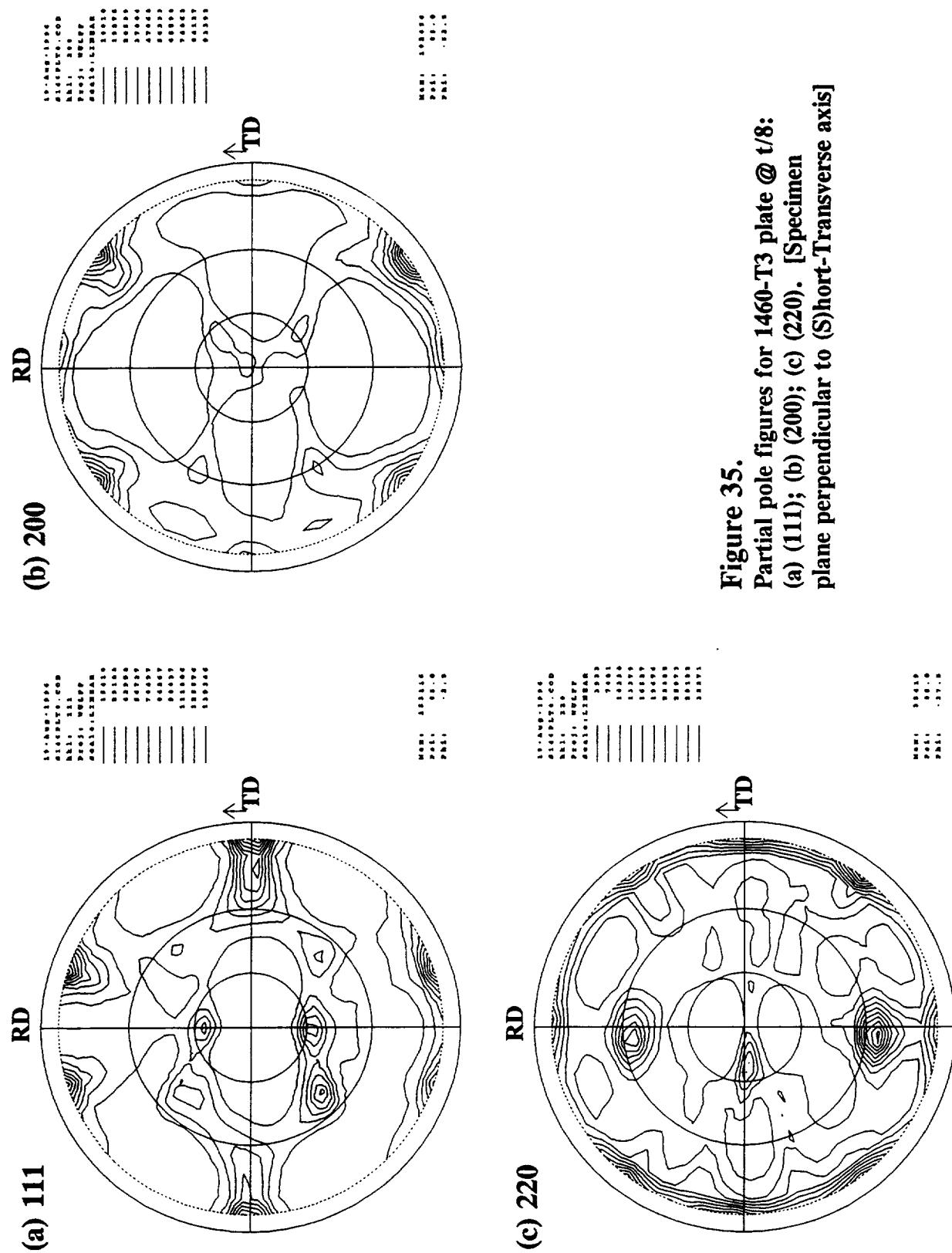
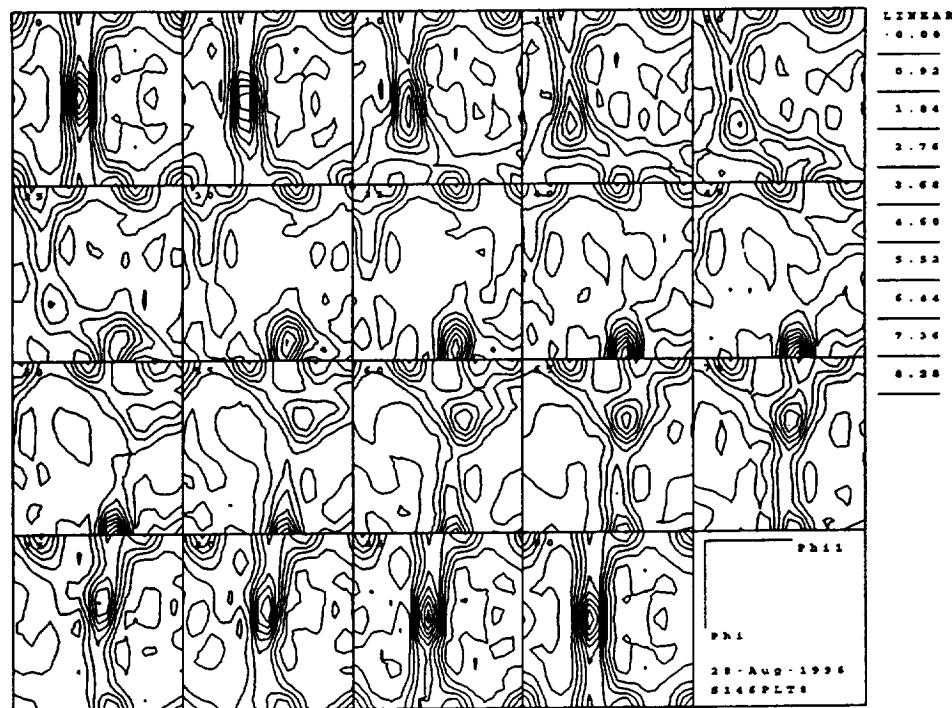


Figure 35.
Partial pole figures for 1460-T3 plate @ t/8:
(a) (111); (b) (200); (c) (220). [Specimen plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

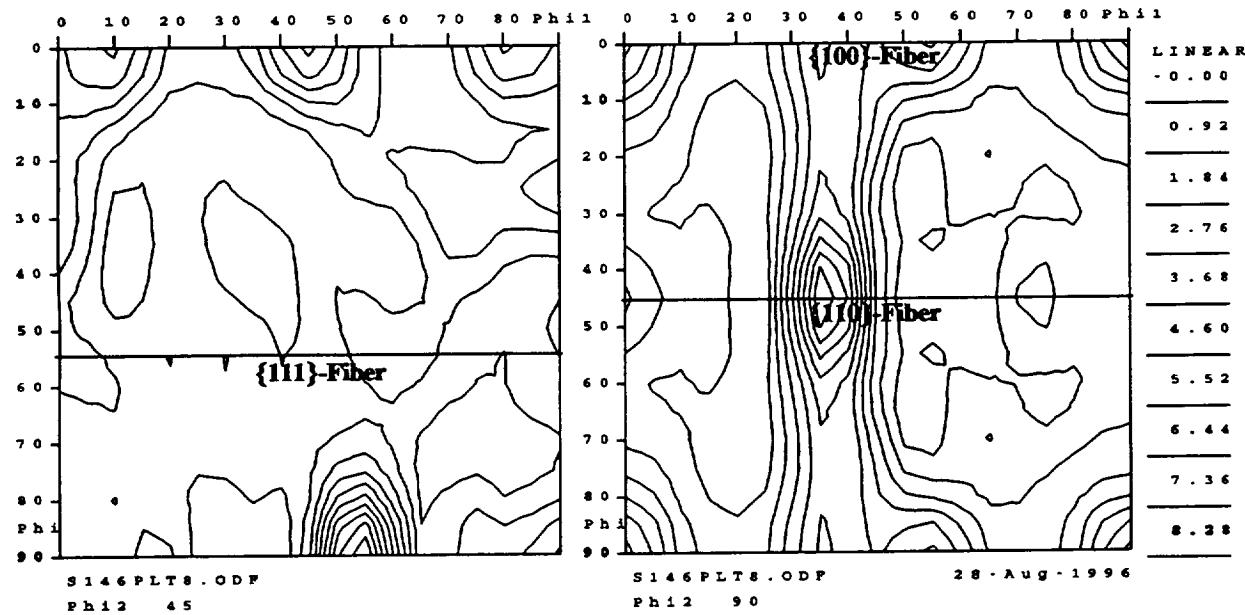


Figure 36. CODF sections for 1460-T3 plate @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.

[Specimen plane perpendicular to (S)hort-Transverse axis]

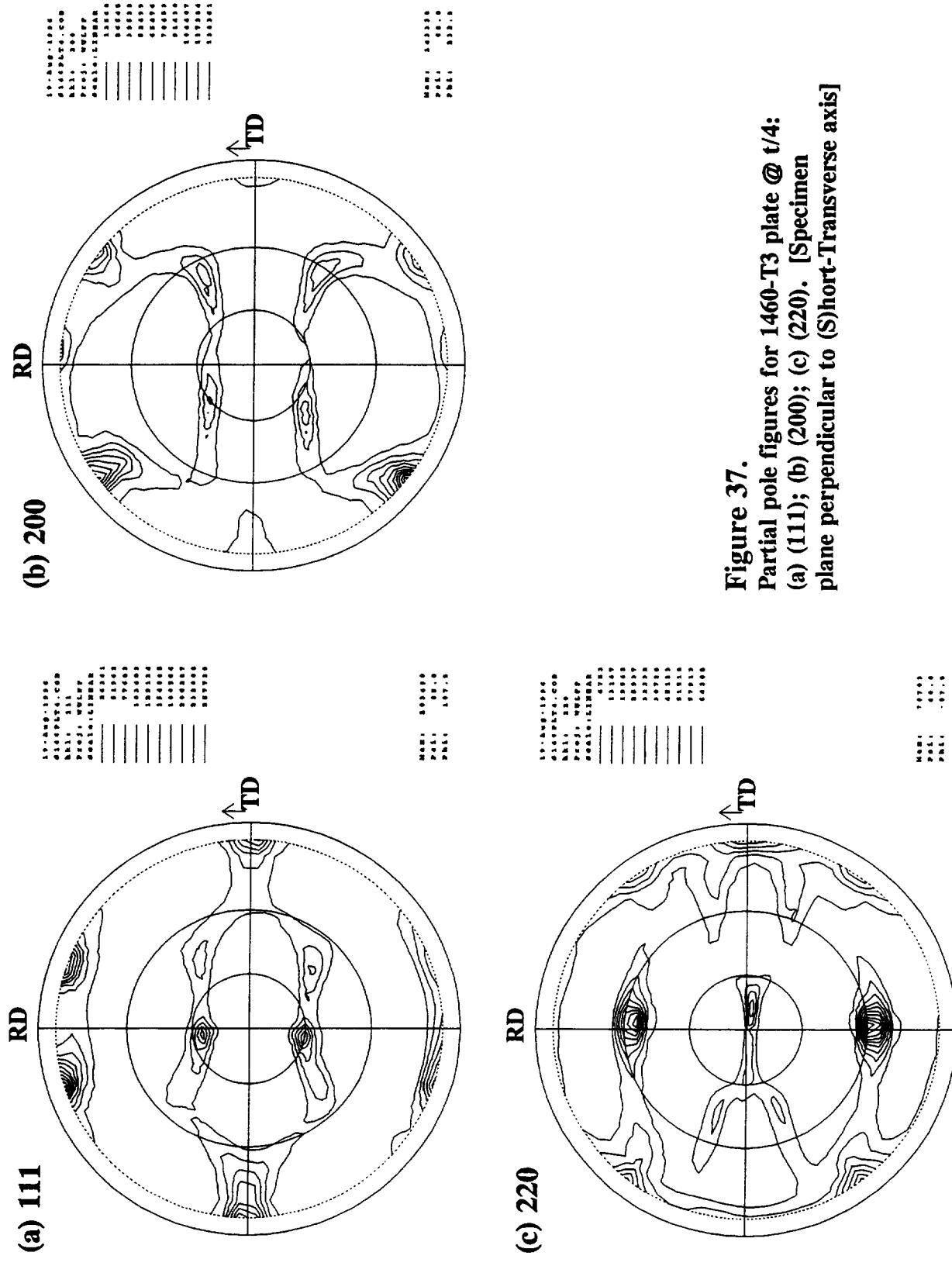
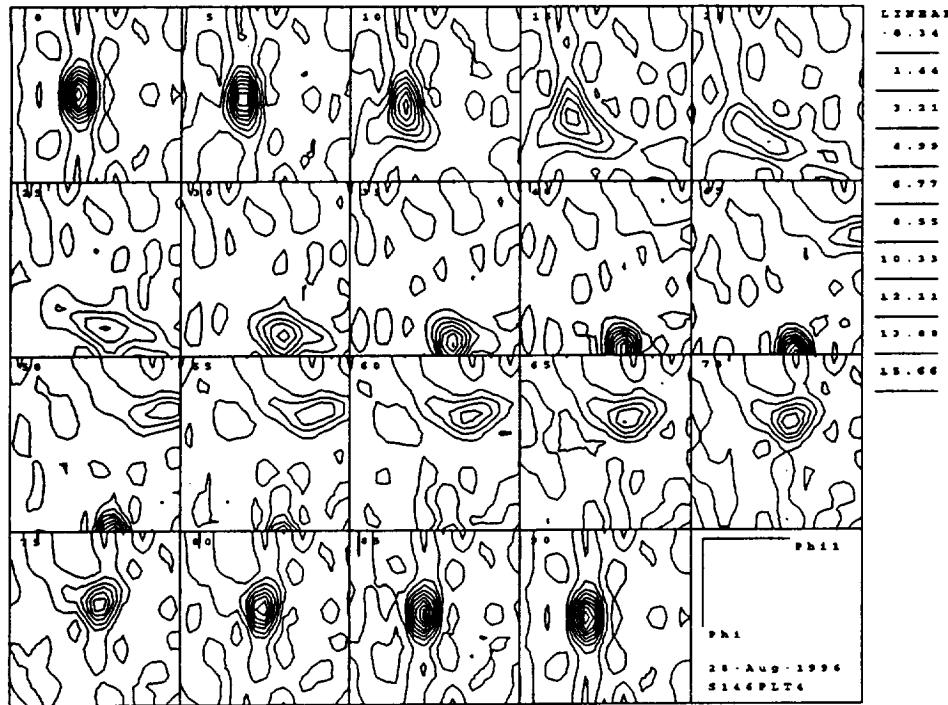


Figure 37.
Partial pole figures for 1460-T3 plate @ $t/4$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

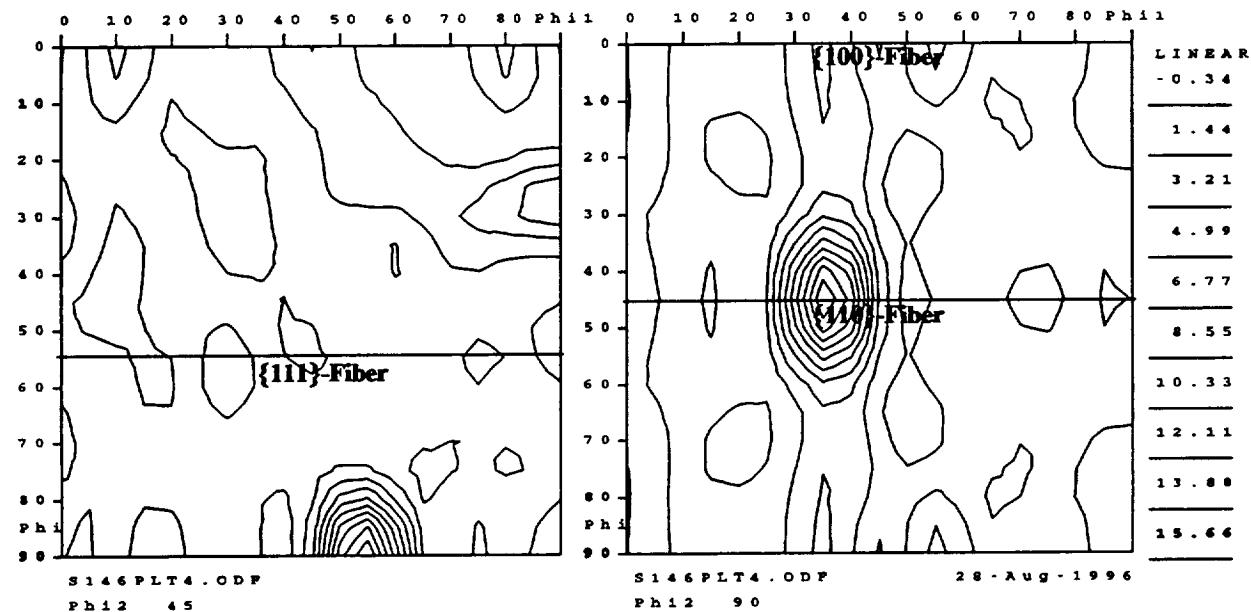


Figure 38. CODF sections for 1460-T3 plate @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

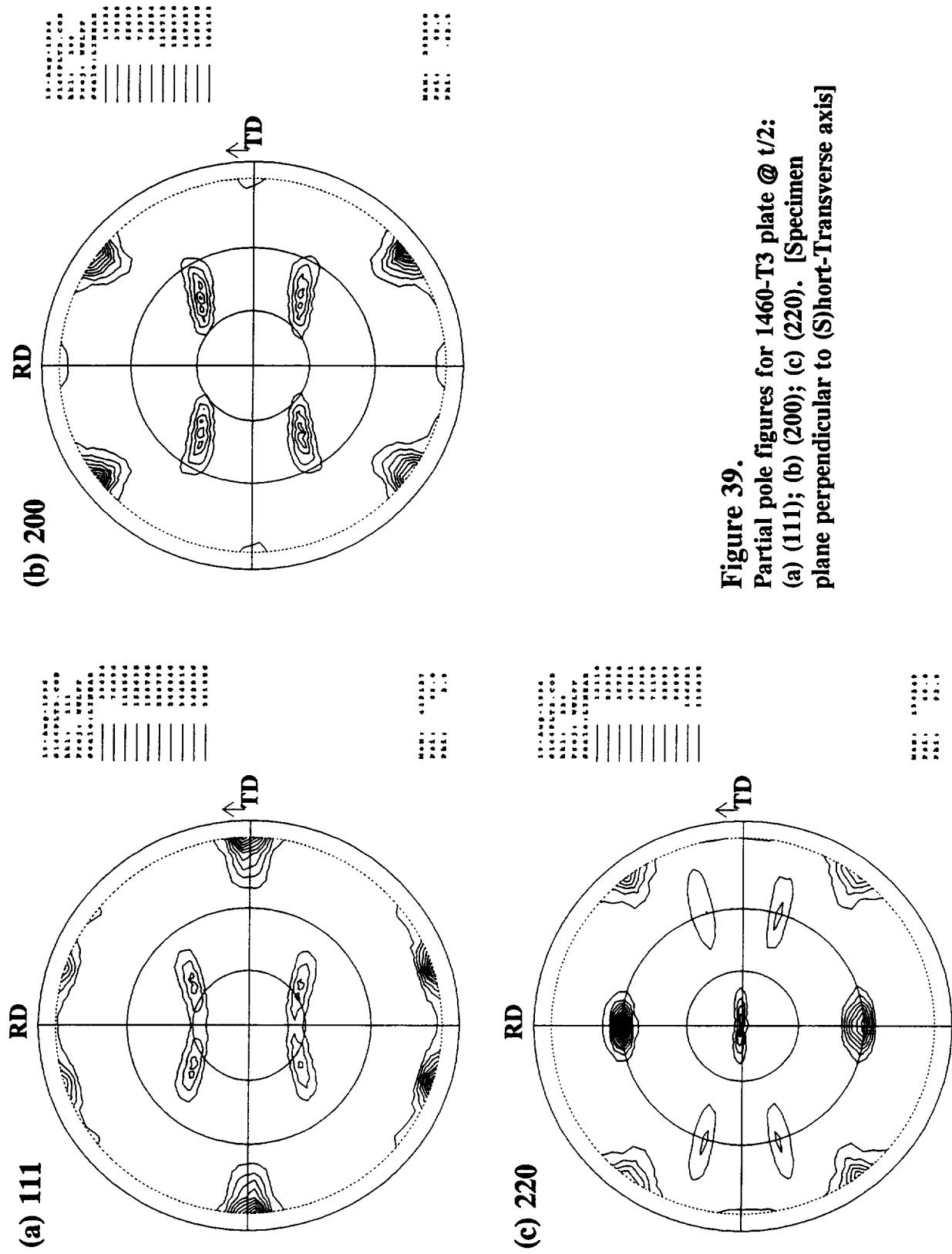
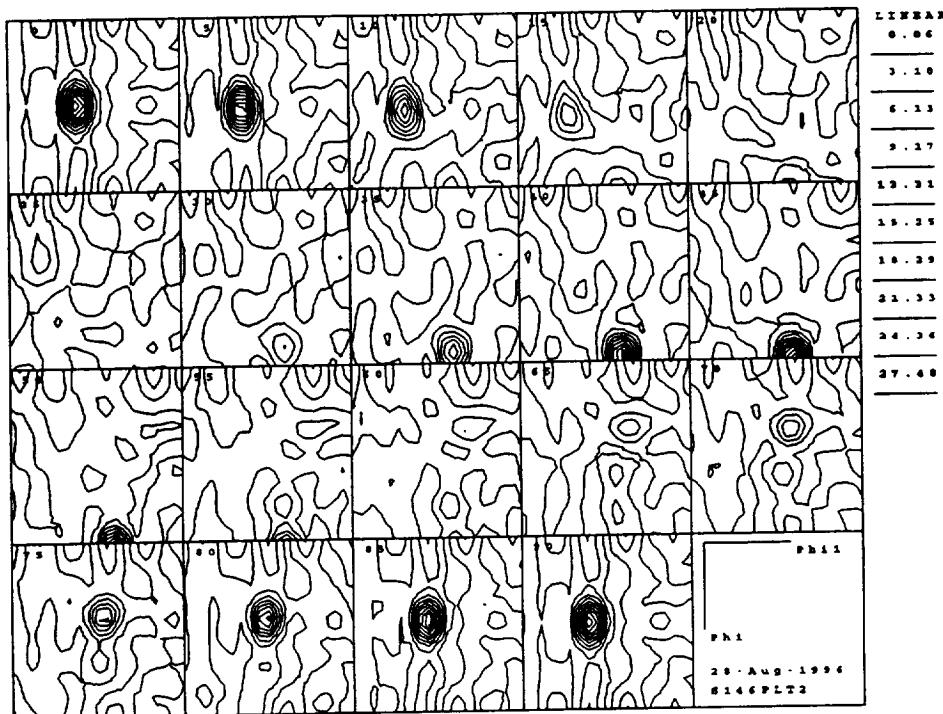


Figure 39.
Partial pole figures for 1460-T3 plate @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

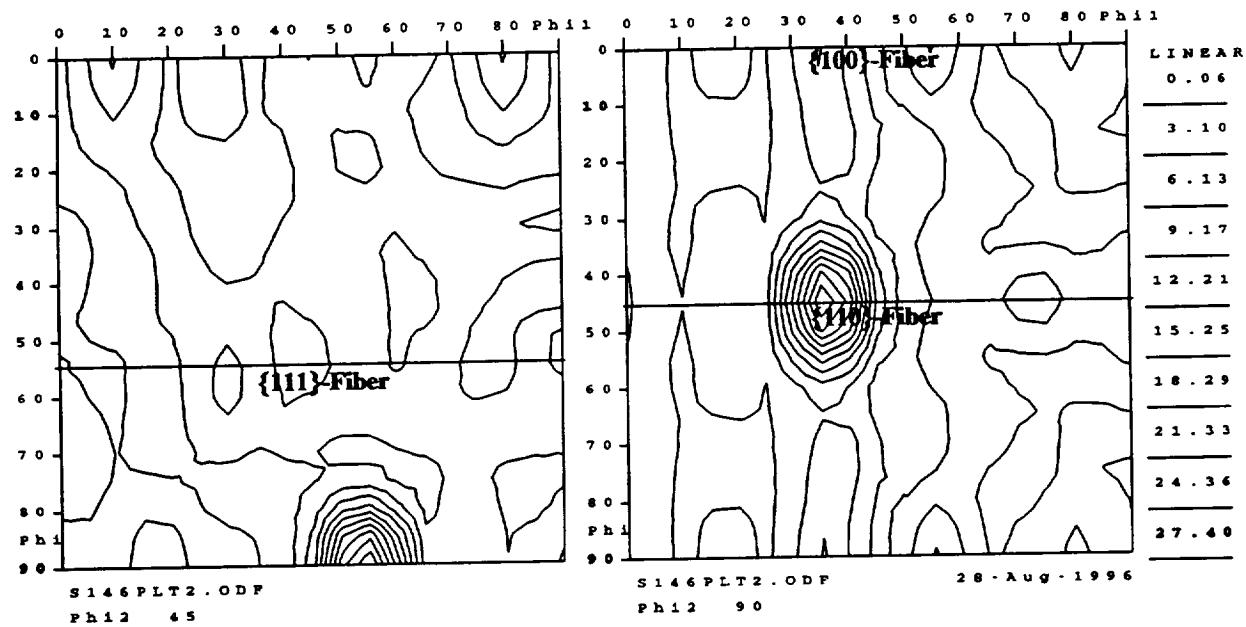


Figure 40. CODF sections for 1460-T3 plate @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

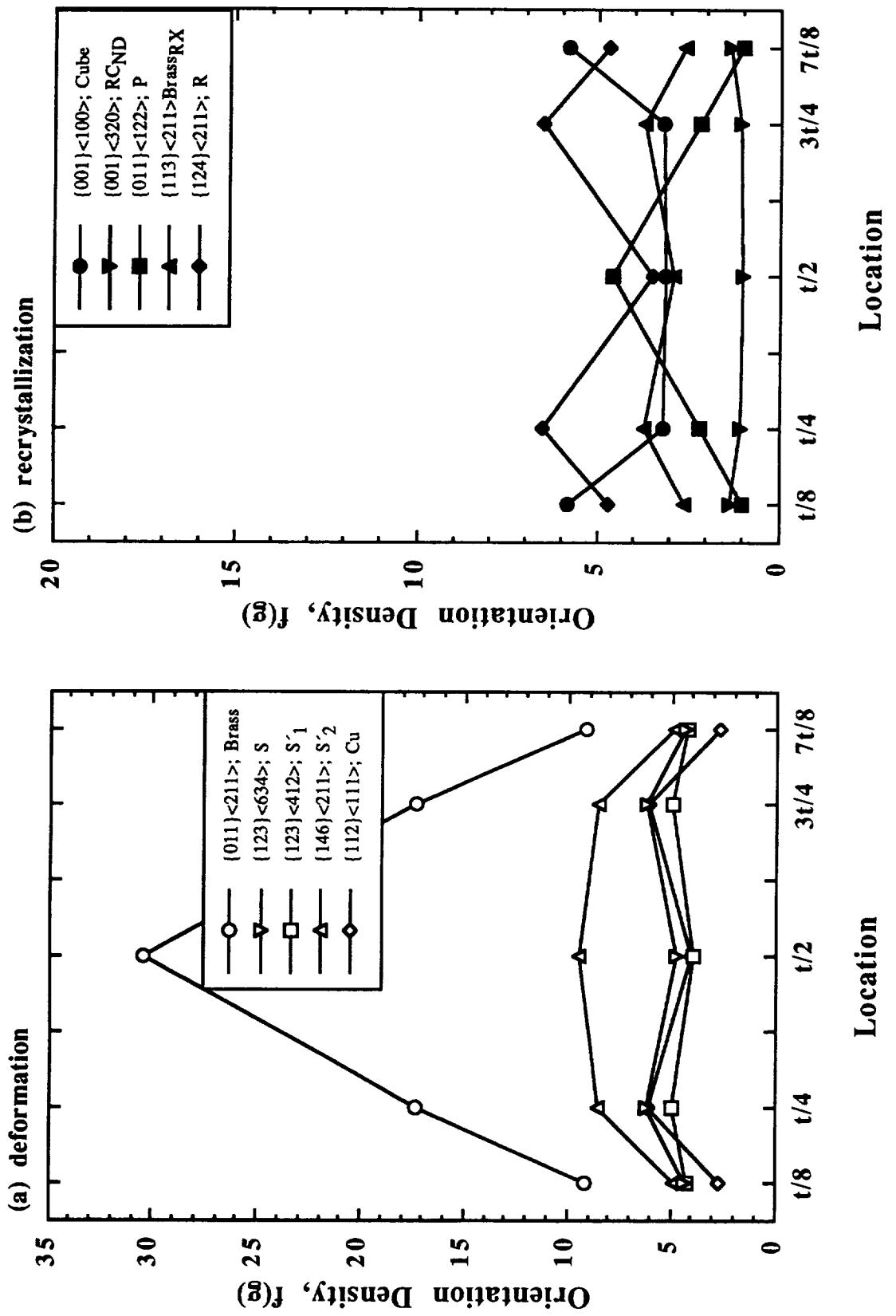


Figure 41. Orientation density, $f(g)$, as a function of location through the cross-section for the 1460-T3 plate:
 (a) Deformation-related components; (b) Recrystallization-related components.

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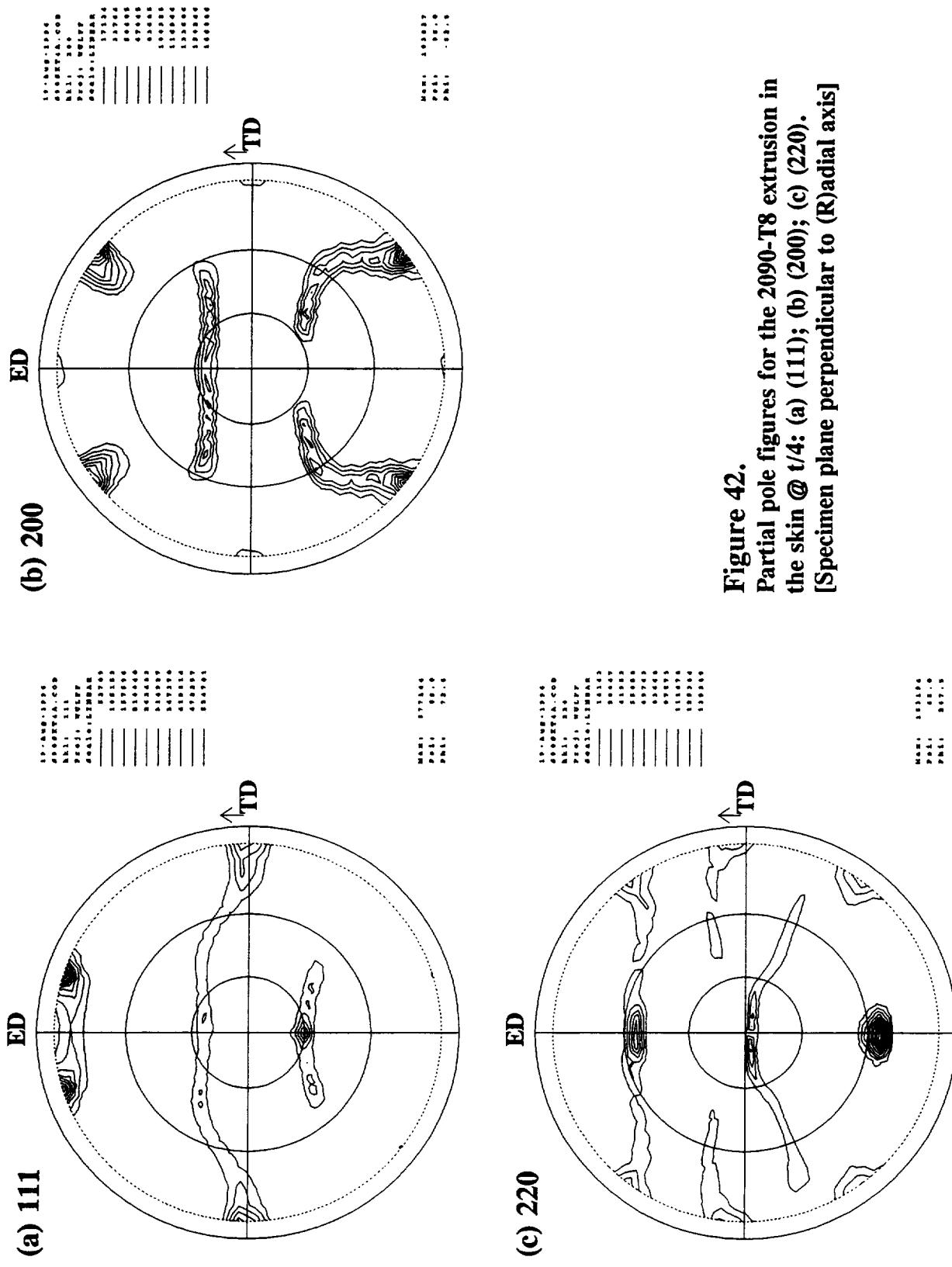
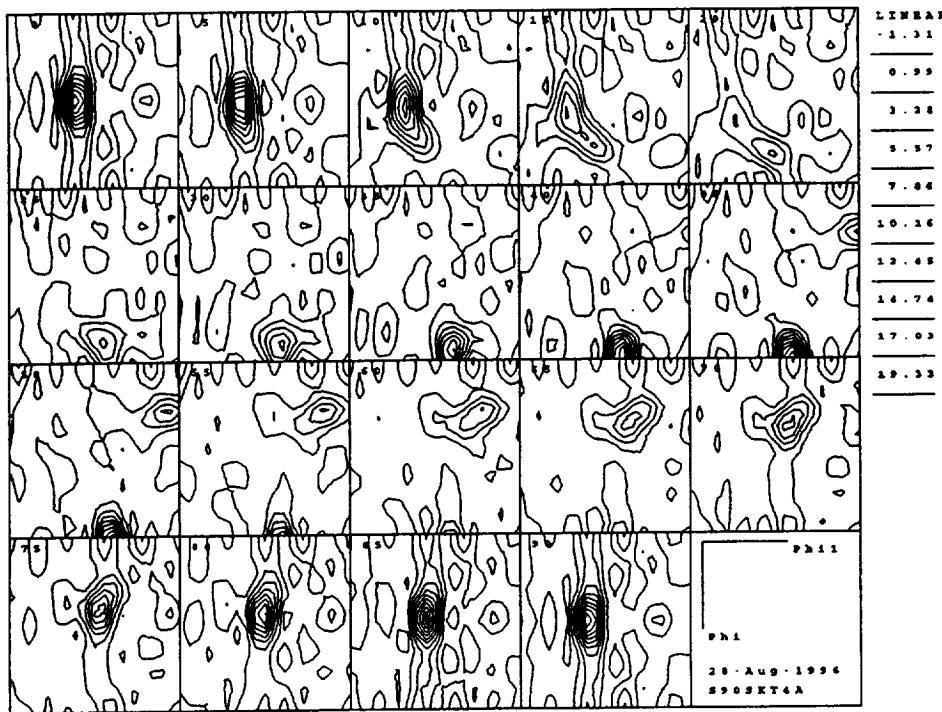


Figure 42.
Partial pole figures for the 2090-T8 extrusion in
the skin @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

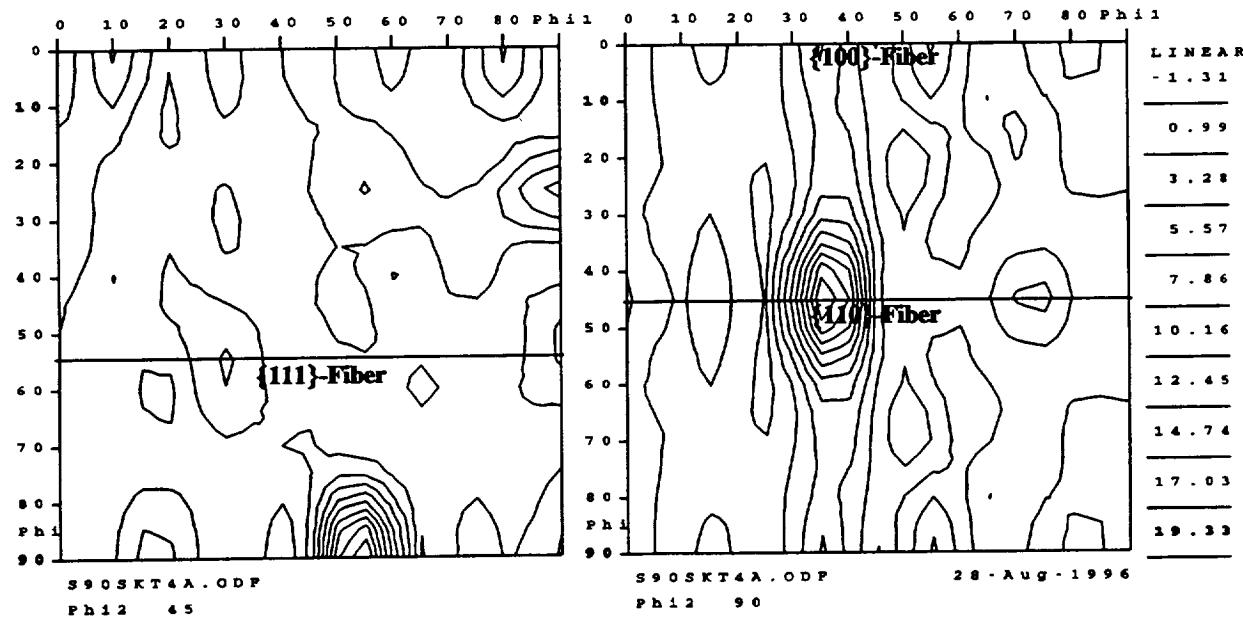


Figure 43. CODF sections for the 2090-T8 extrusion in the skin @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

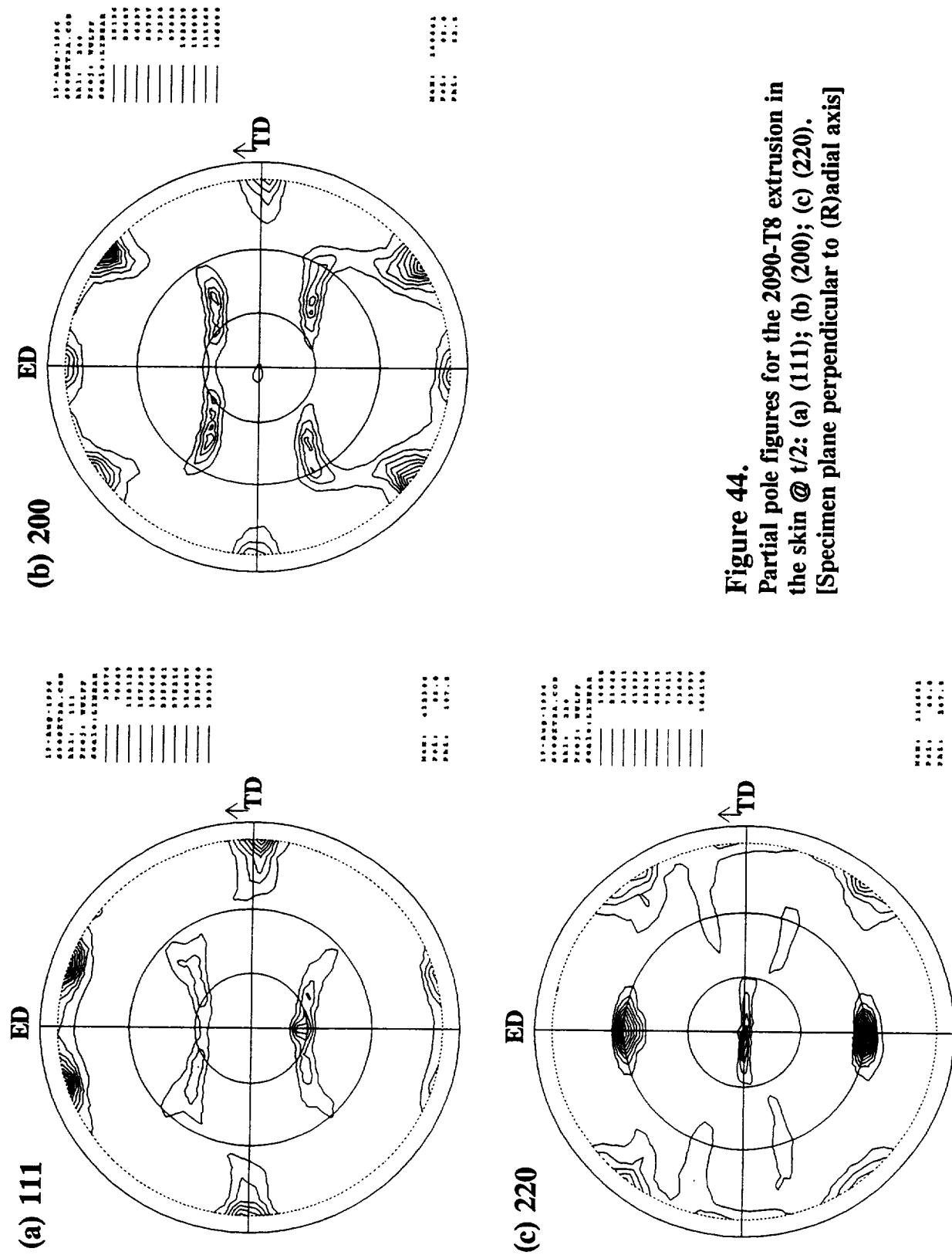
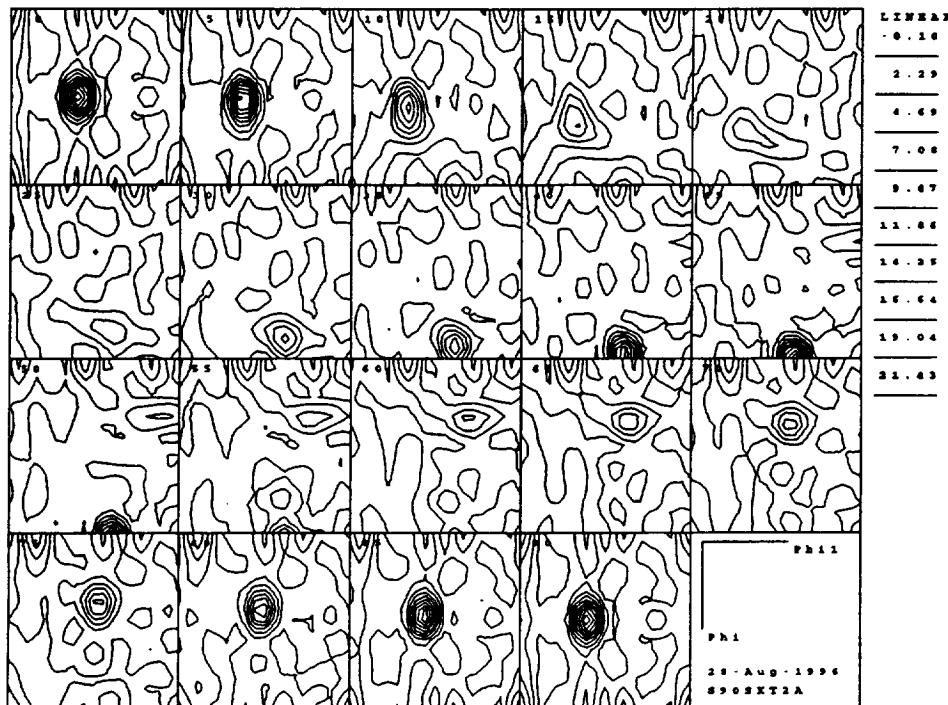


Figure 44.
Partial pole figures for the 2090-T8 extrusion in
the skin @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

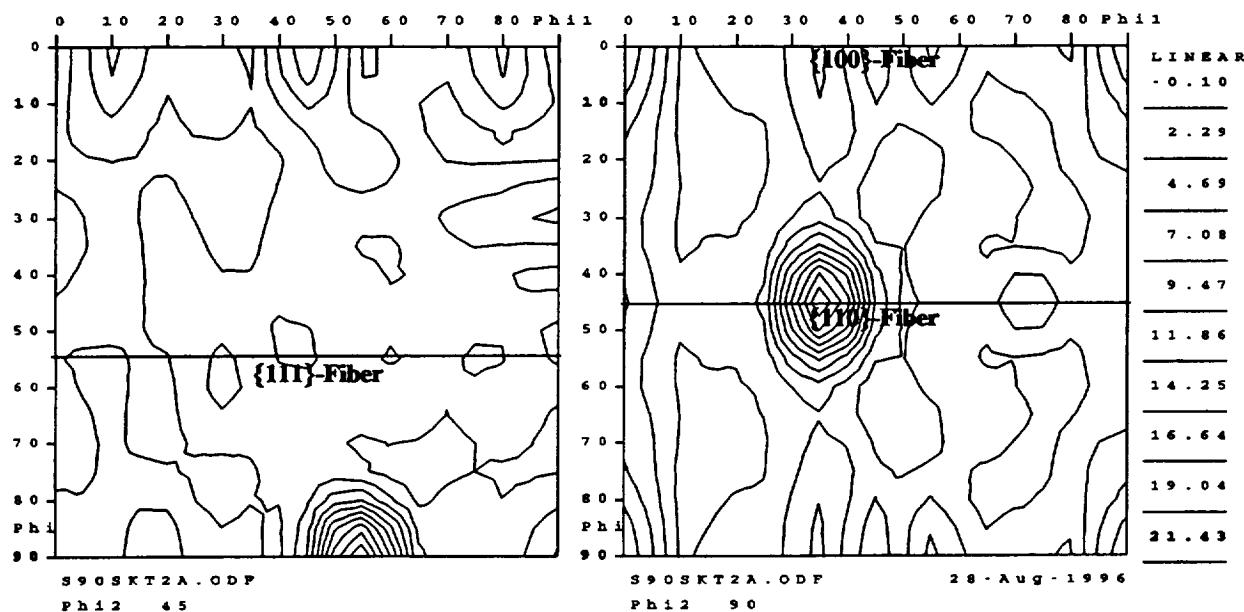


Figure 45. CODF sections for the 2090-T8 extrusion in the skin @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

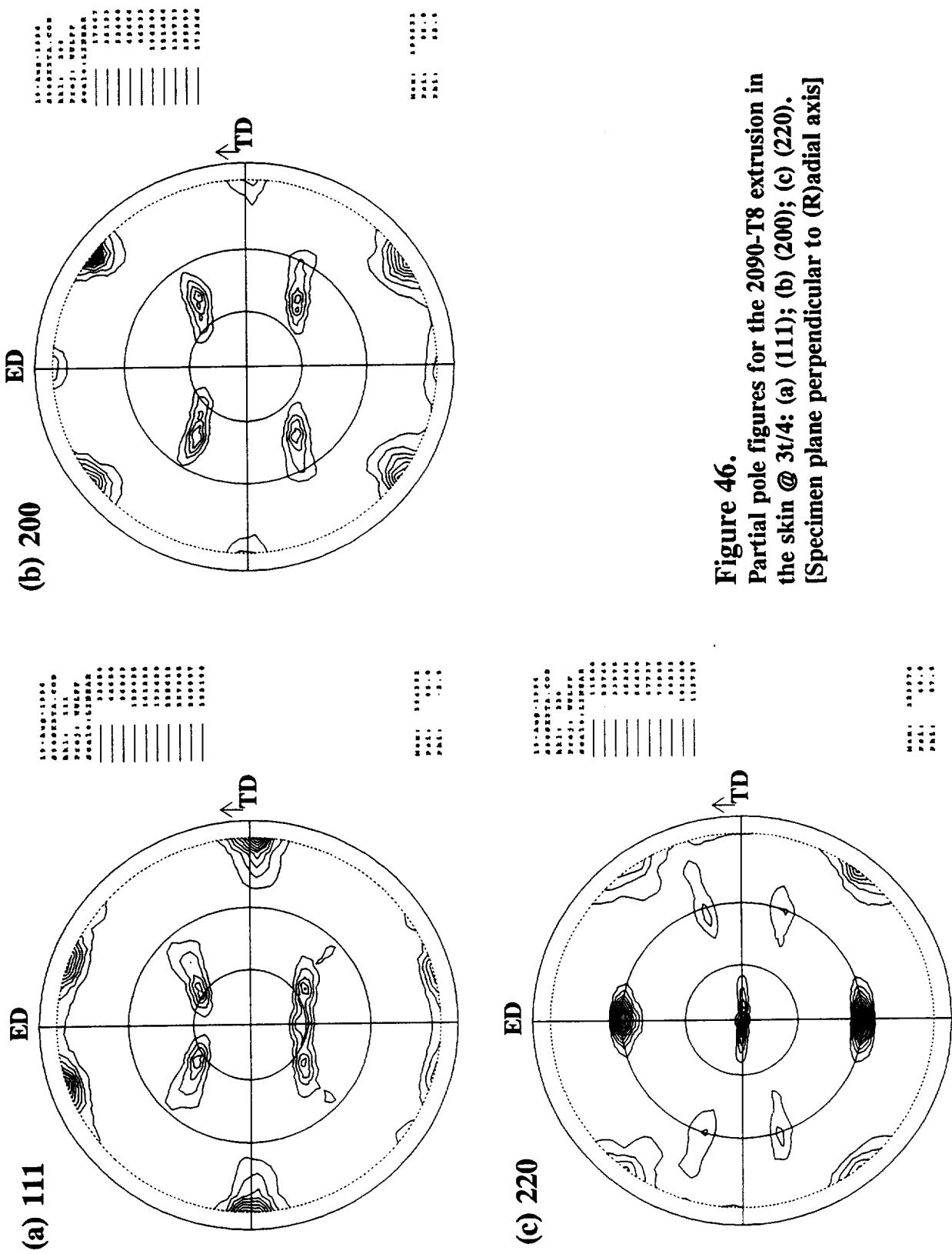
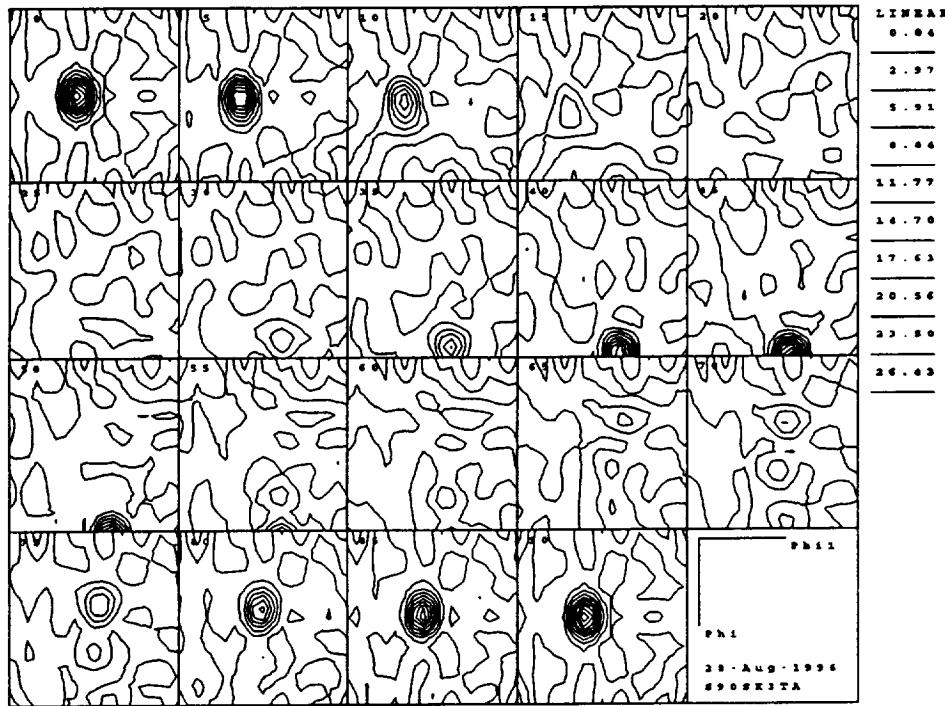


Figure 46.
Partial pole figures for the 2090-T8 extrusion in
the skin @ 3T/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

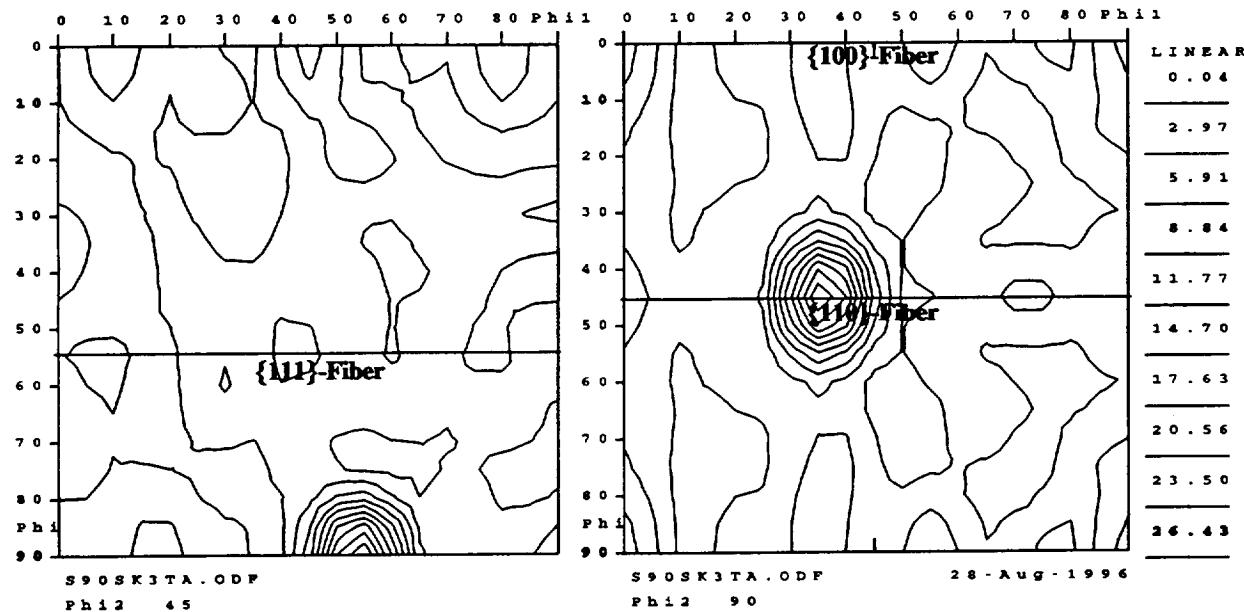


Figure 47. CODF sections for the 2090-T8 extrusion in the skin @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

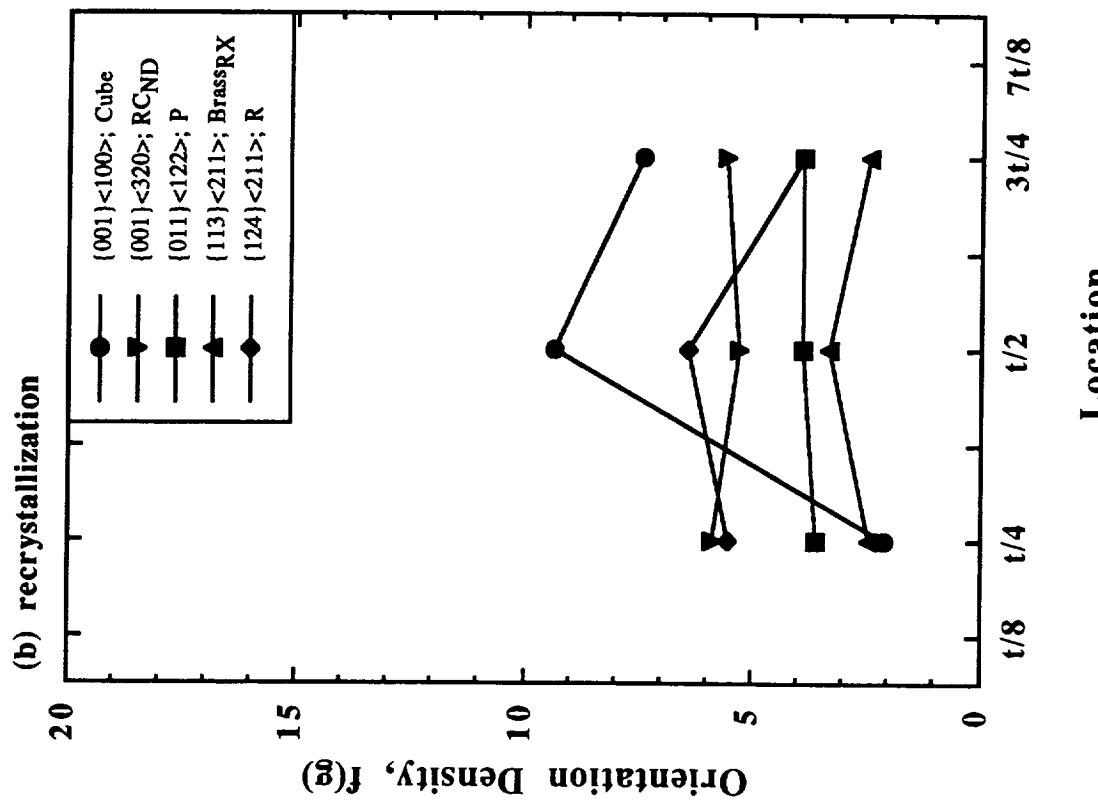
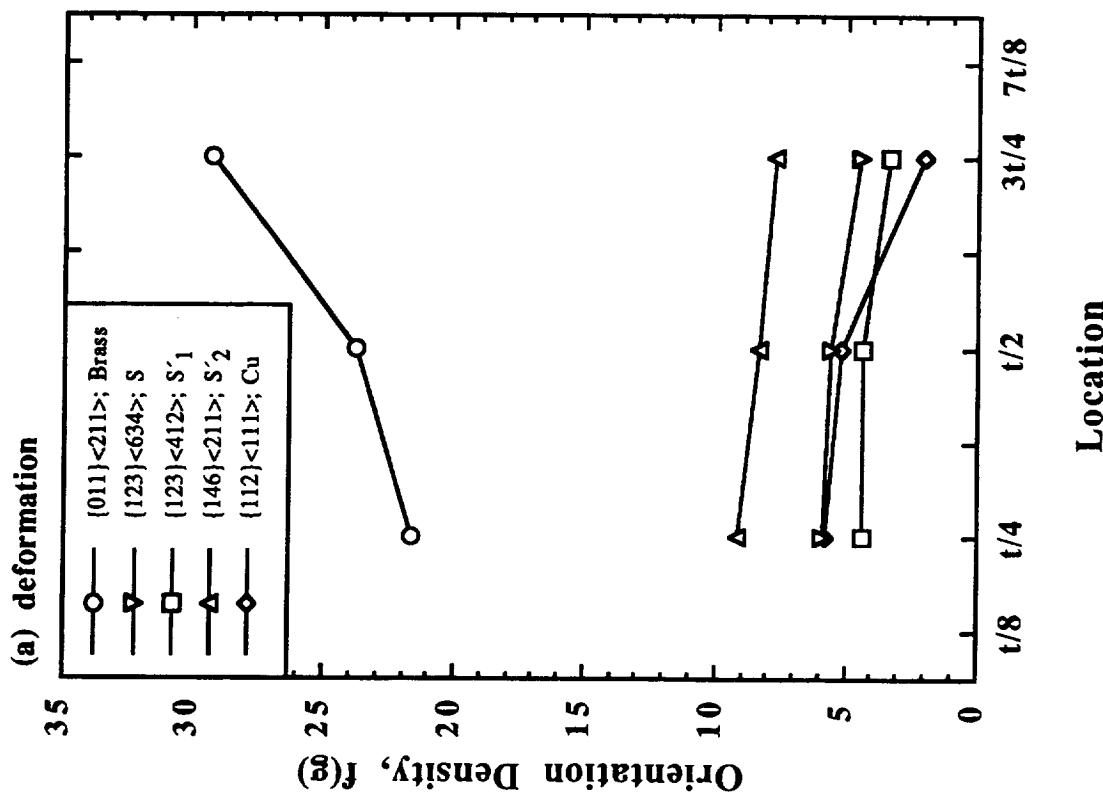


Figure 48. Orientation density, $f(g)$, as a function of location through the cross-section for the 2090-T8 extrusion in the skin region: (a) Deformation-related components; (b) Recrystallization-related components.

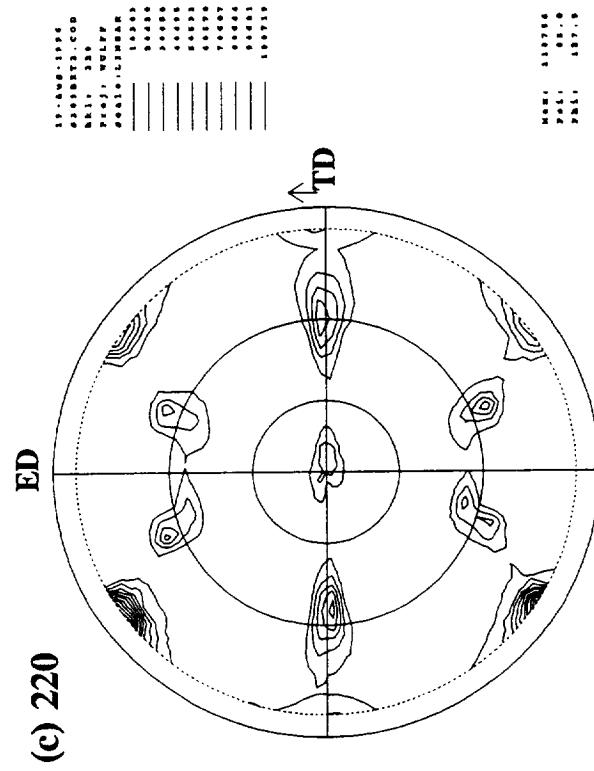
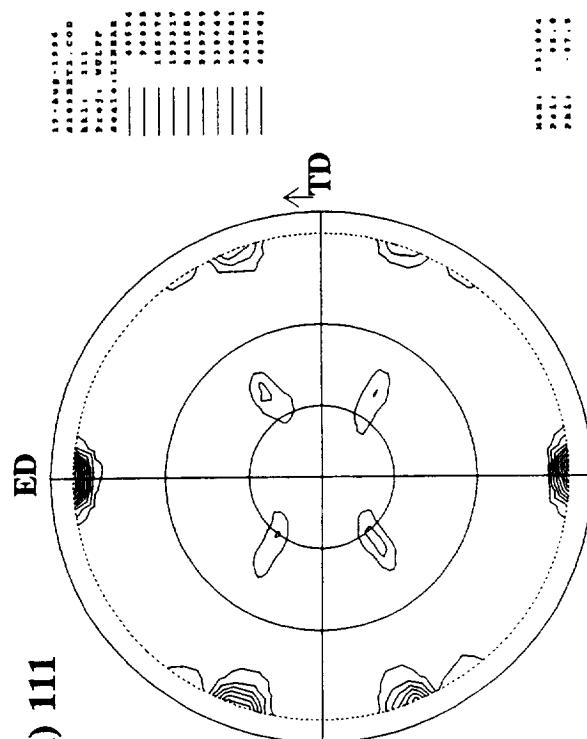
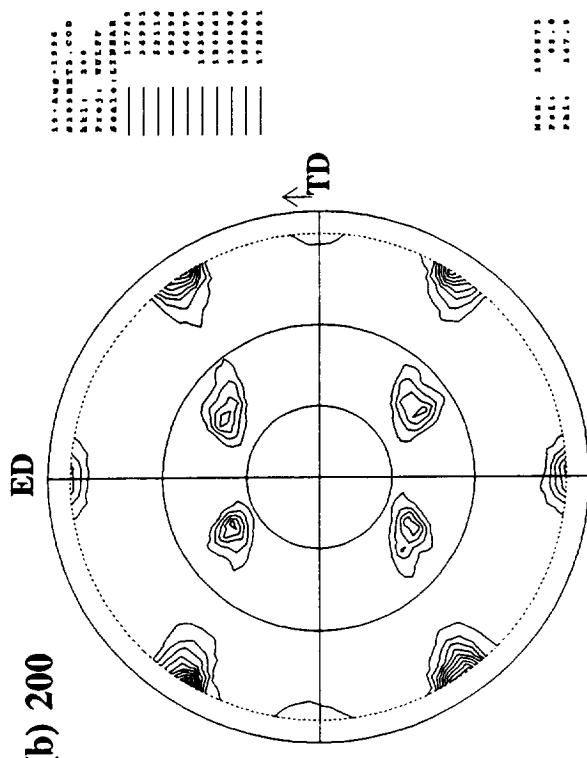
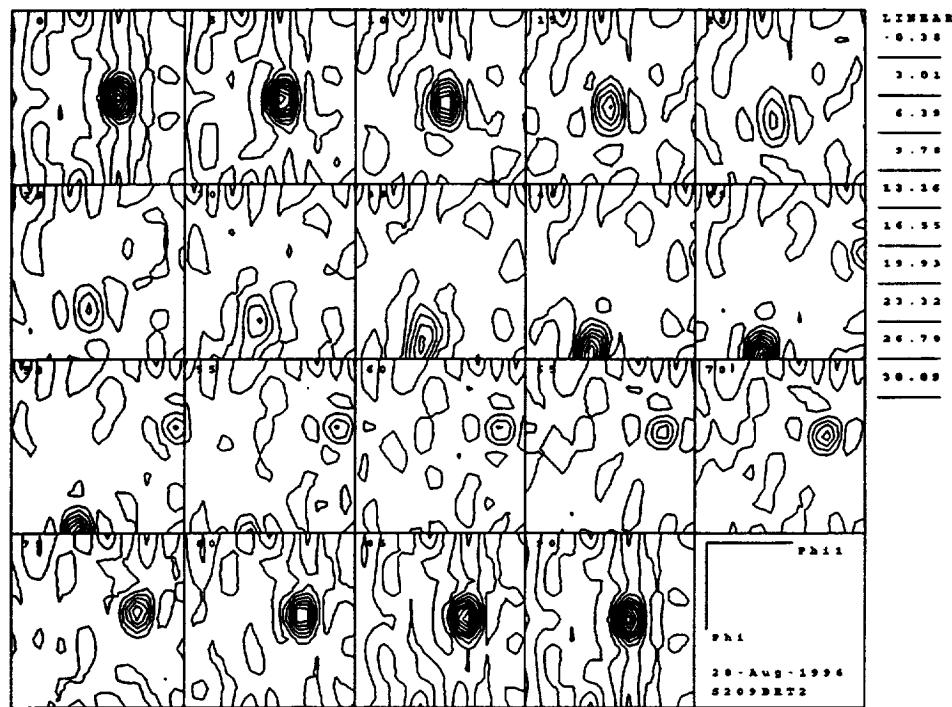


Figure 49.
Partial pole figures for the 2090-T8 extrusion in
the base @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

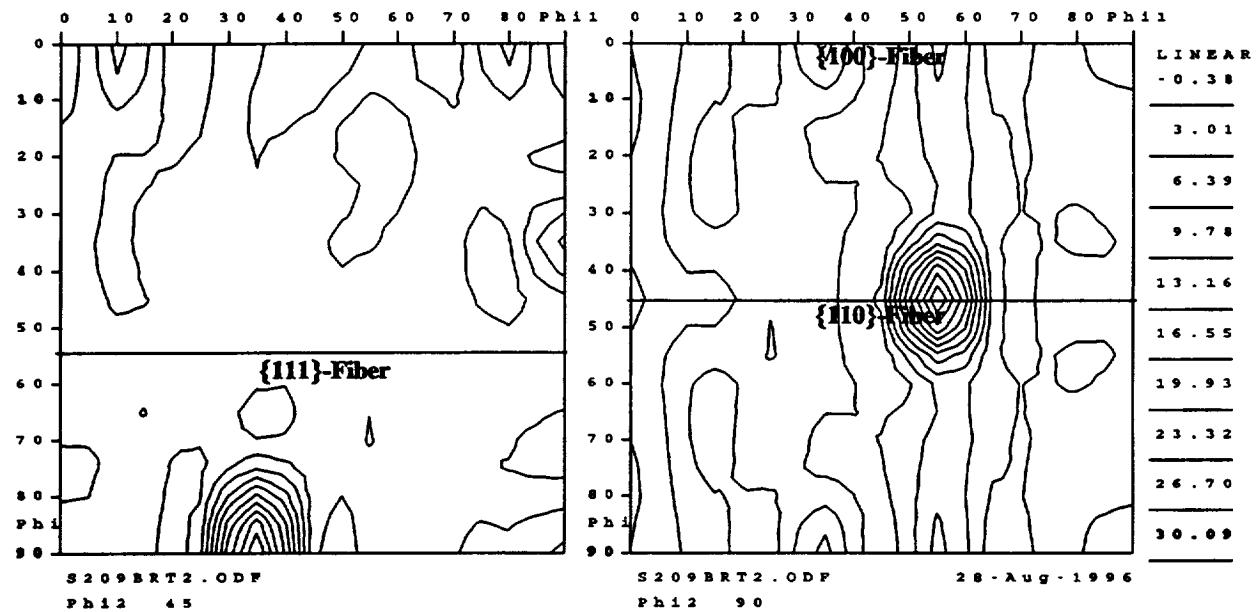
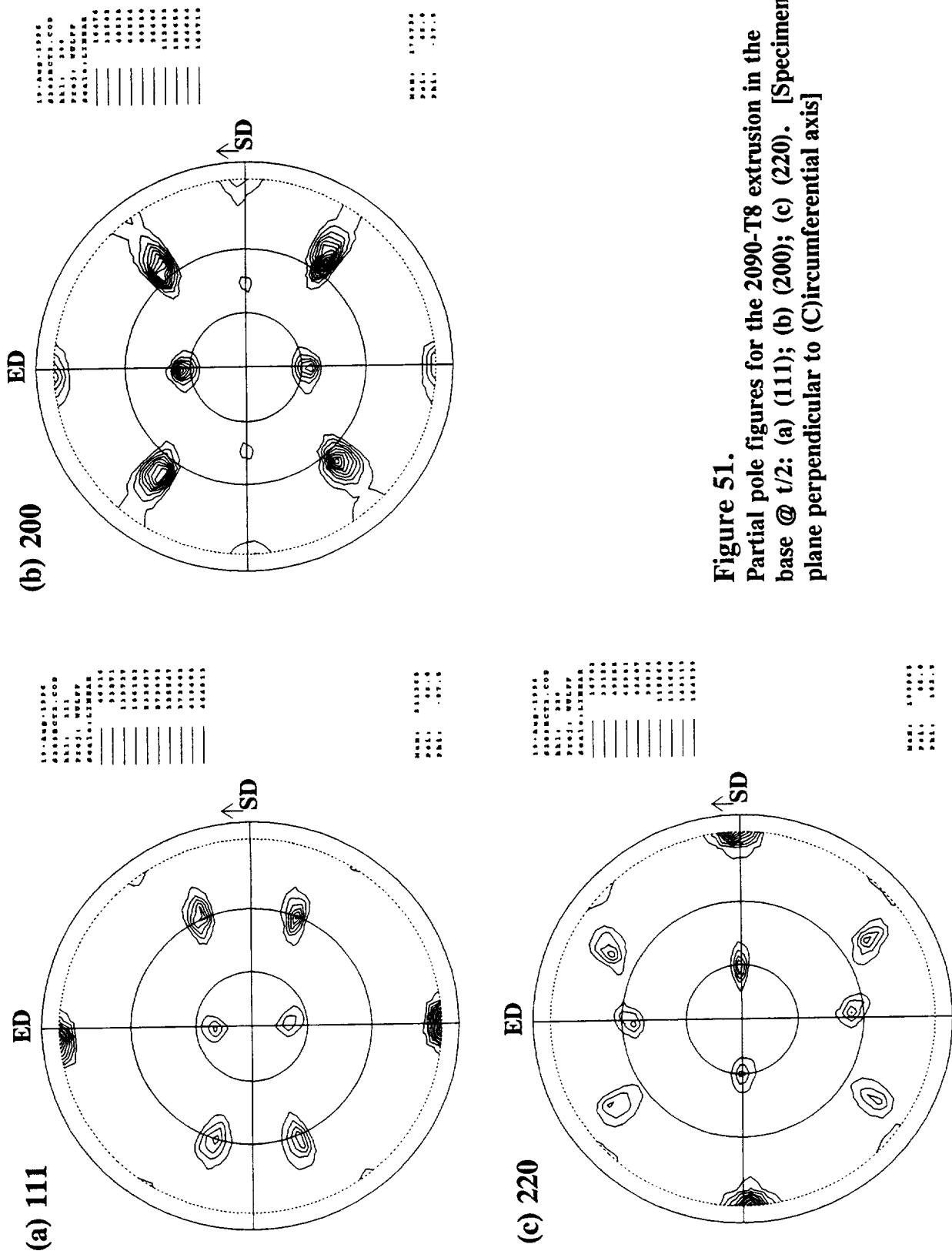
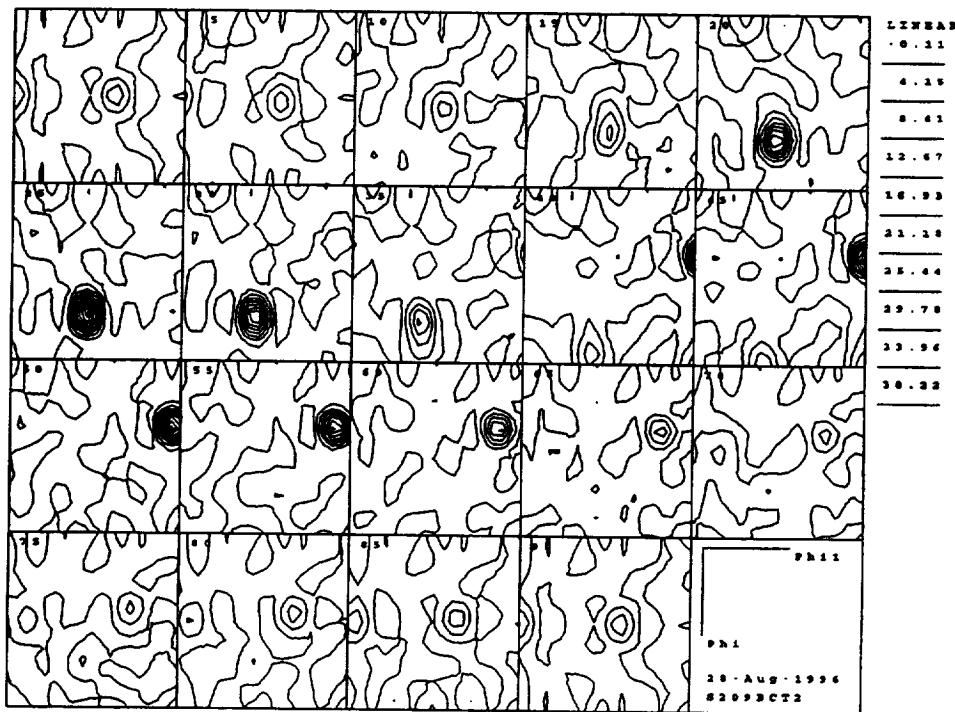


Figure 50. CODF sections for the 2090-T8 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

Figure 51.
Partial pole figures for the 2090-T8 extrusion in the
base @ t/2: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]



(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

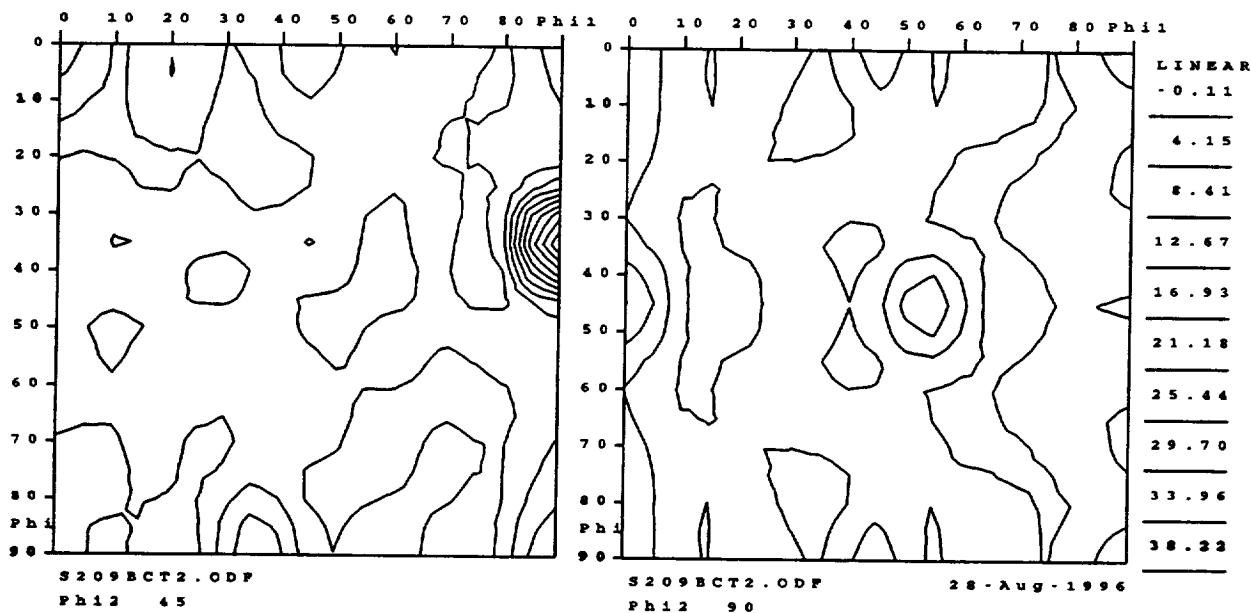


Figure 52. CODF sections for the 2090-T8 extrusion in the base @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. [Specimen plane perpendicular to (C)ircumferential axis]

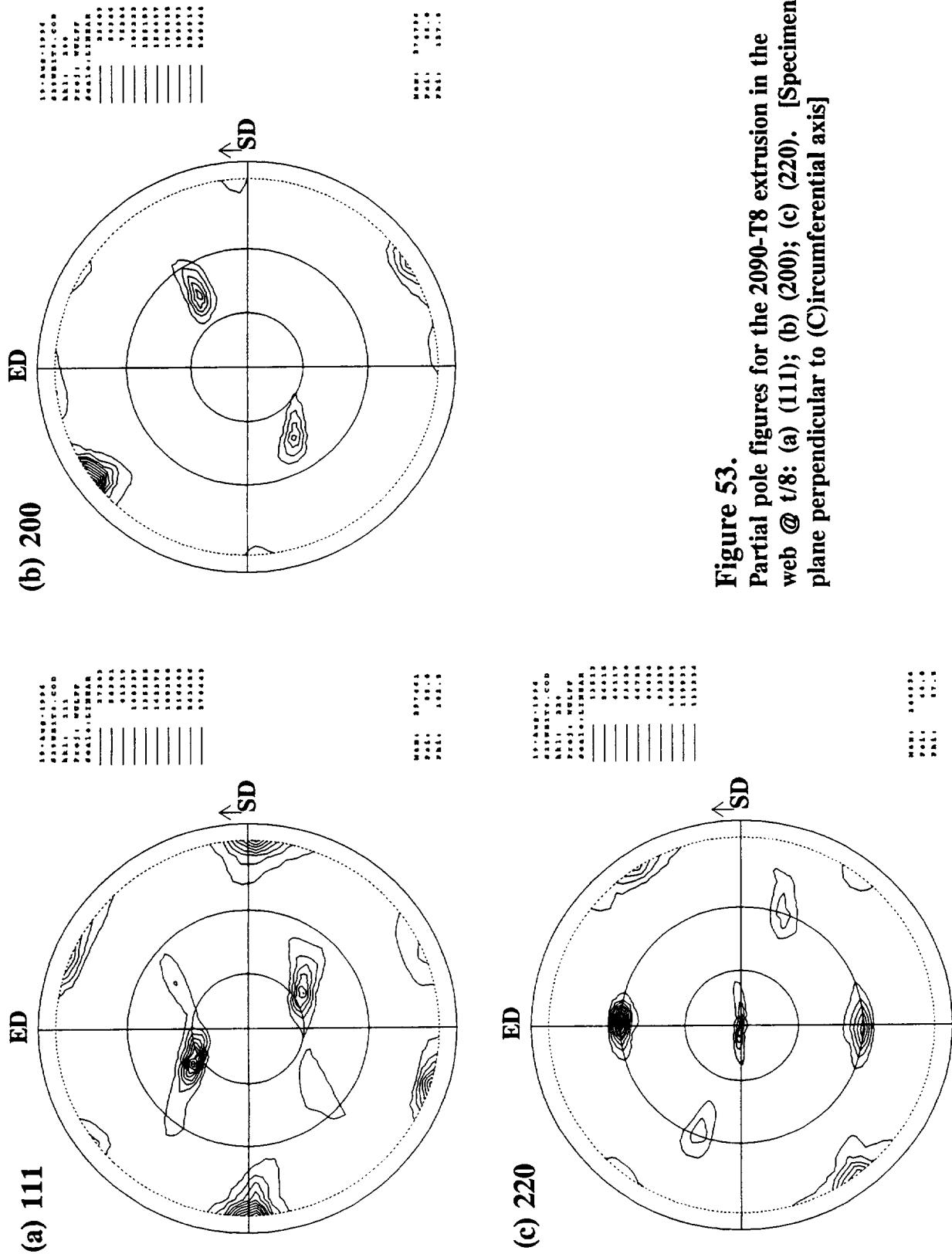
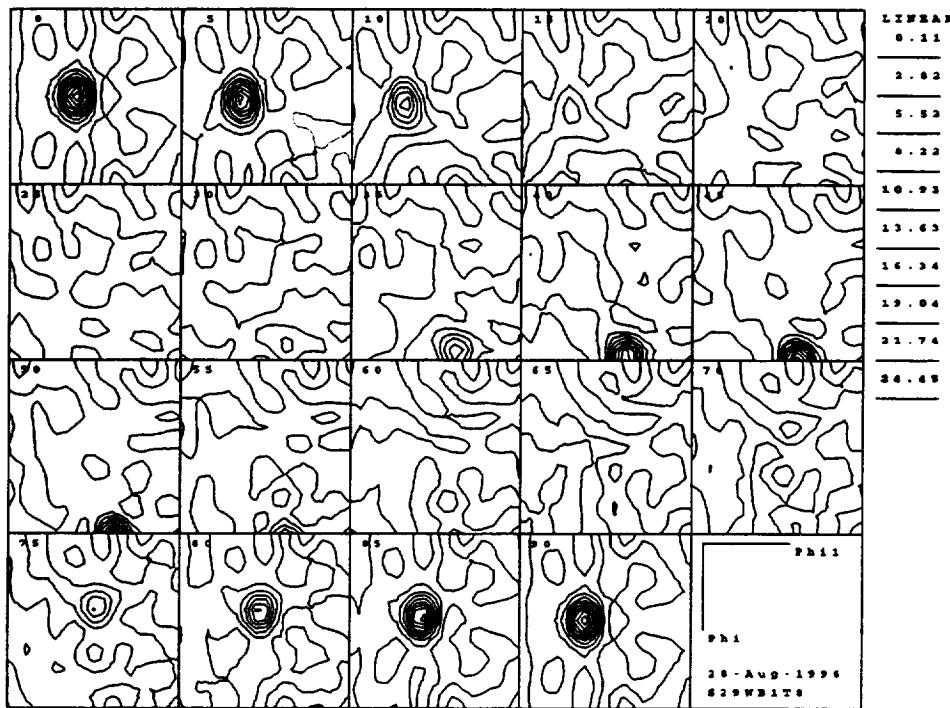


Figure 53.
Partial pole figures for the 2090-T8 extrusion in the
web @ t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

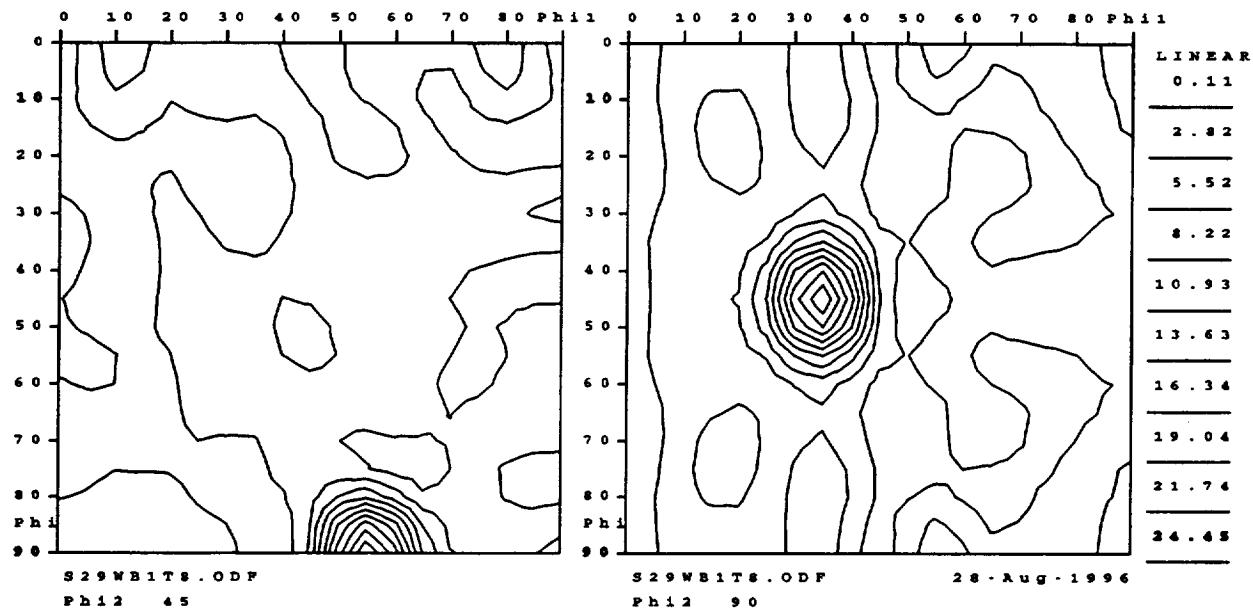


Figure 54. CODF sections for the 2090-T8 extrusion in the web @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. [Specimen plane perpendicular to (C)ircumferential axis]

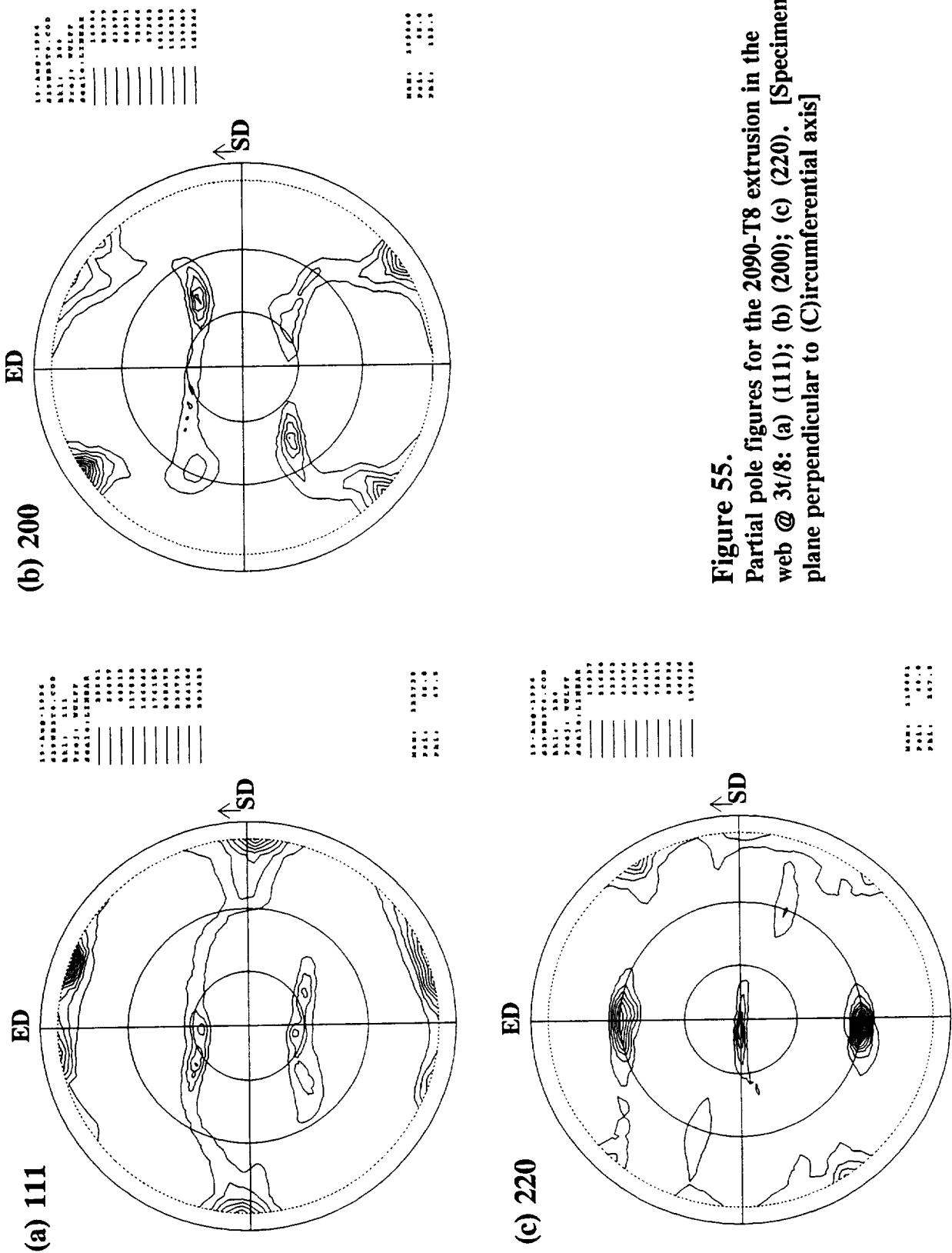
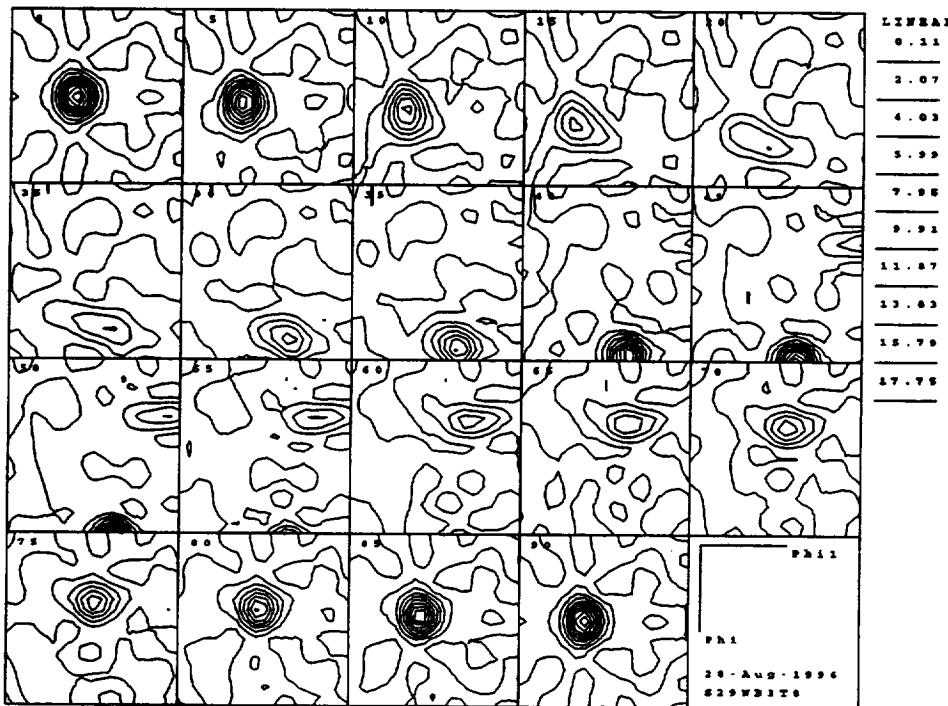


Figure 55.
Partial pole figures for the 2090-T8 extrusion in the
web @ 3t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

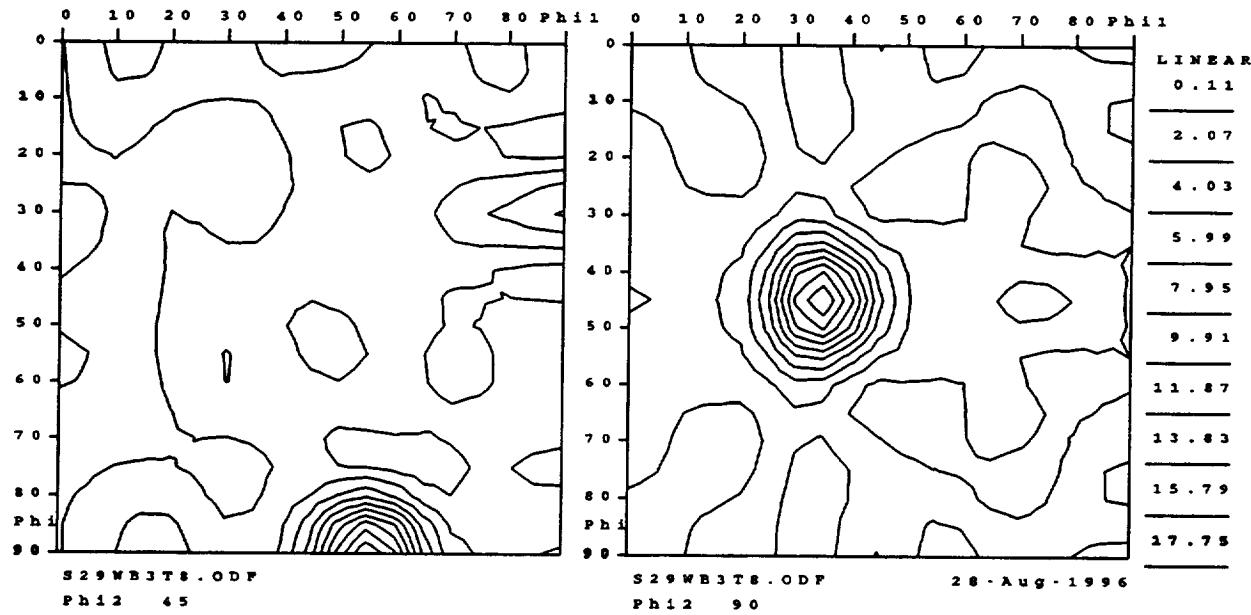


Figure 56. CODF sections for the 2090-T8 extrusion in the web @ 3t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. [Specimen plane perpendicular to (C)ircumferential axis]

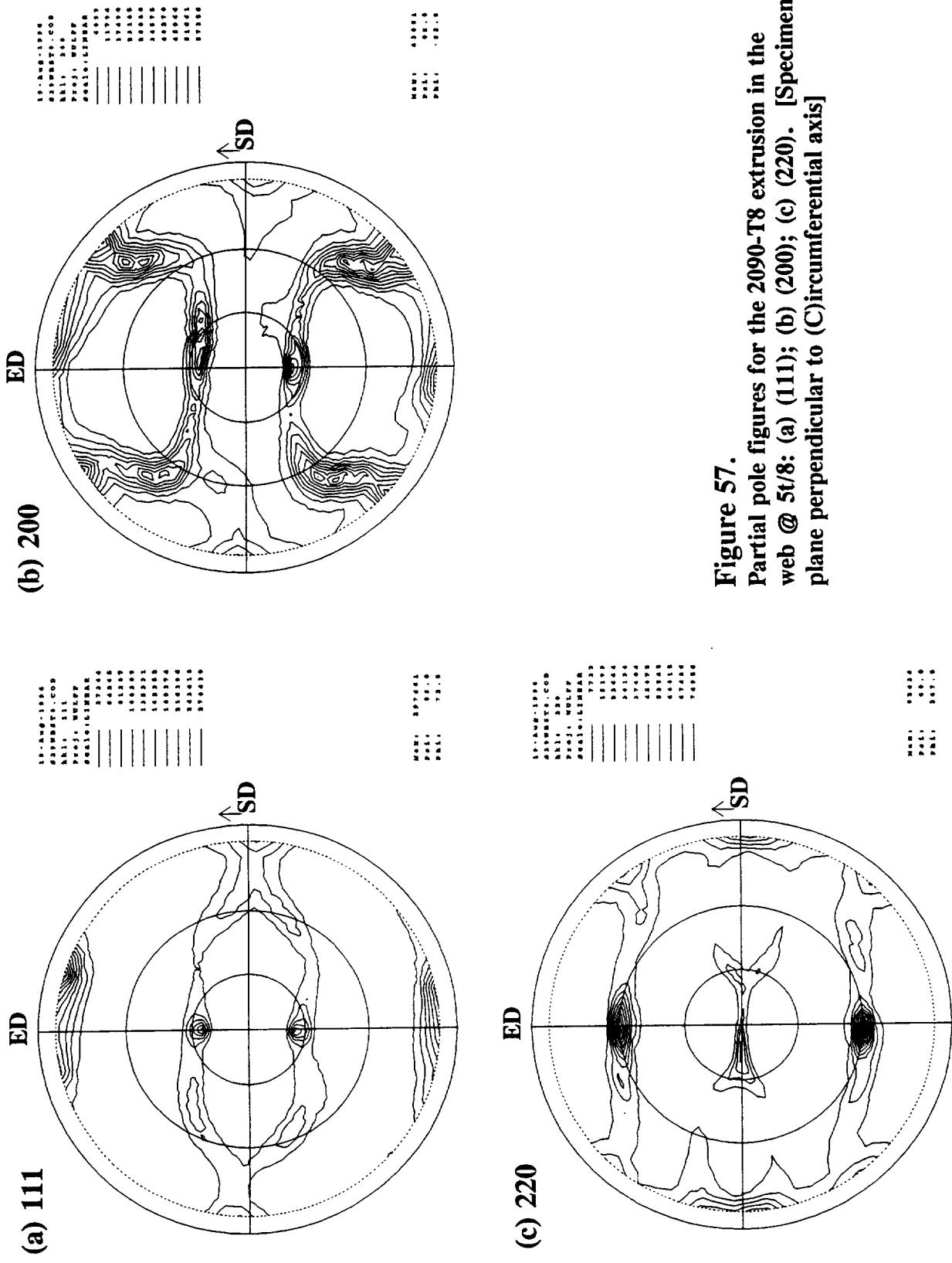


Figure 57.
Partial pole figures for the 2090-T8 extrusion in the
web @ 5t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

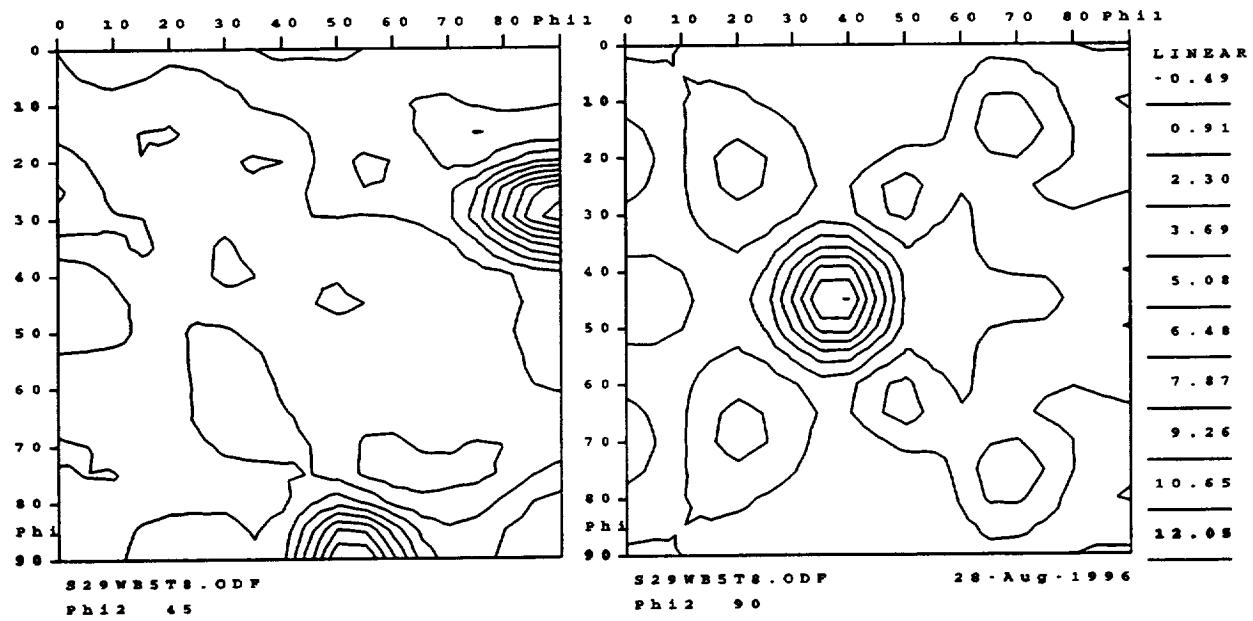


Figure 58. CODF sections for the 2090-T8 extrusion in the web @ 5t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

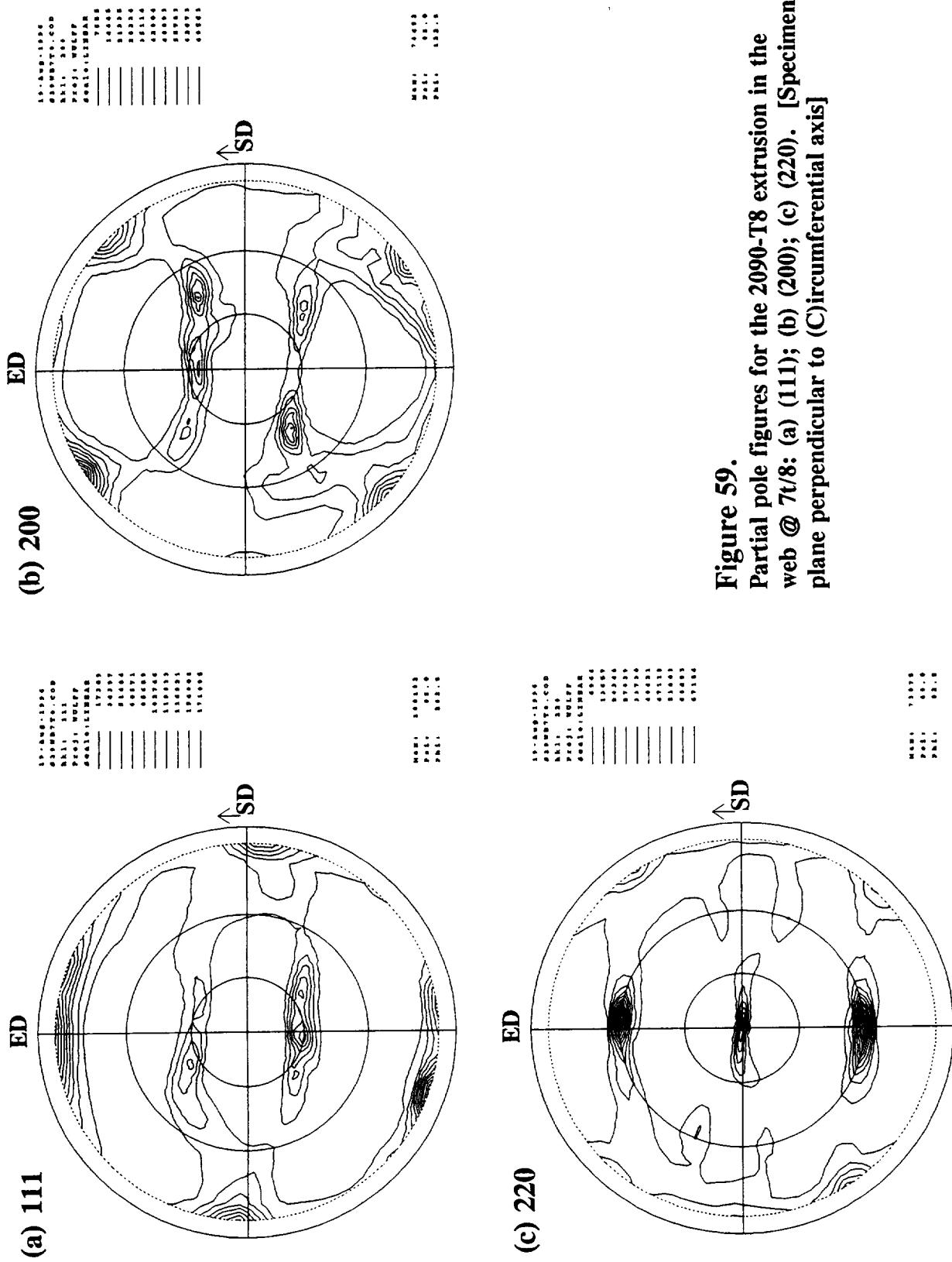
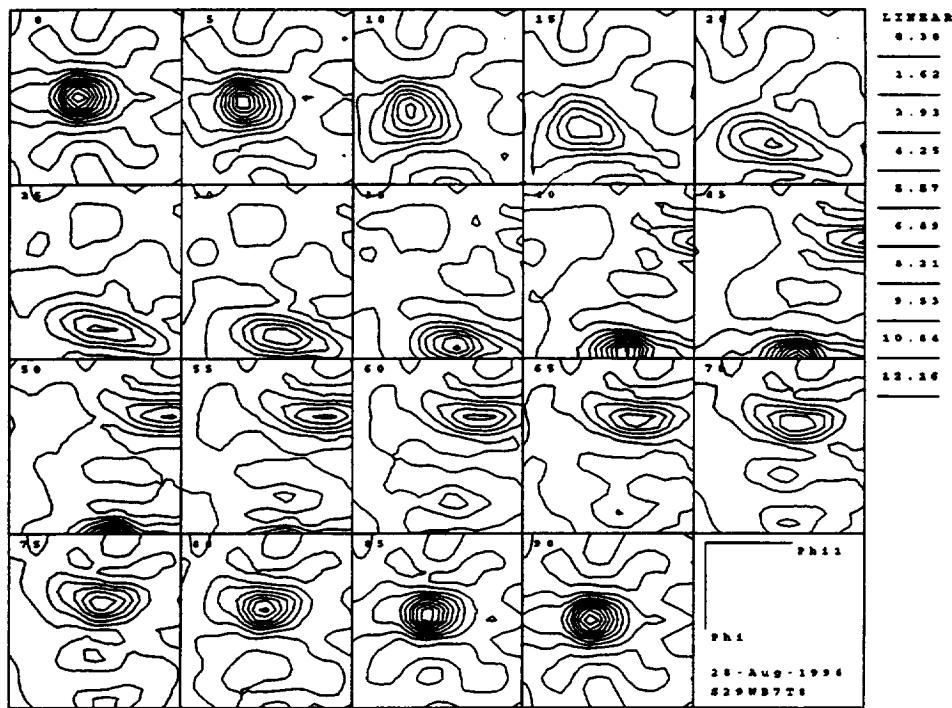


Figure 59.
Partial pole figures for the 2090-T8 extrusion in the
web @ 7t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

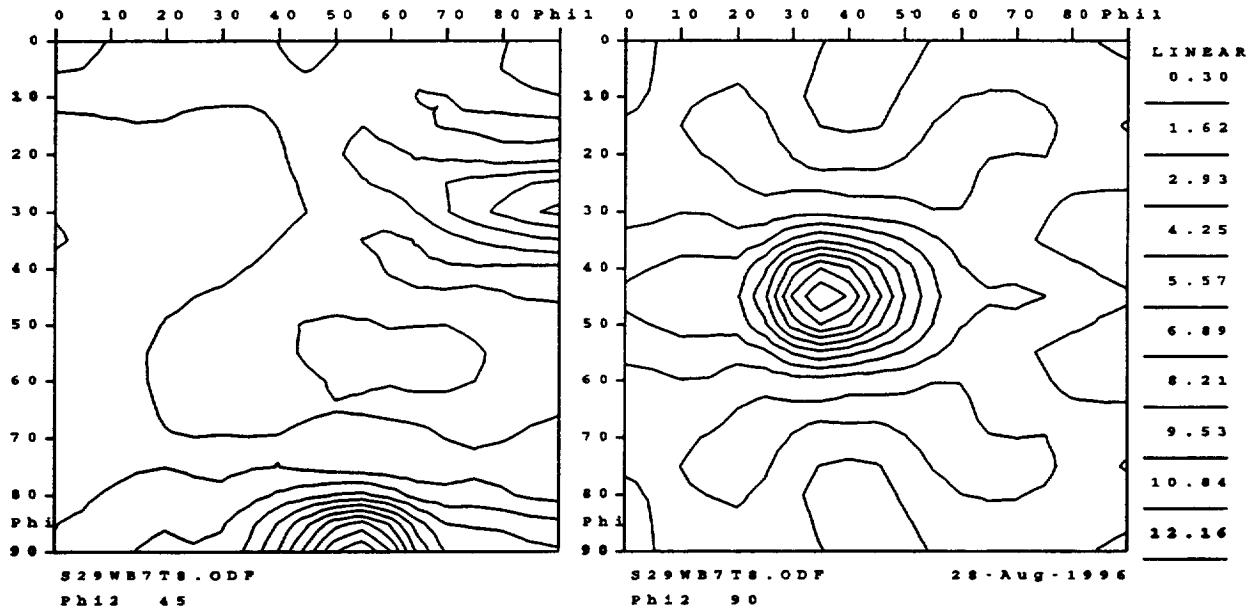


Figure 60. CODF sections for the 2090-T8 extrusion in the web @ 7t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

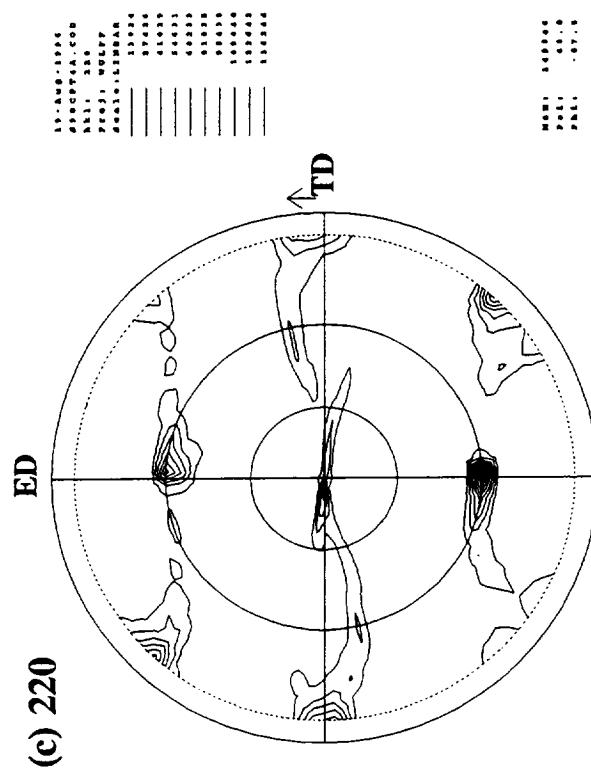
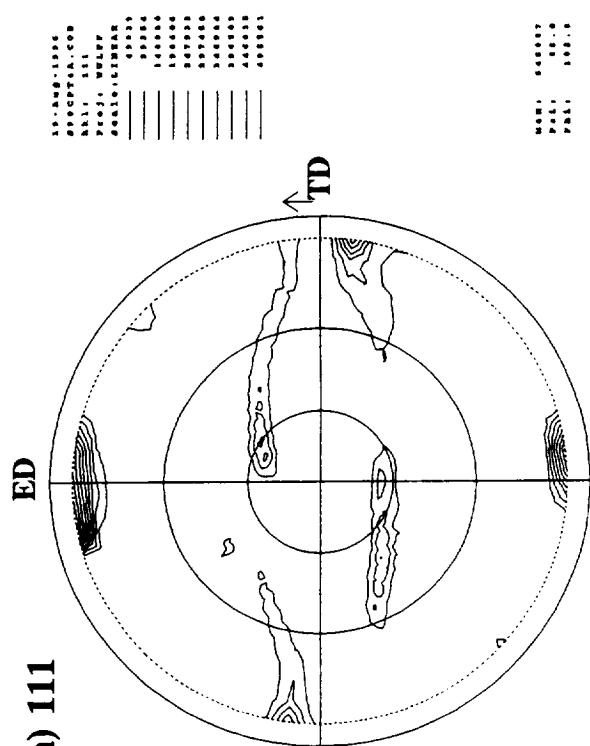
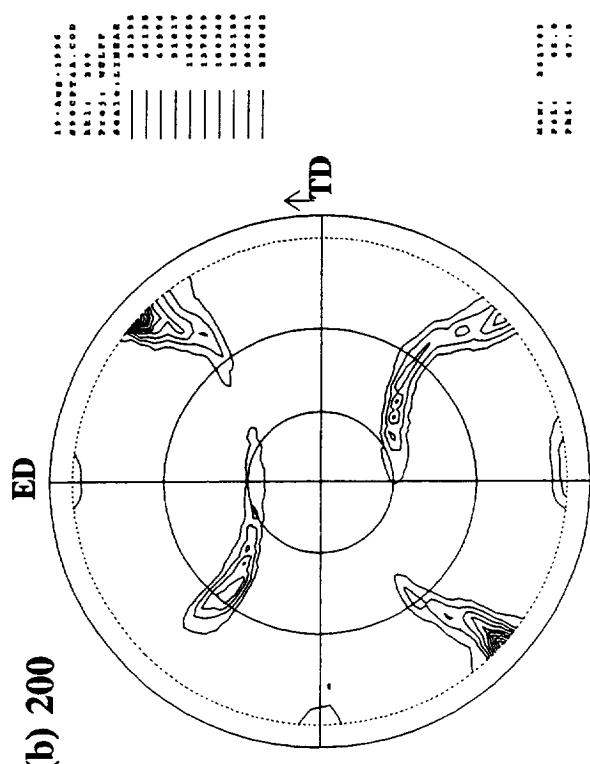
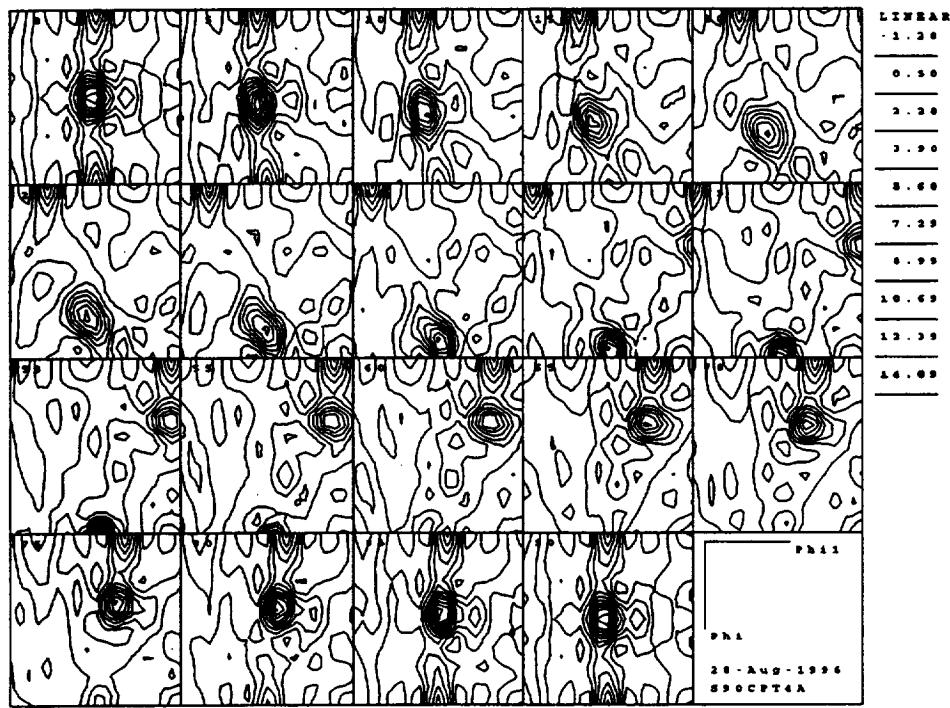


Figure 61.
Partial pole figures for the 2090-T8 extrusion in
the cap @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R) radial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

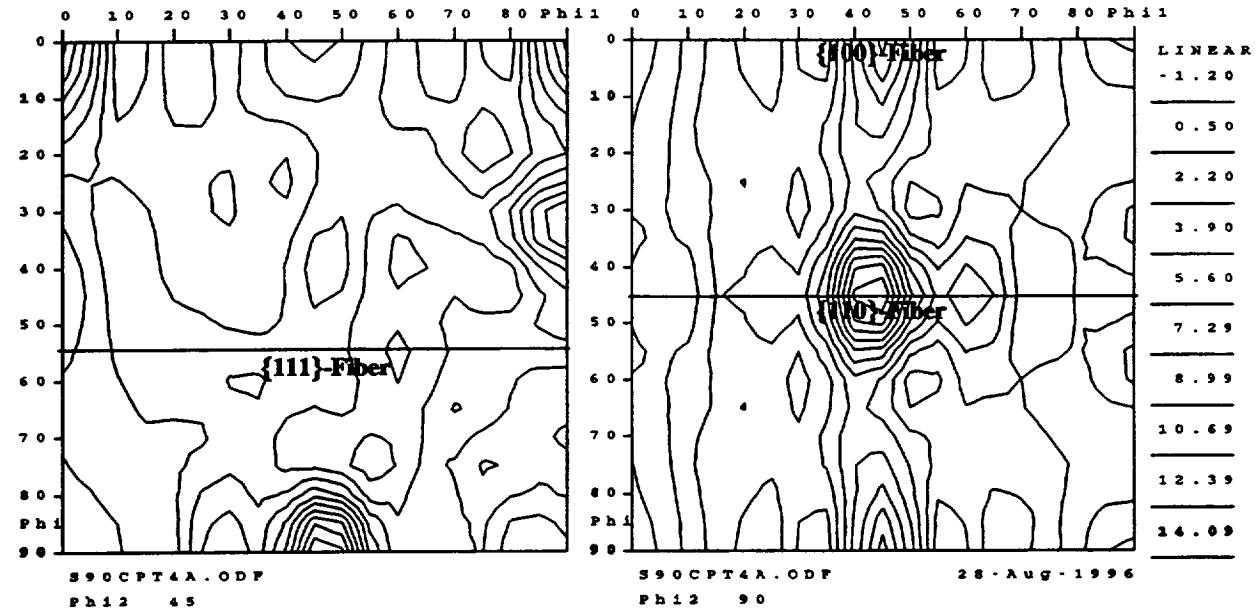


Figure 62. CODF sections for the 2090-T8 extrusion in the cap @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

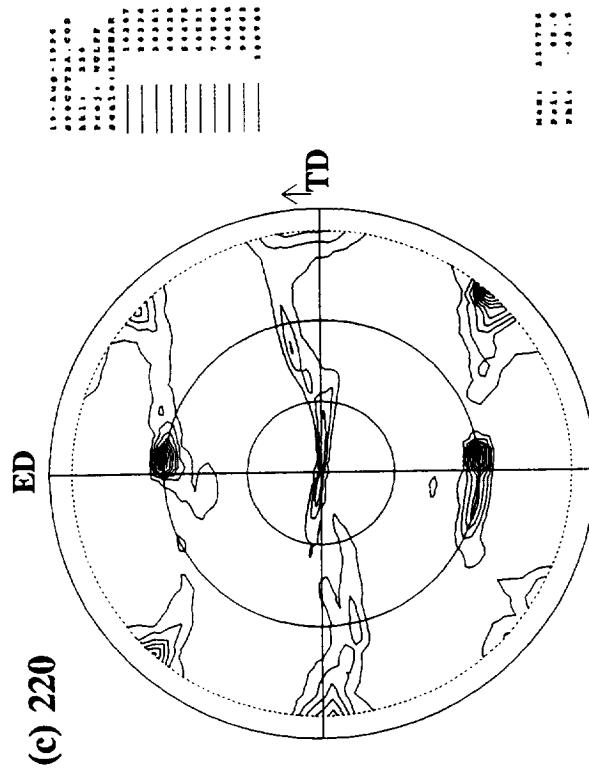
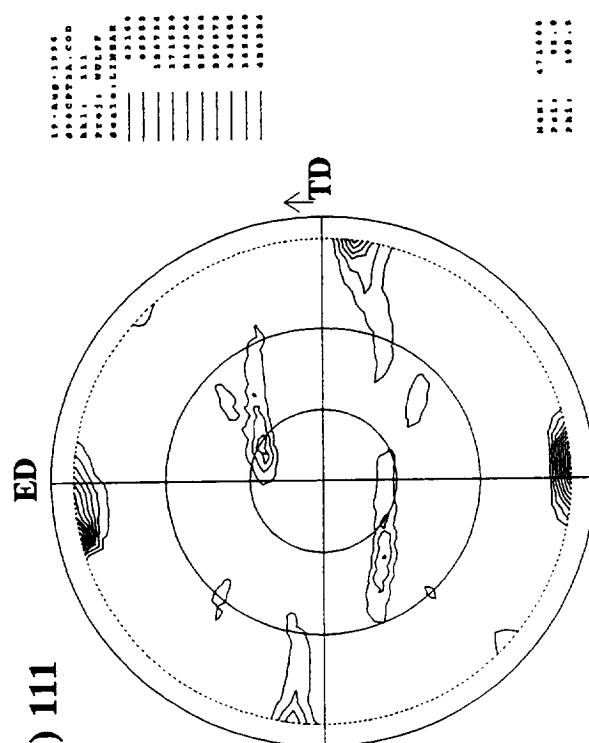
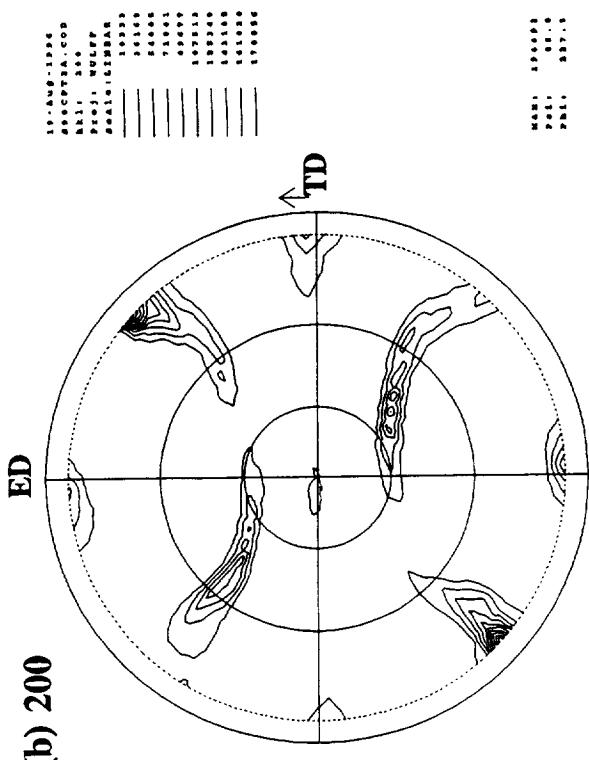
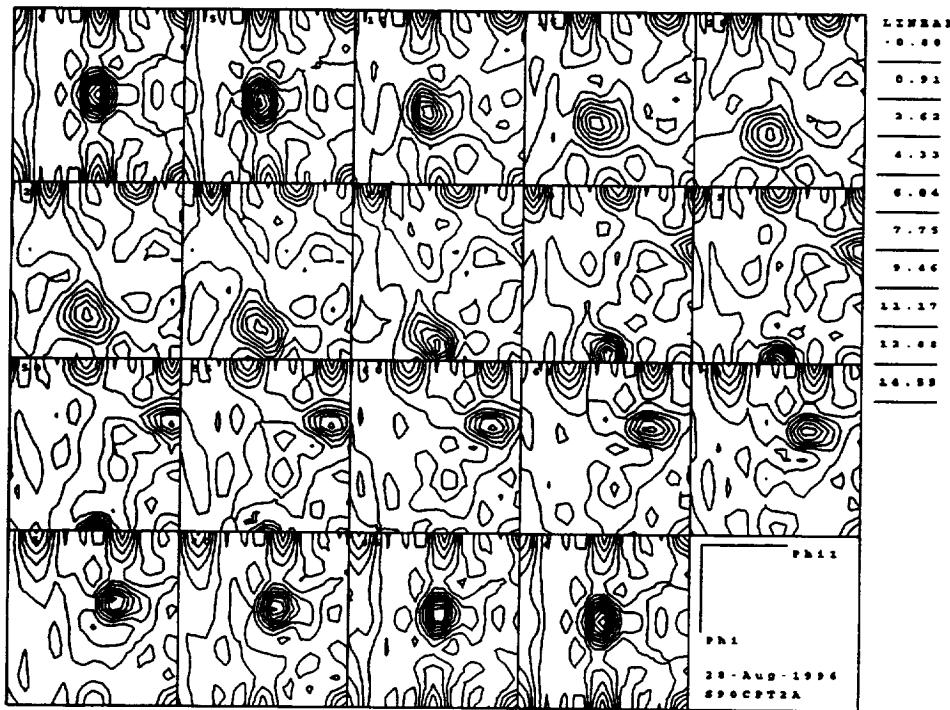


Figure 63.
Partial pole figures for the 2090-T8 extrusion in
the cap @ t/2: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

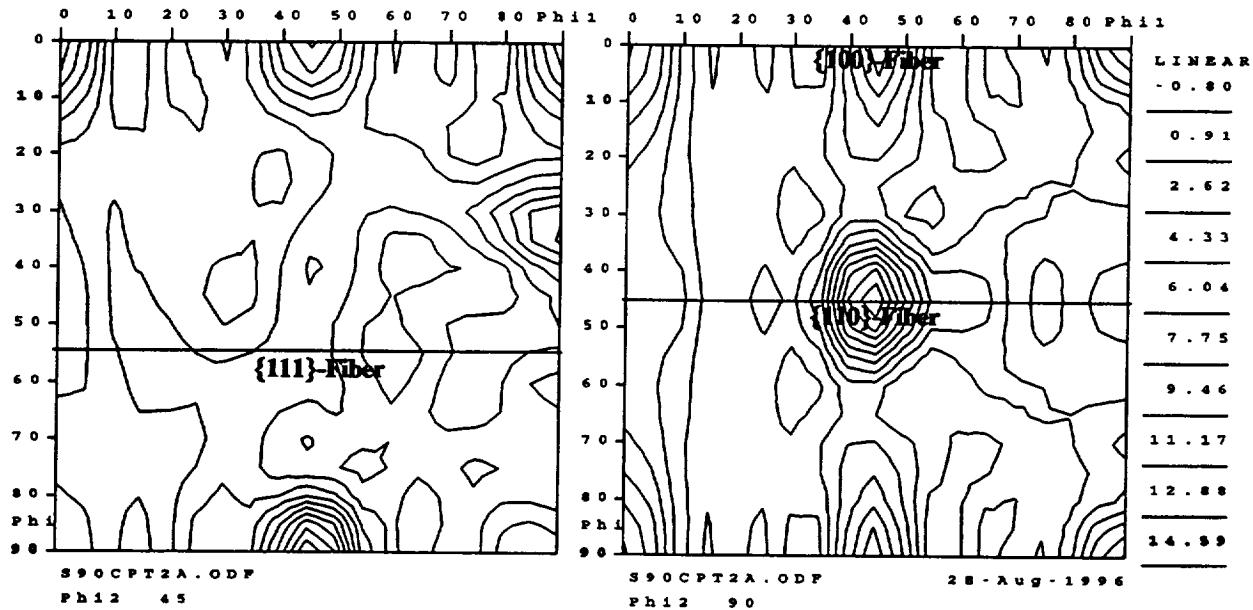


Figure 64. CODF sections for the 2090-T8 extrusion in the cap @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

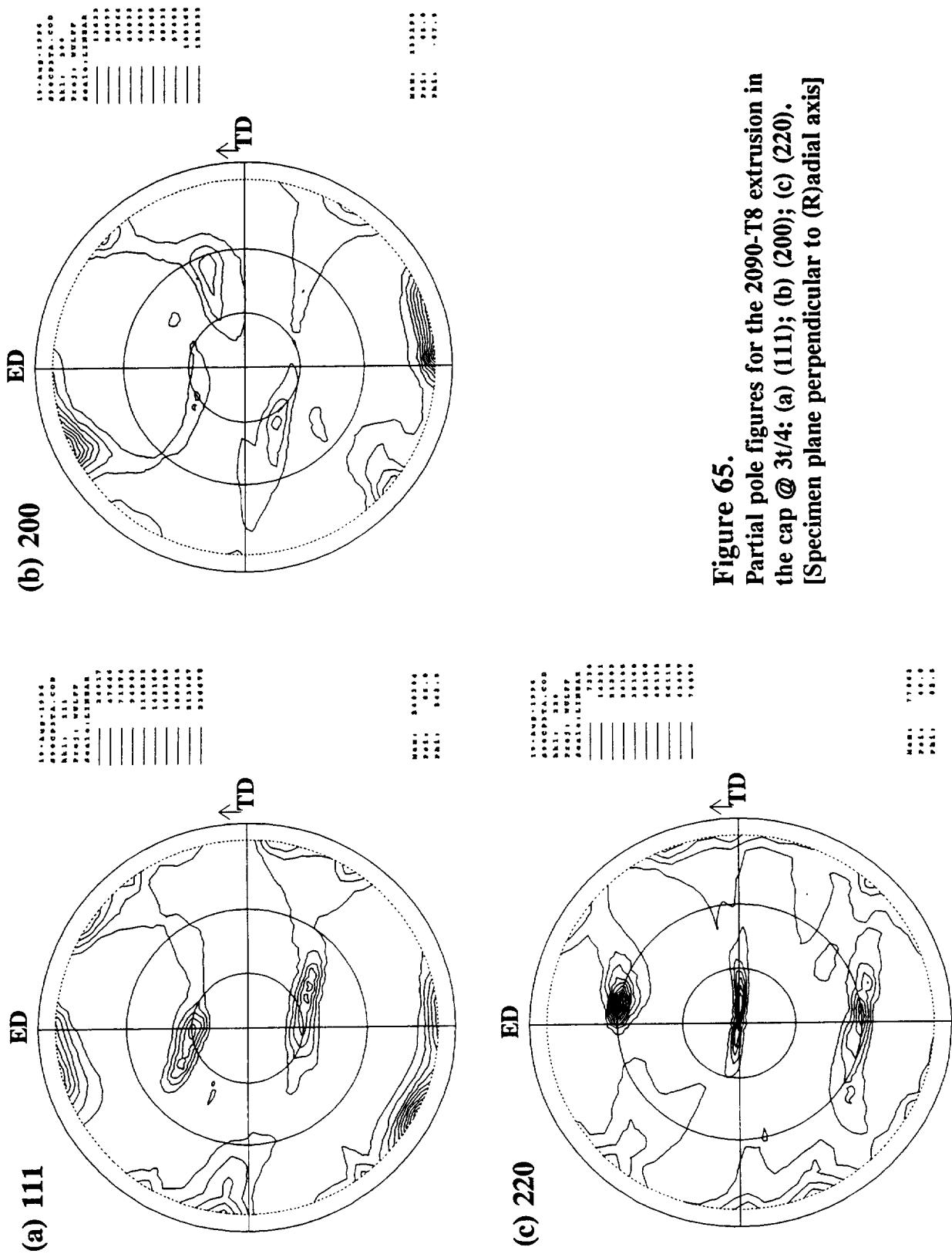
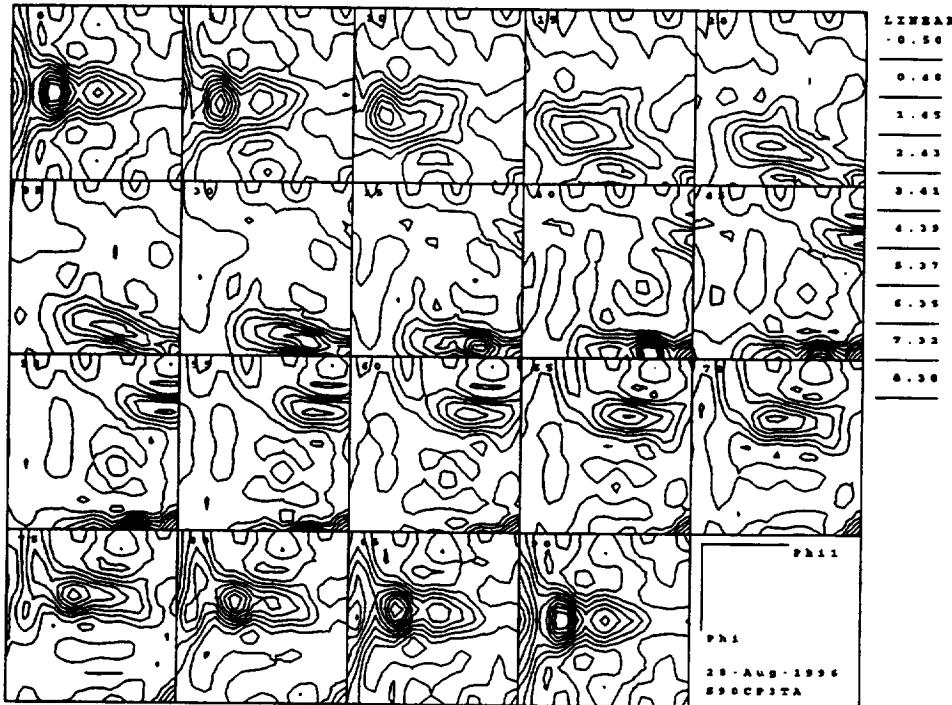


Figure 65.
Partial pole figures for the 2090-T8 extrusion in
the cap @ 3t/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R) radial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

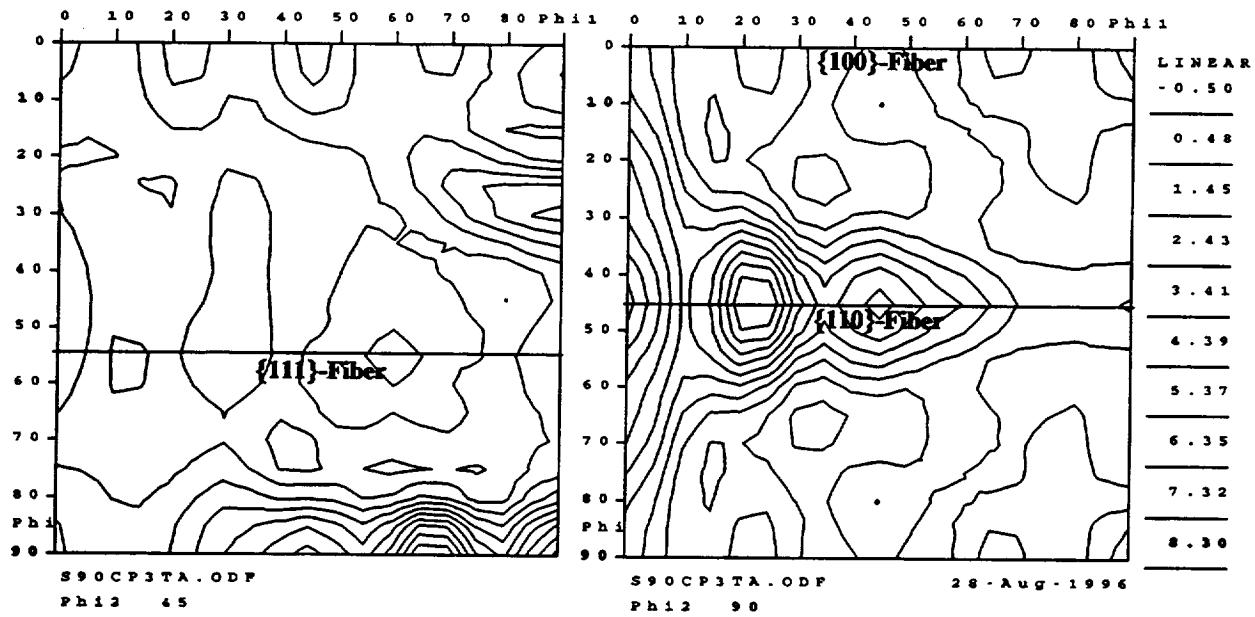


Figure 66. CODF sections for the 2090-T8 extrusion in the cap @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

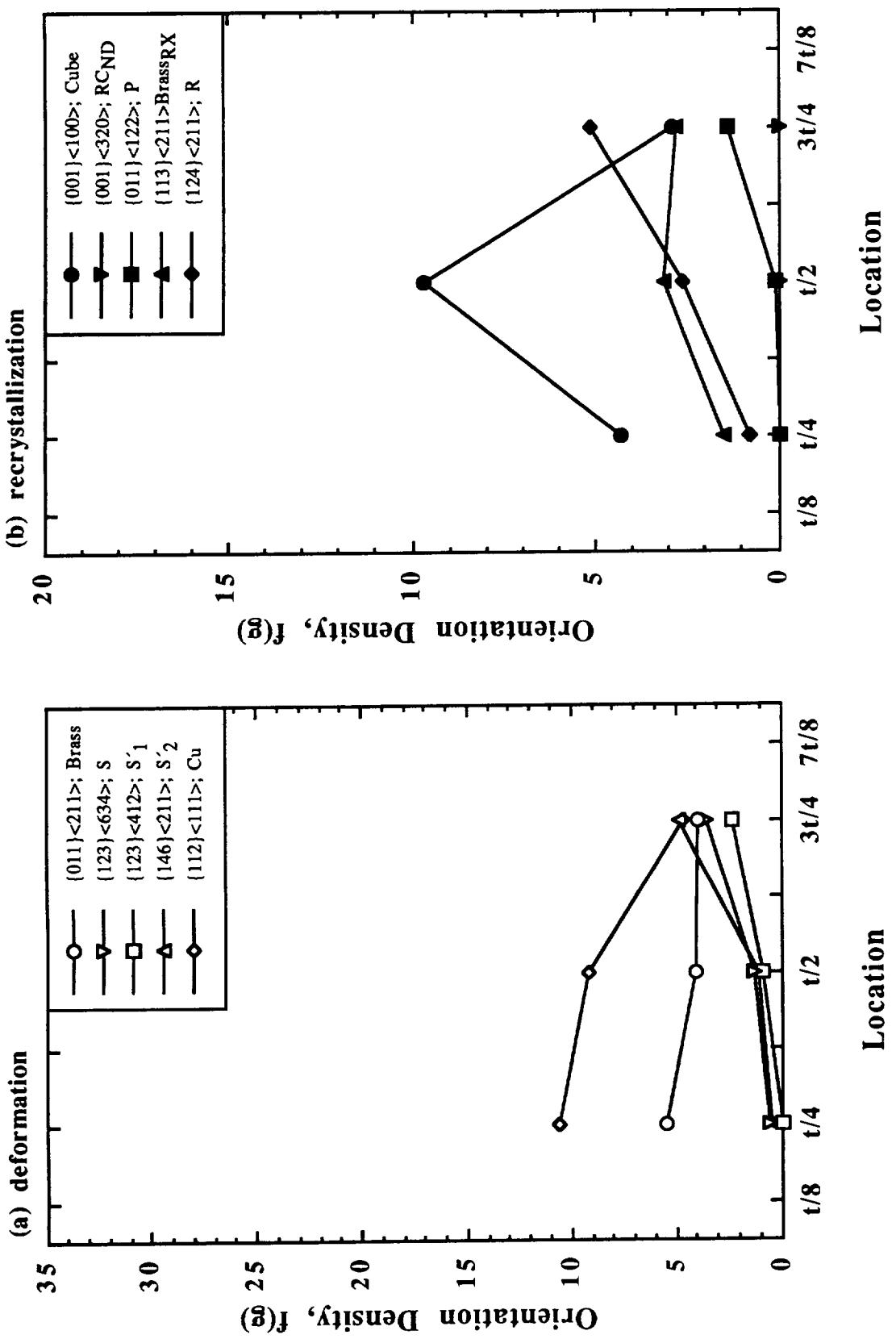
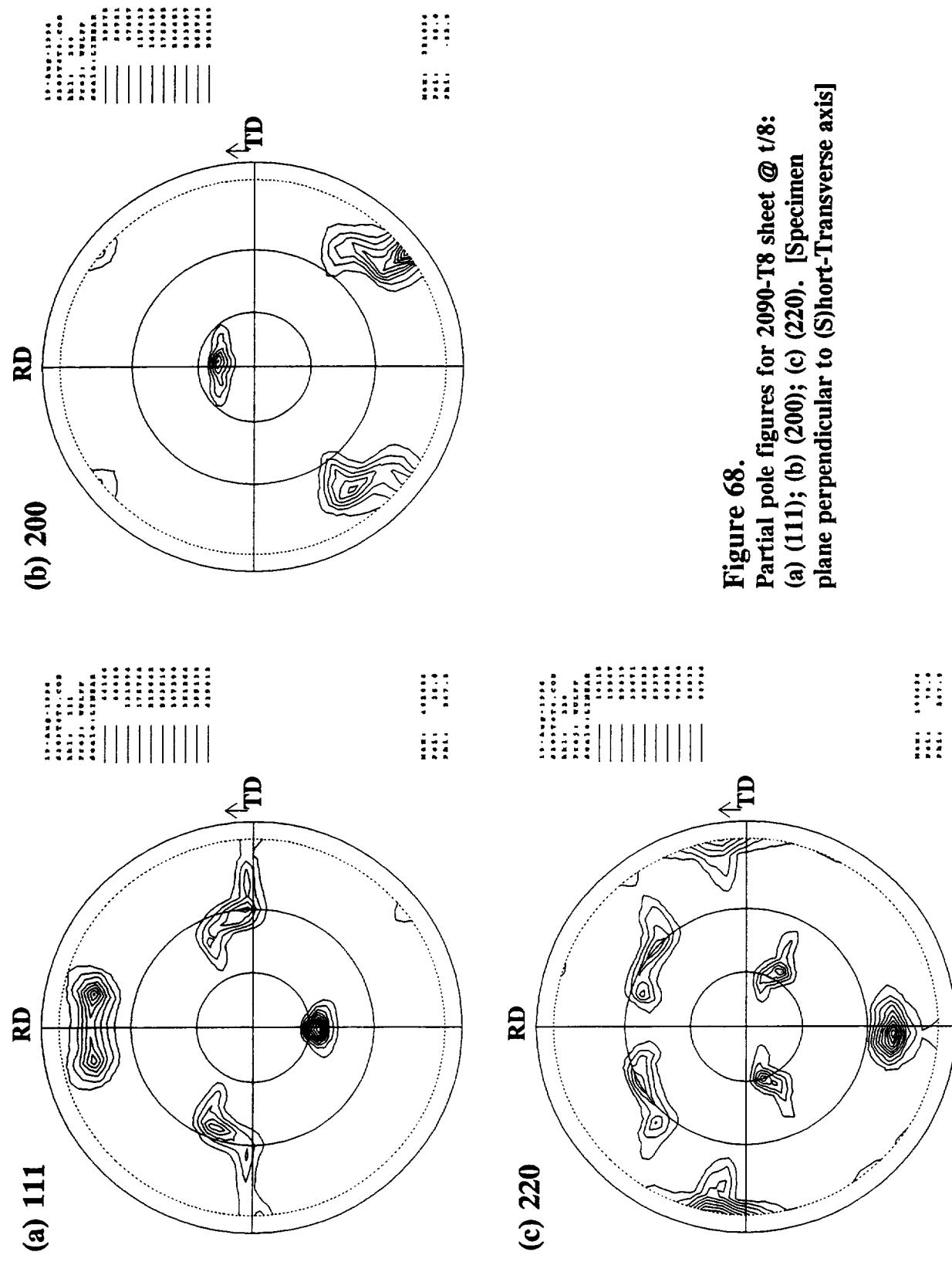
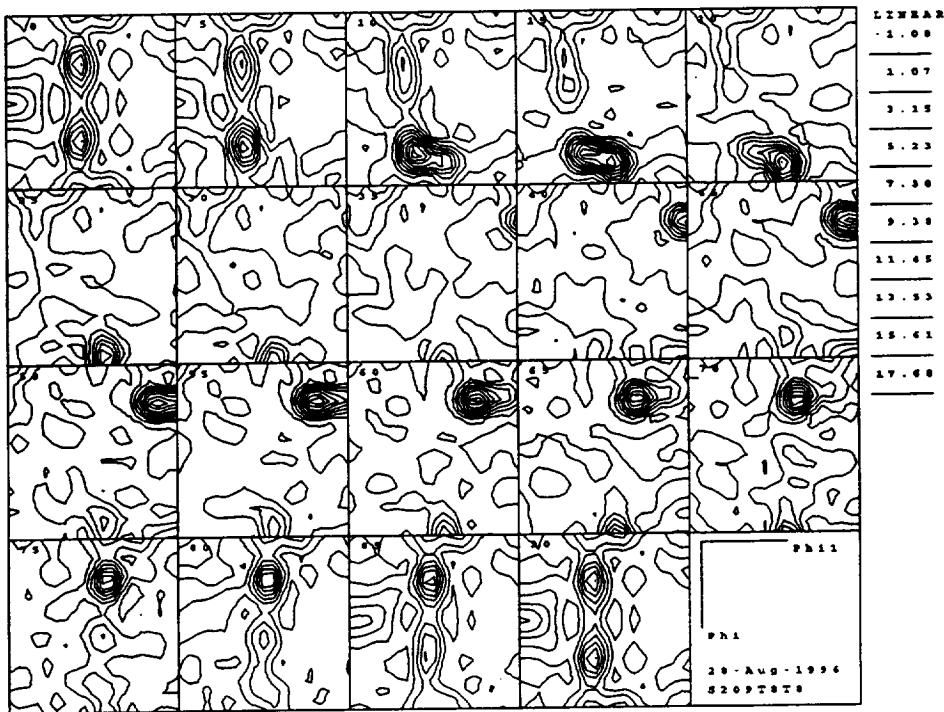


Figure 67. Orientation density, $f(g)$, as a function of location through the cross-section for the 2090-T8 extrusion in the cap region: (a) Deformation-related components; (b) Recrystallization-related components.



(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

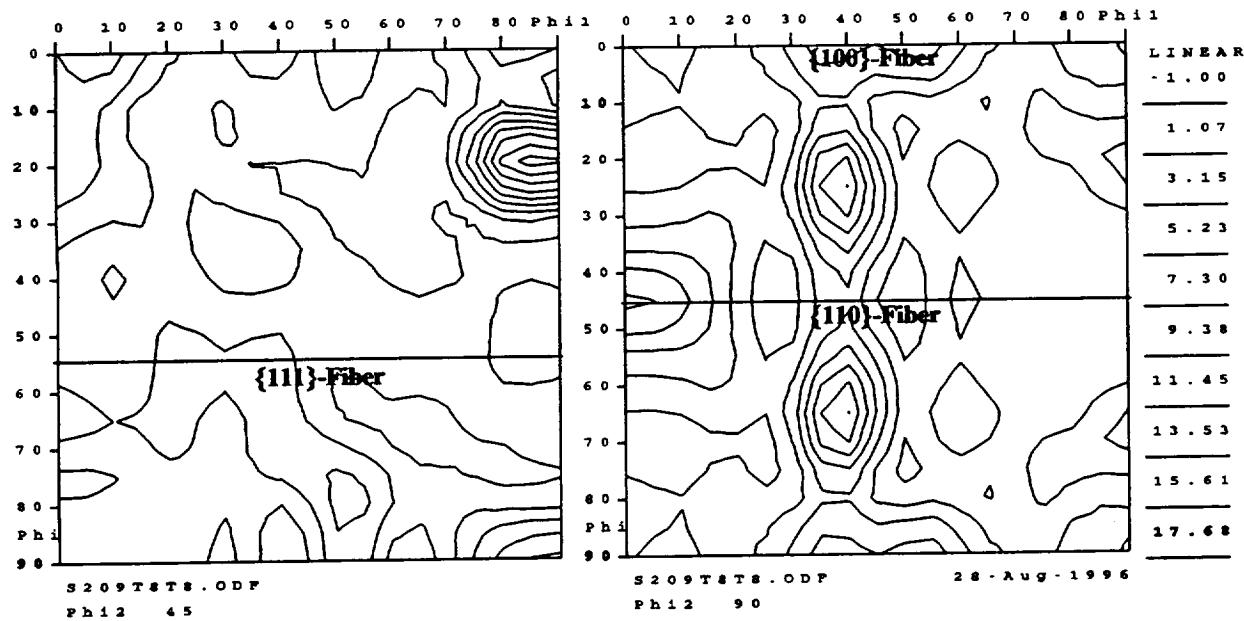
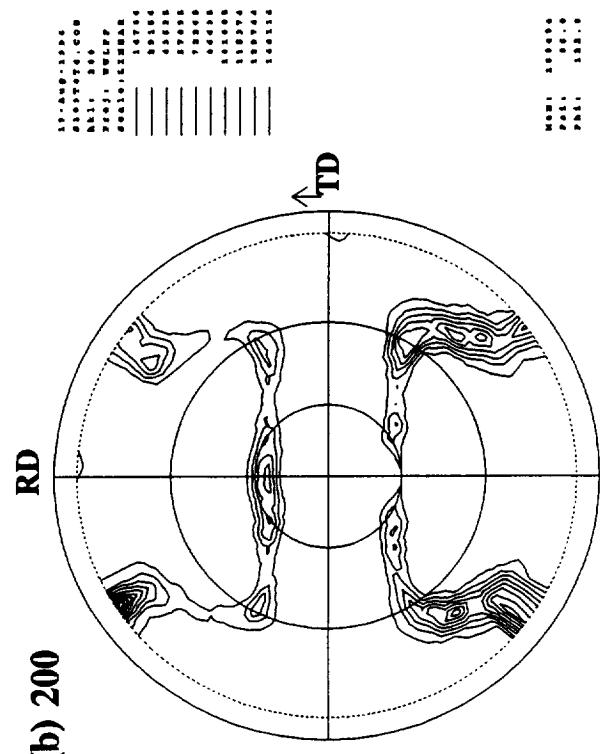
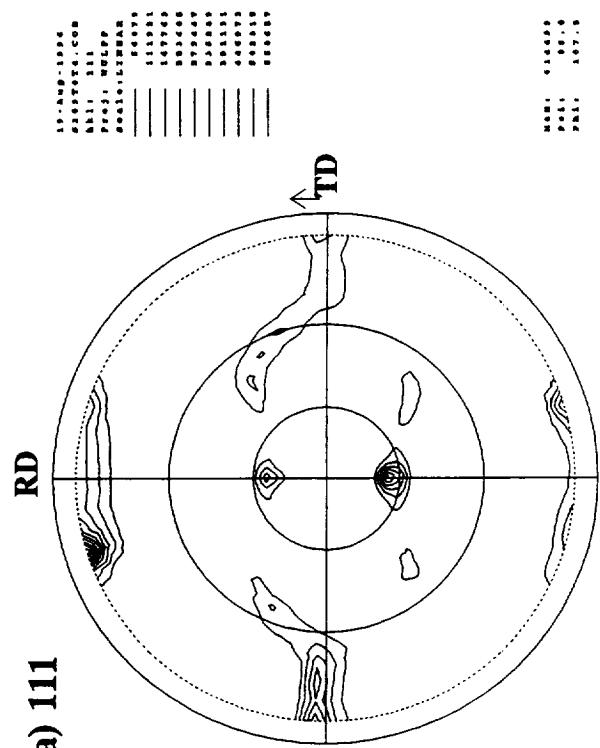


Figure 69. CODF sections for 2090-T8 sheet @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.

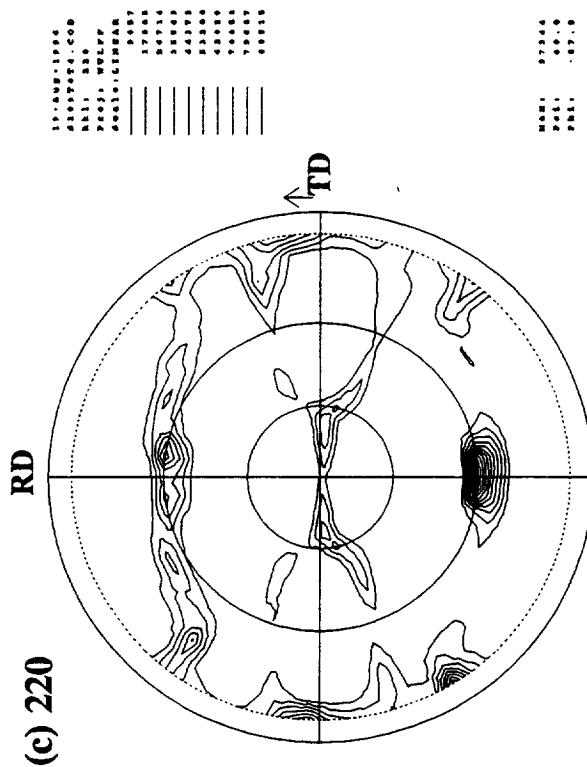
[Specimen plane perpendicular to (S)hort-Transverse axis]



(b) 200



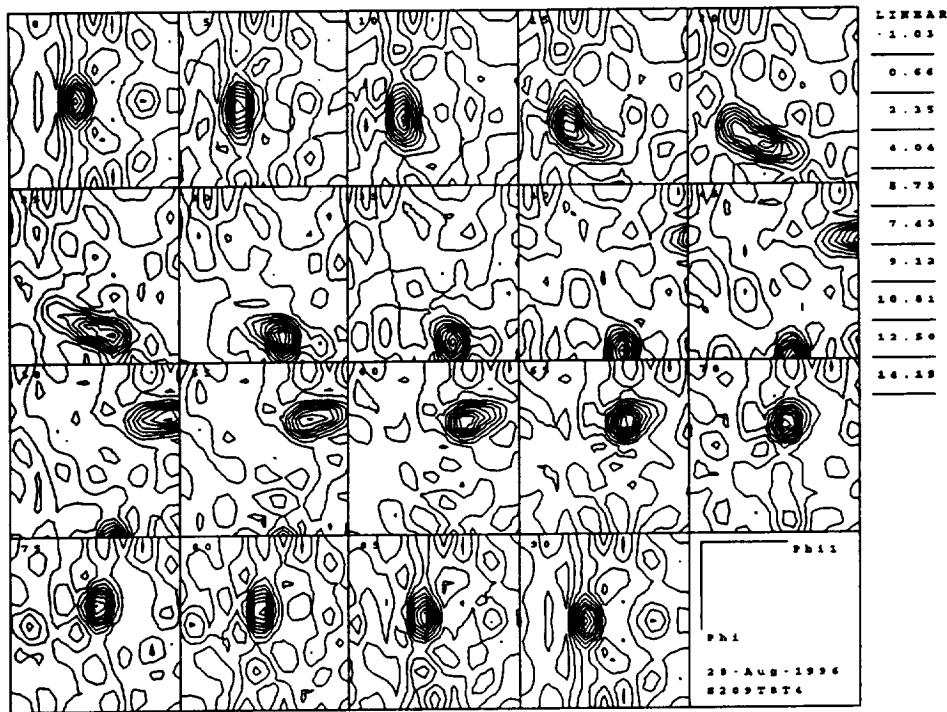
(a) 111



(c) 220

Figure 70.
Partial pole figures for 2090-T8 sheet @ t/4:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

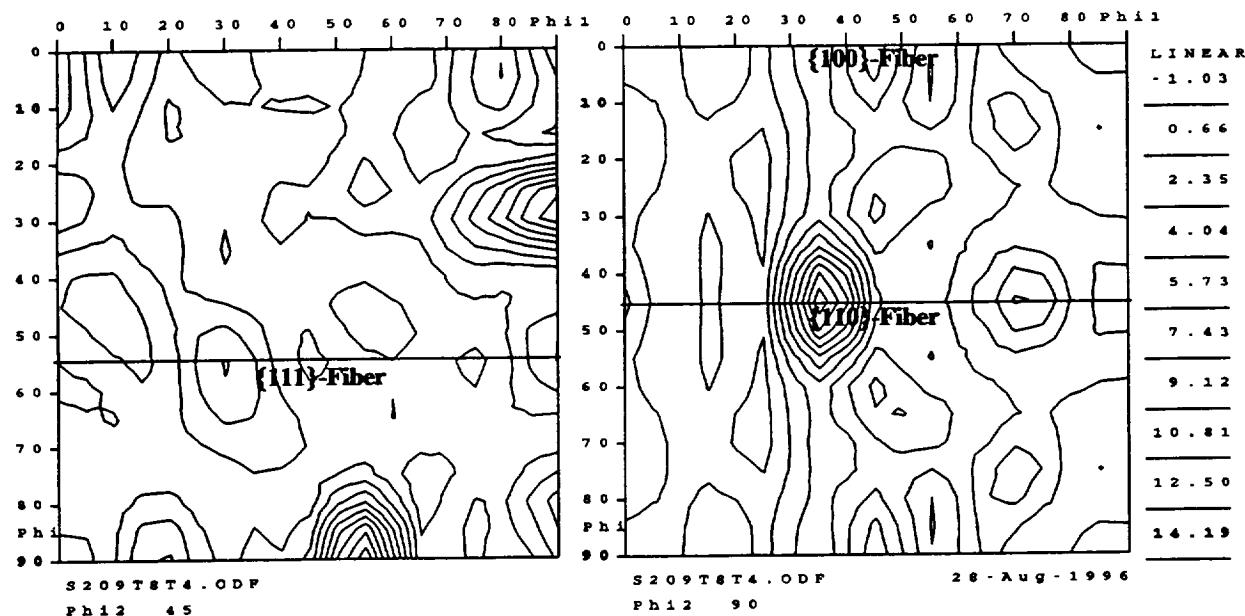


Figure 71. CODF sections for 2090-T8 sheet @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

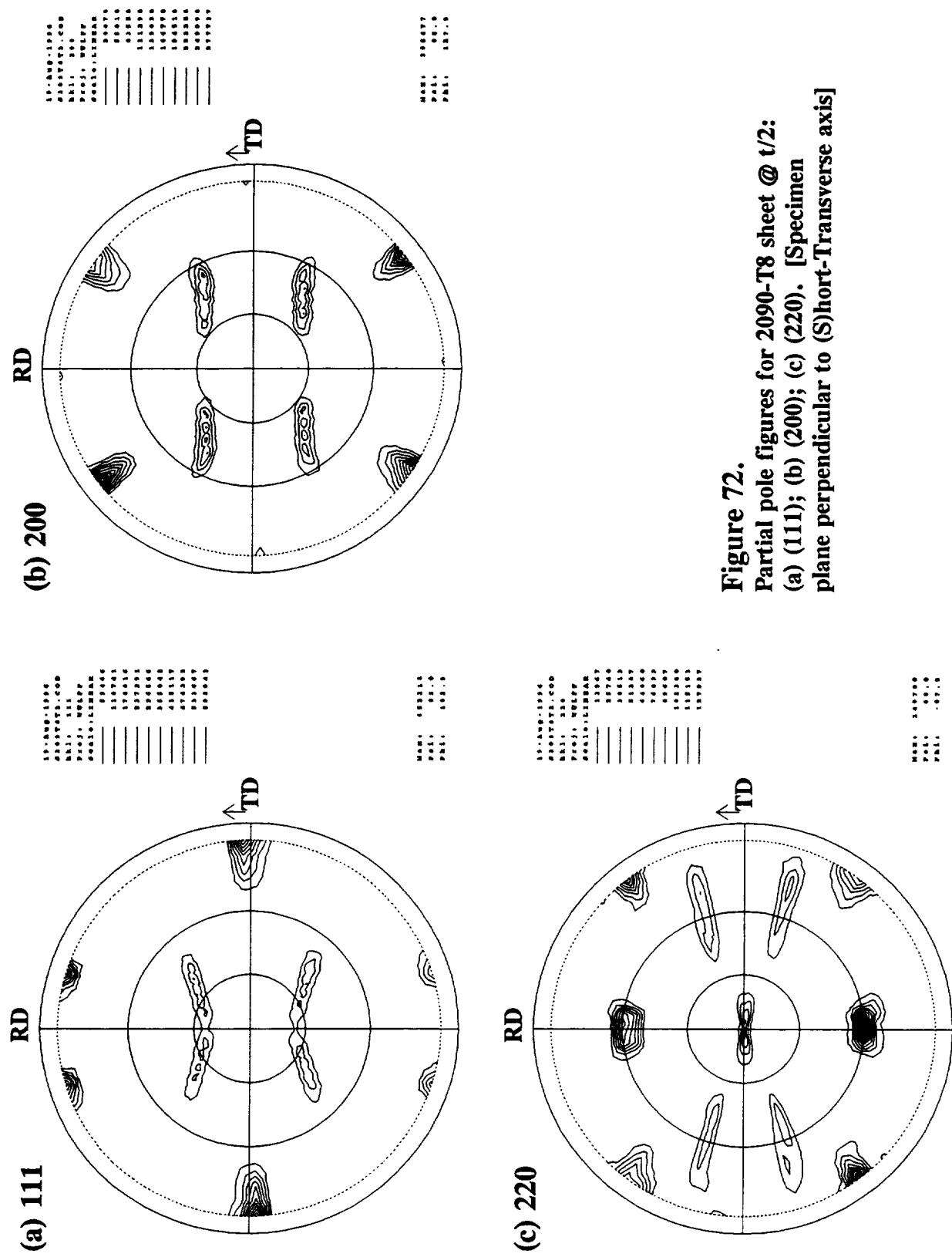
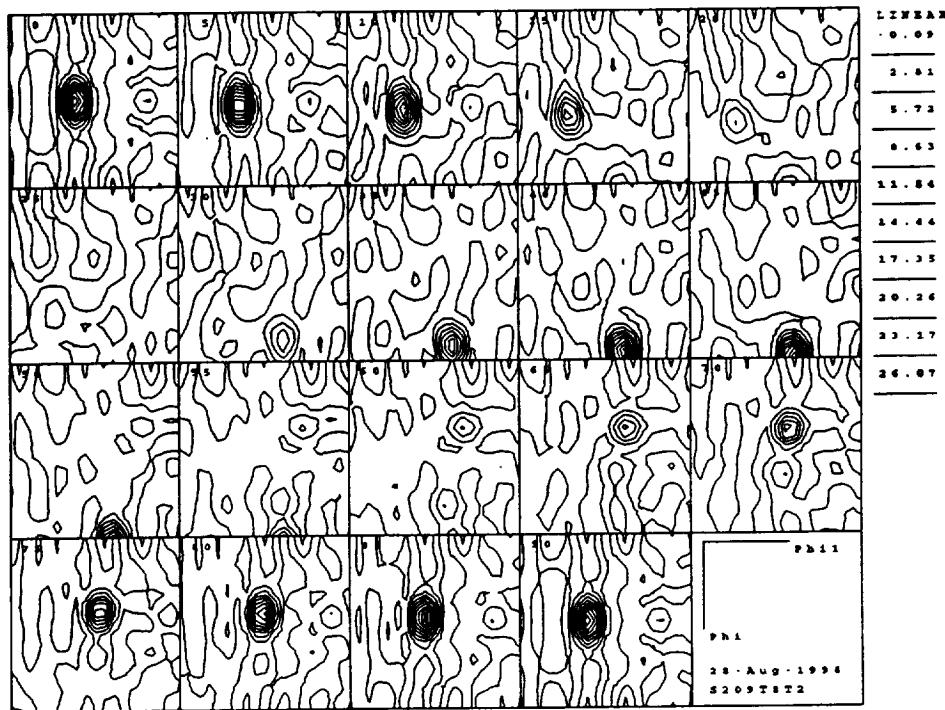


Figure 72.
Partial pole figures for 2090-T8 sheet @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

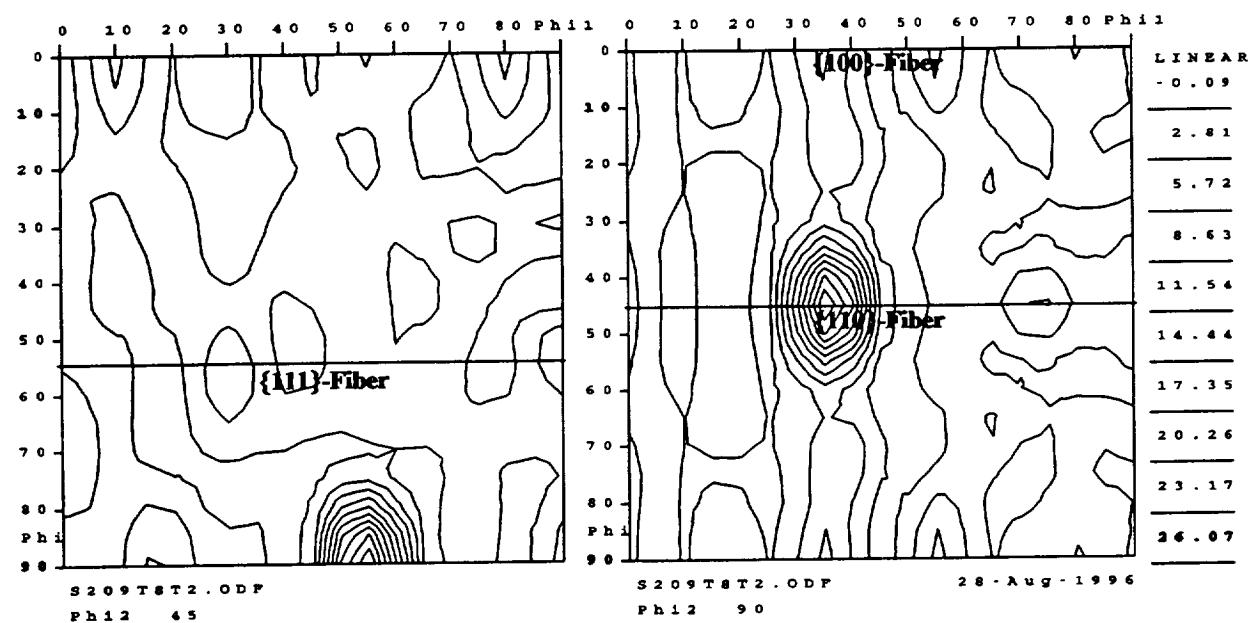


Figure 73. CODF sections for 2090-T8 sheet @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

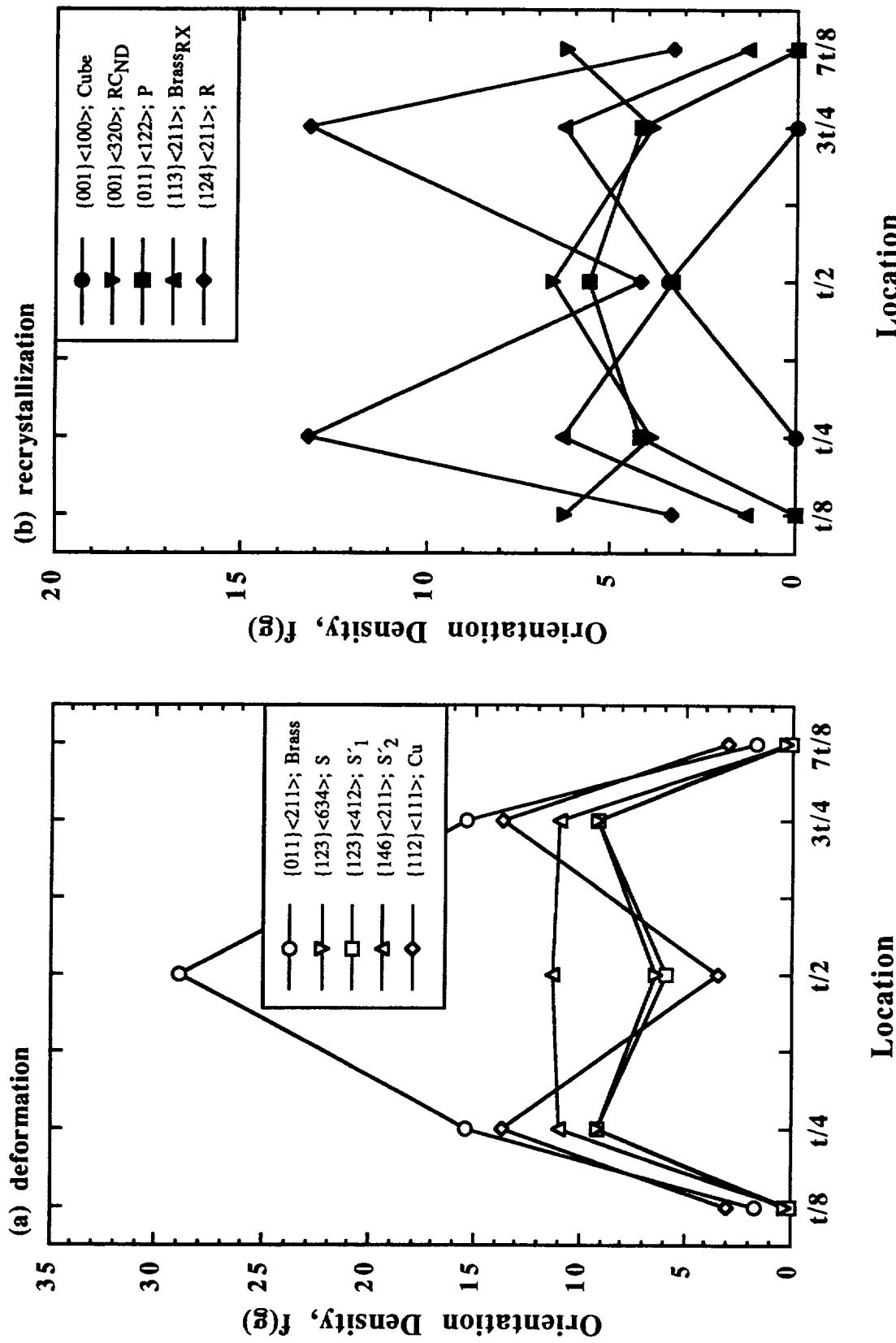


Figure 74. Orientation density, $f(g)$, as a function of location through the cross-section for the 2090-T8 sheet:
 (a) Deformation-related components; (b) Recrystallization-related components.

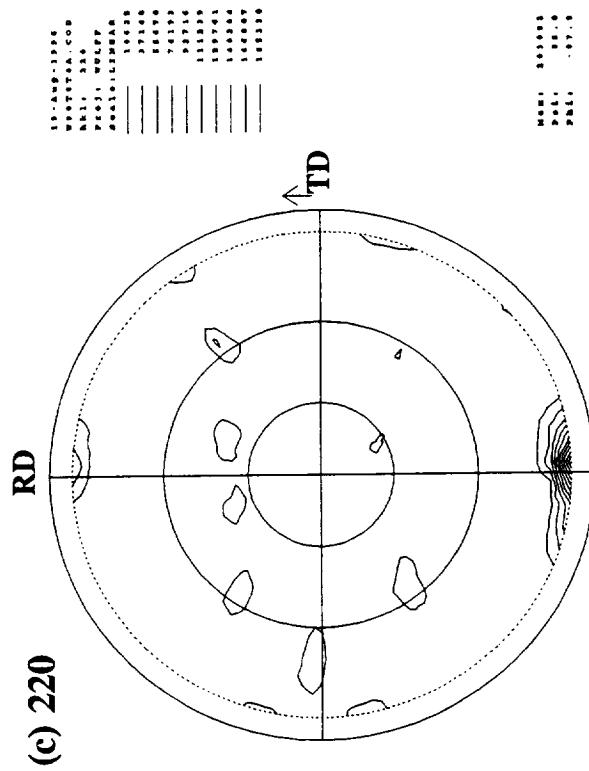
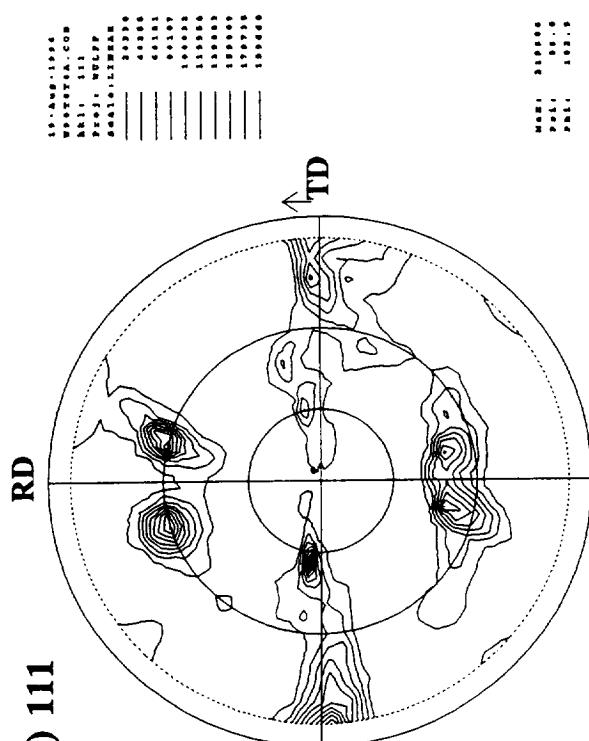
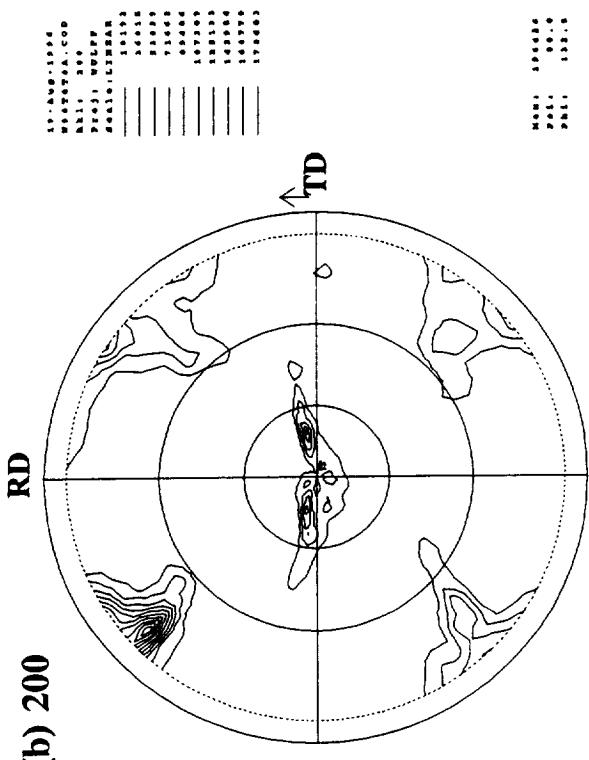
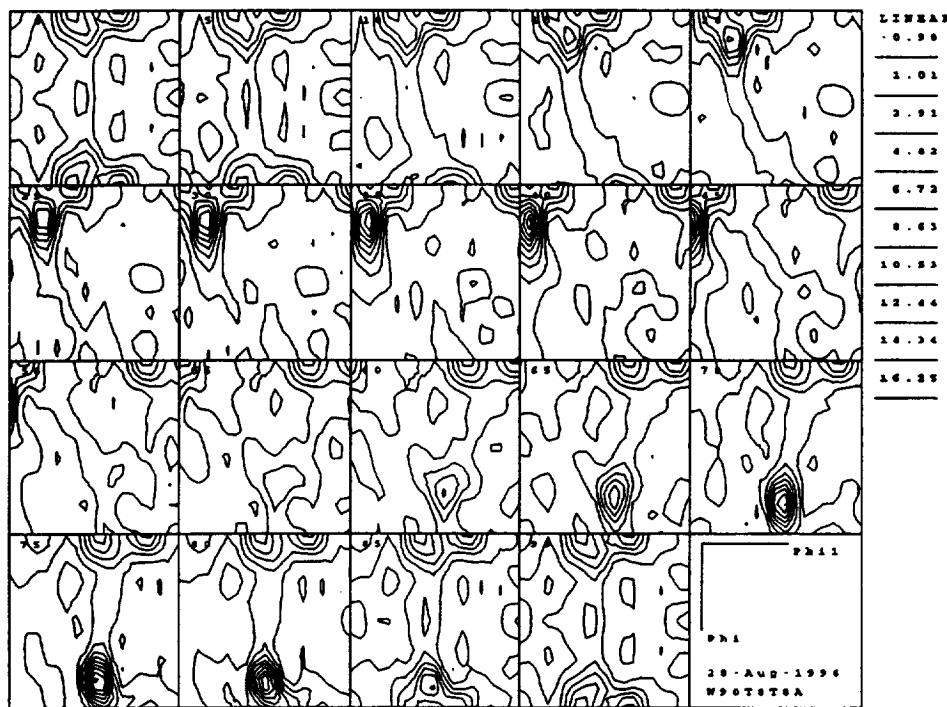


Figure 75.
Partial pole figures for 2090-T8 plate @ t/8:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

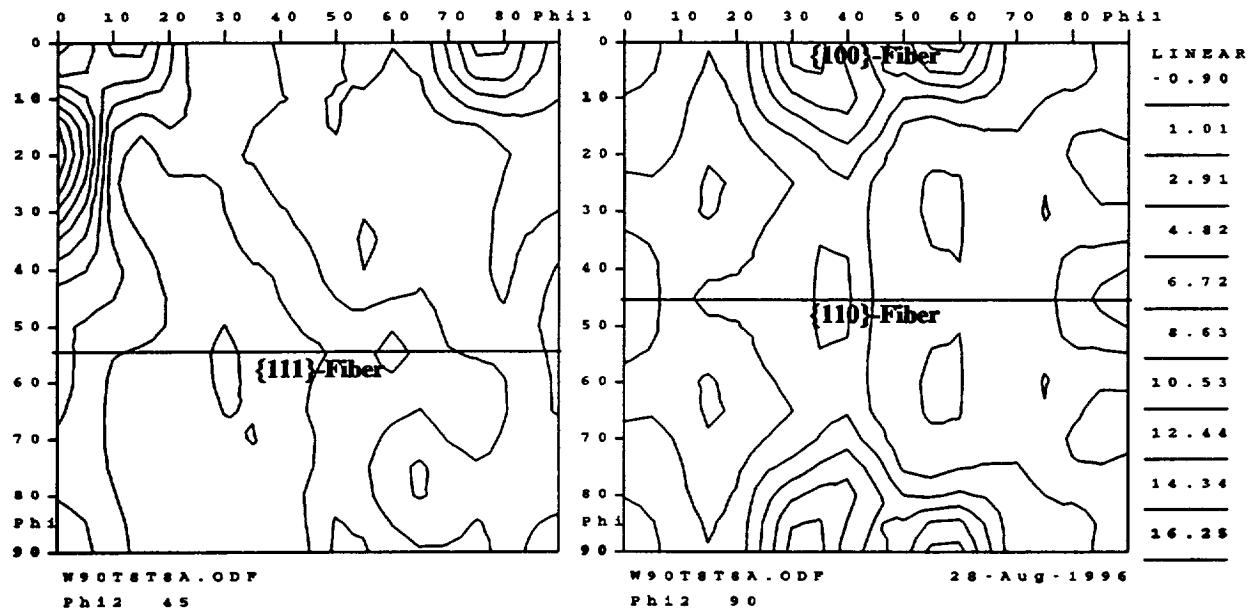


Figure 76. CODF sections for 2090-T8 plate @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

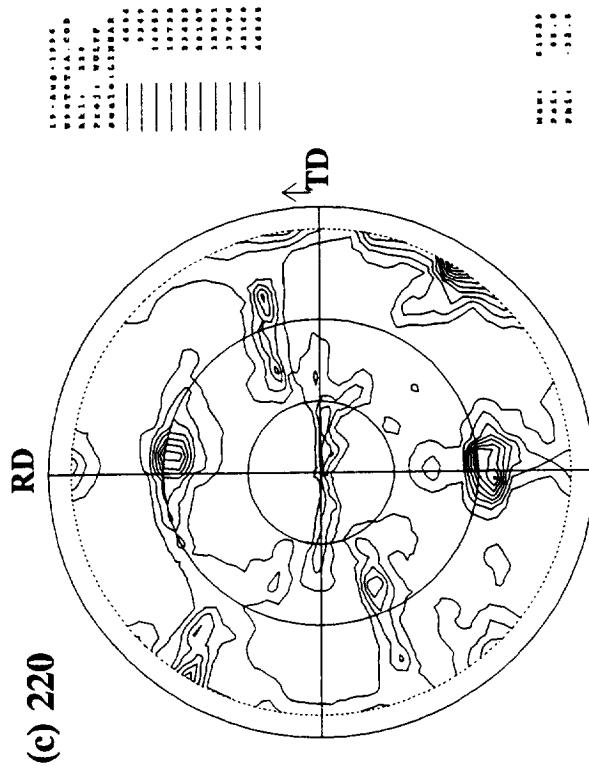
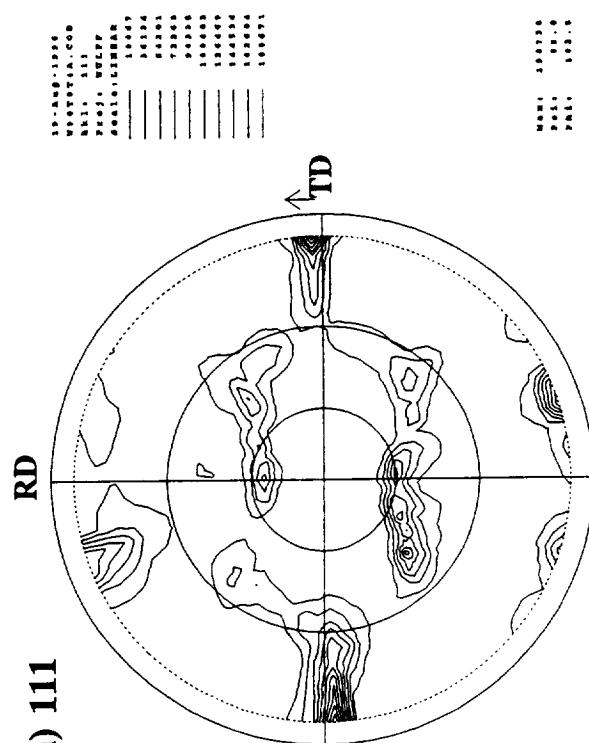
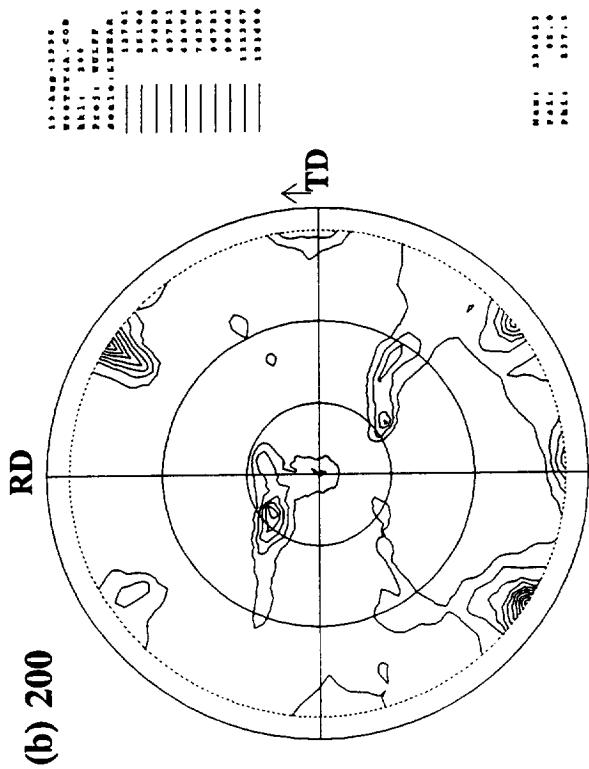
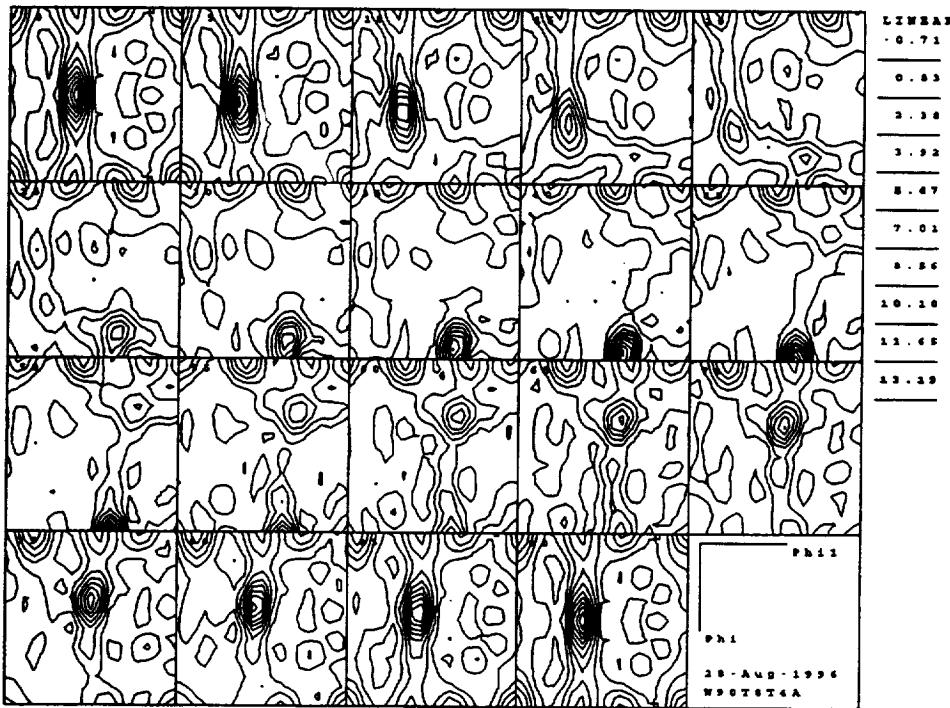


Figure 77.
Partial pole figures for 2090-T8 plate @ $t/4$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

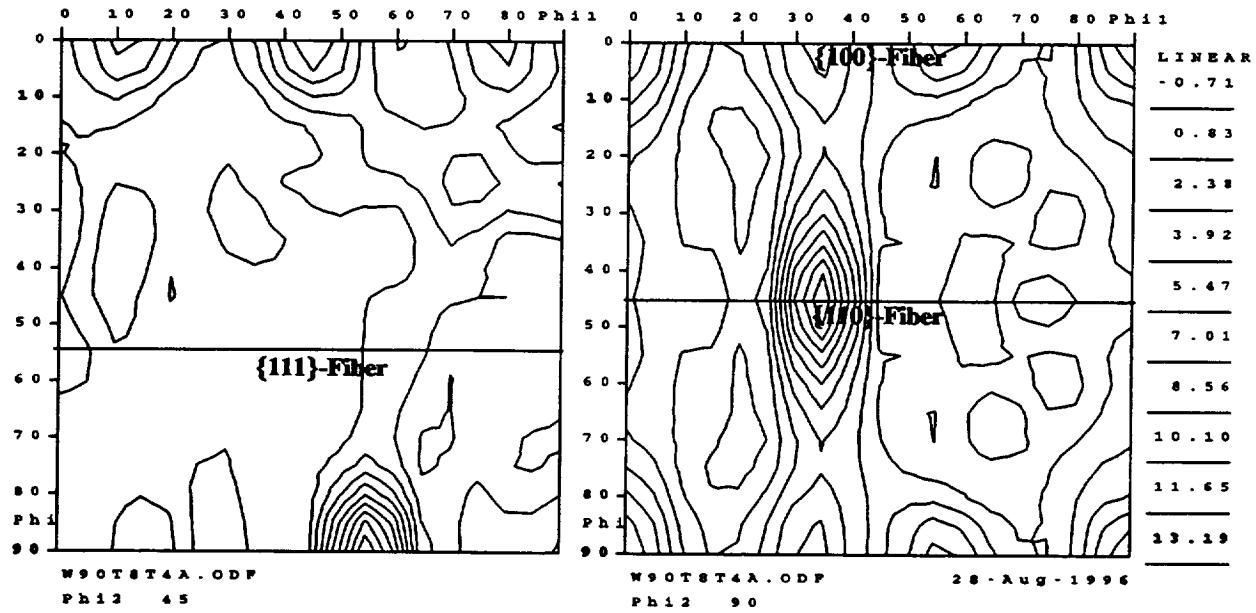


Figure 78. CODF sections for 2090-T8 plate @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

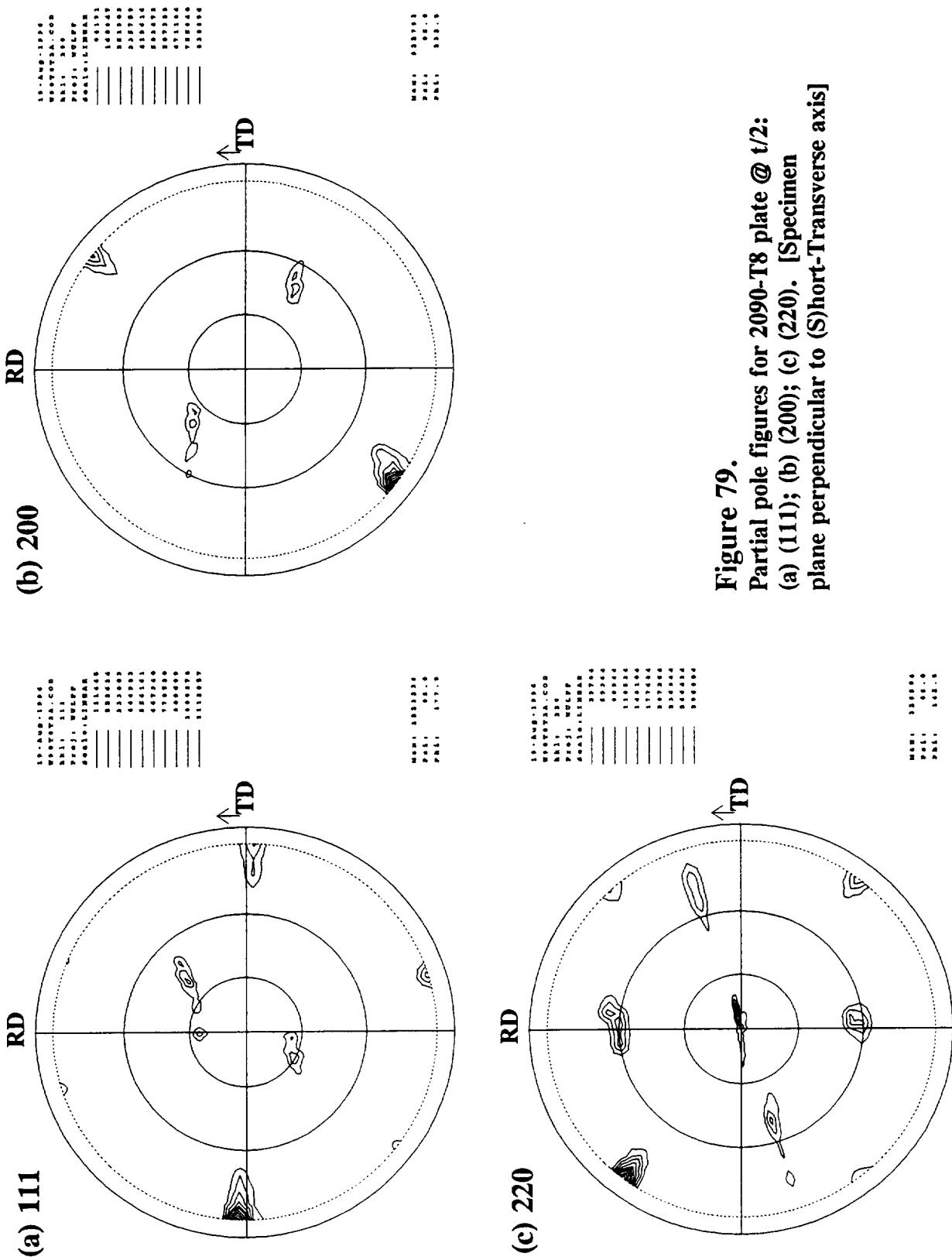
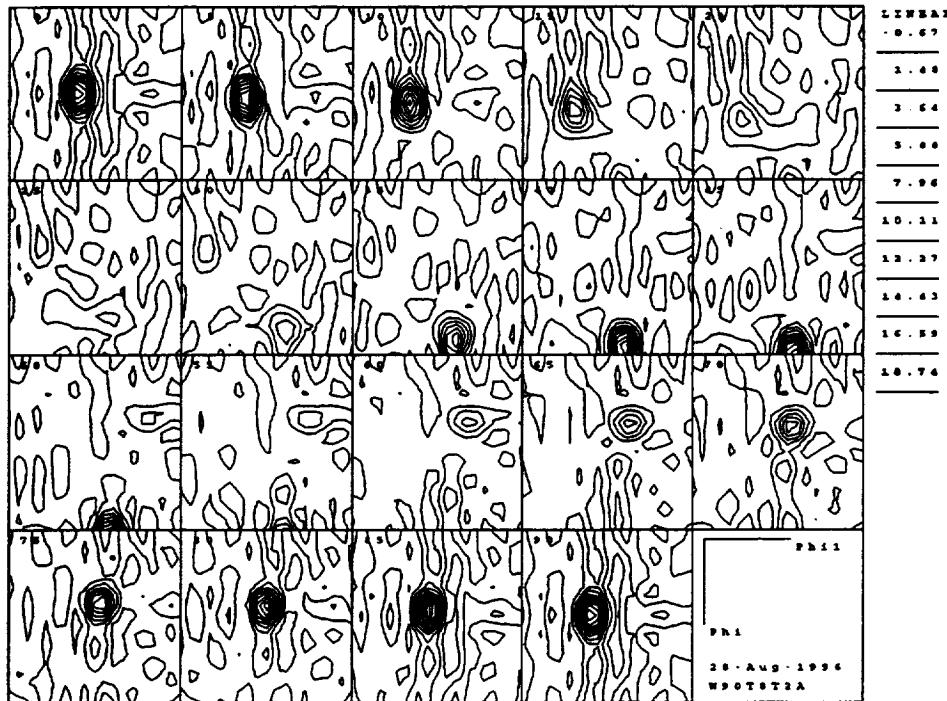


Figure 79.
Partial pole figures for 2090-T8 plate @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

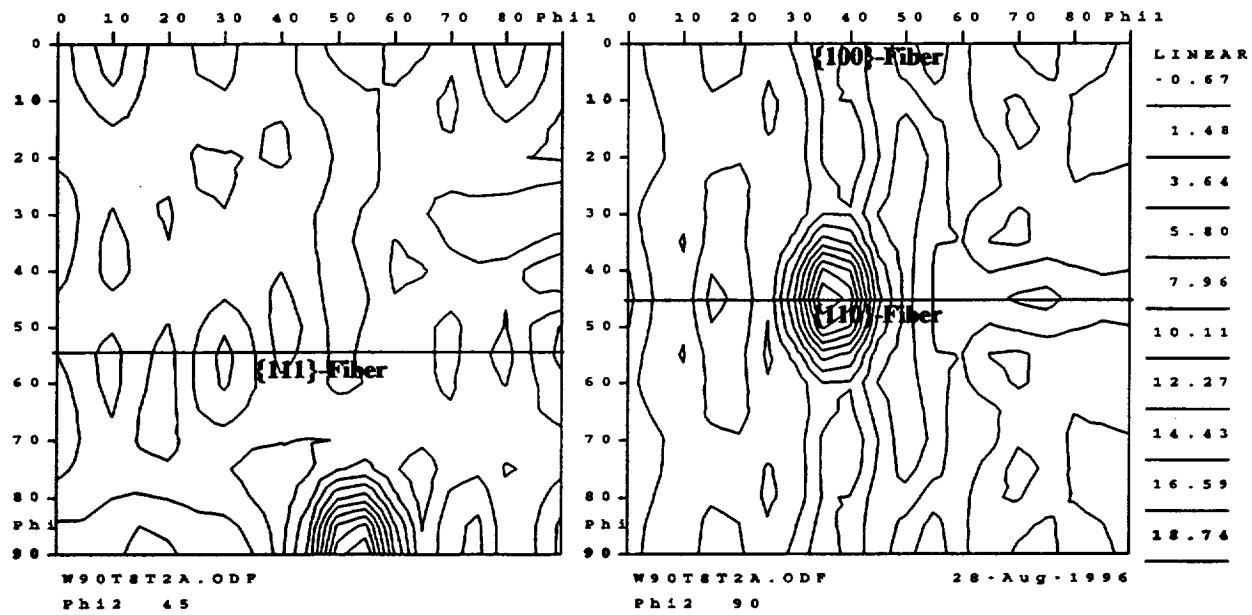


Figure 80. CODF sections for 2090-T8 plate @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

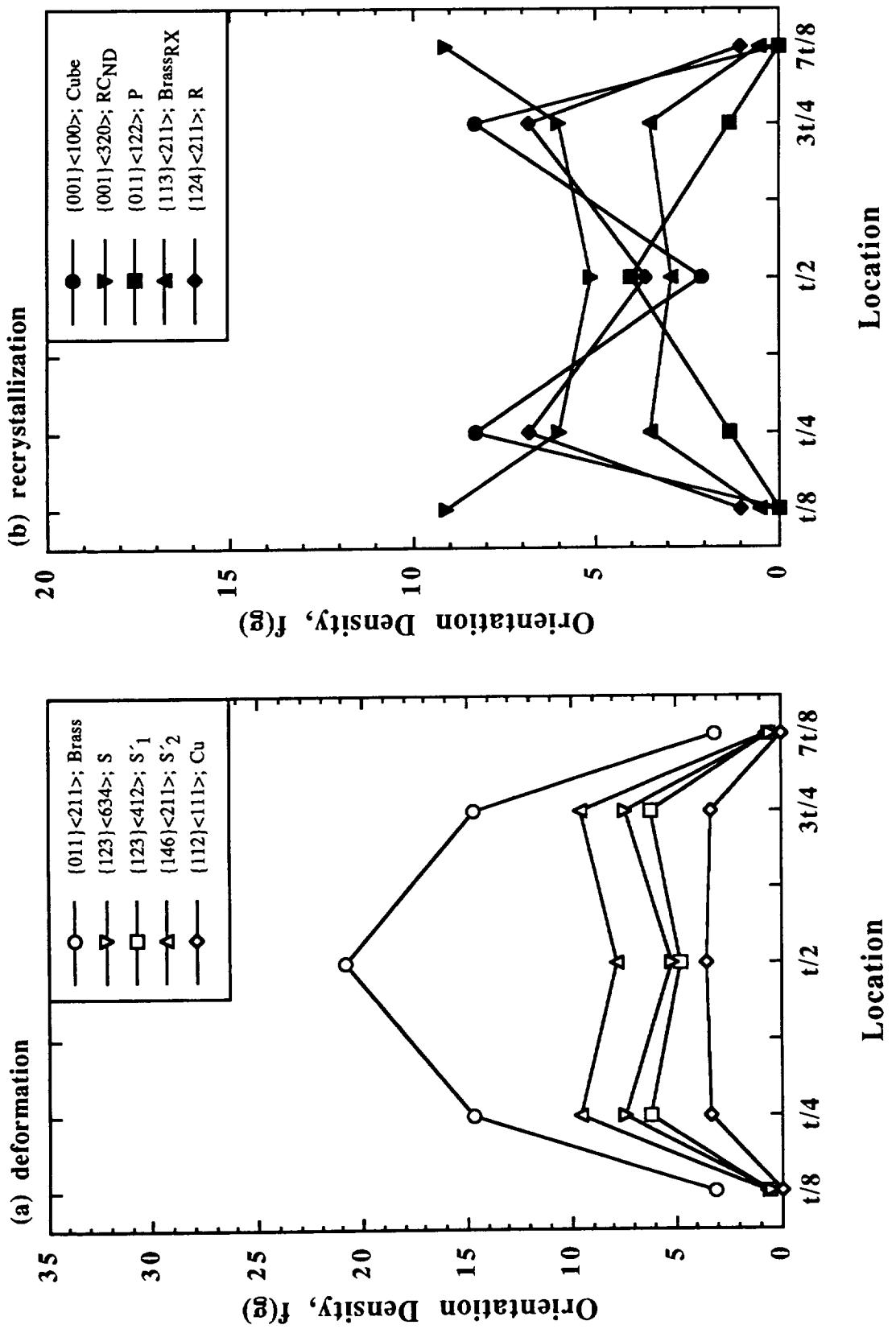


Figure 81. Orientation density, $f(g)$, as a function of location through the cross-section for the 2090-T8 plate:
(a) Deformation-related components; (b) Recrystallization-related components.

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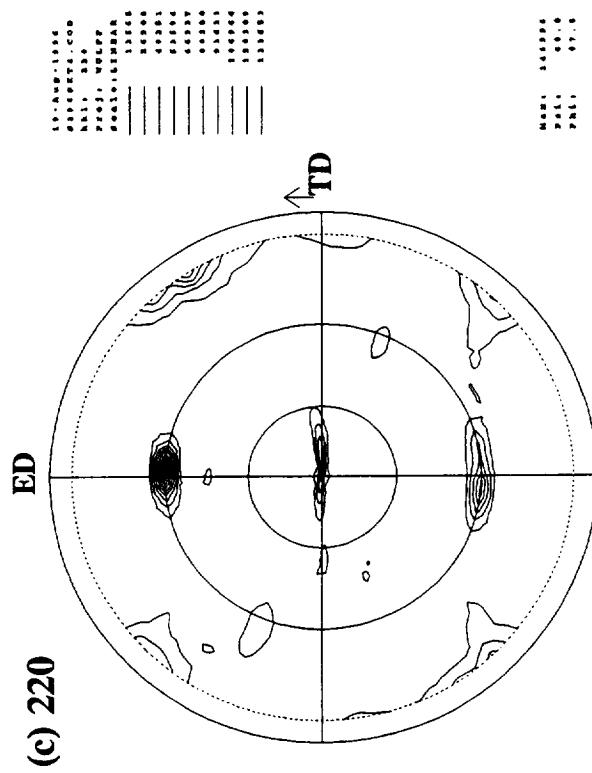
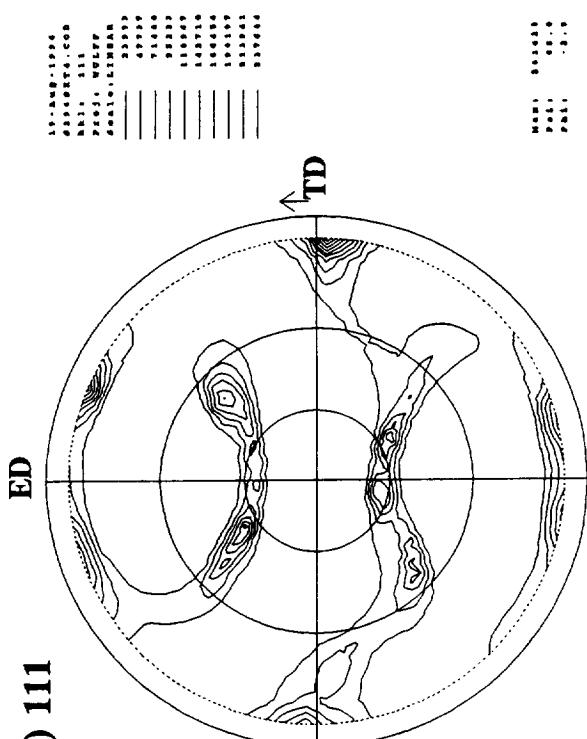
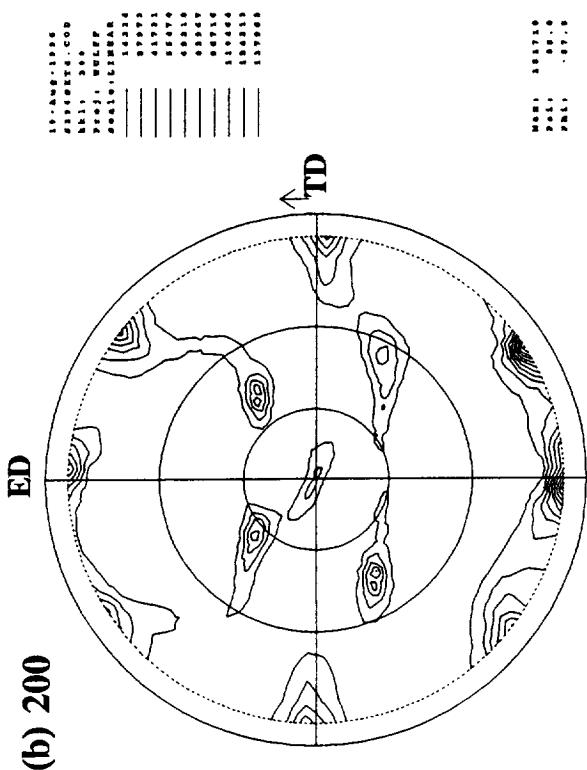
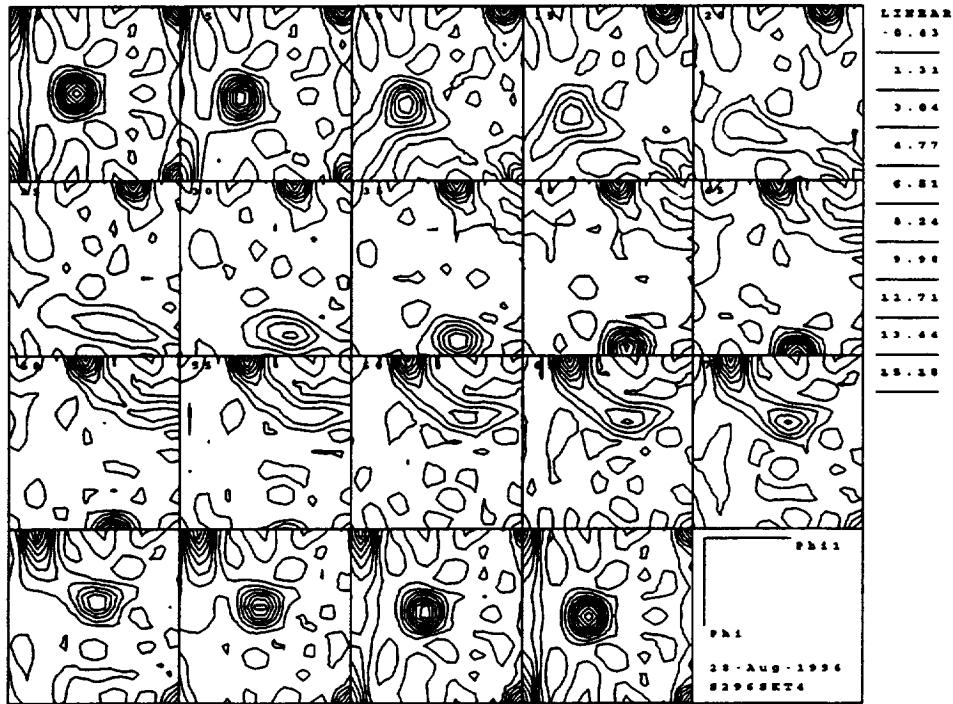


Figure 82.
Partial pole figures for the 2096-T3 extrusion in
the skin @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

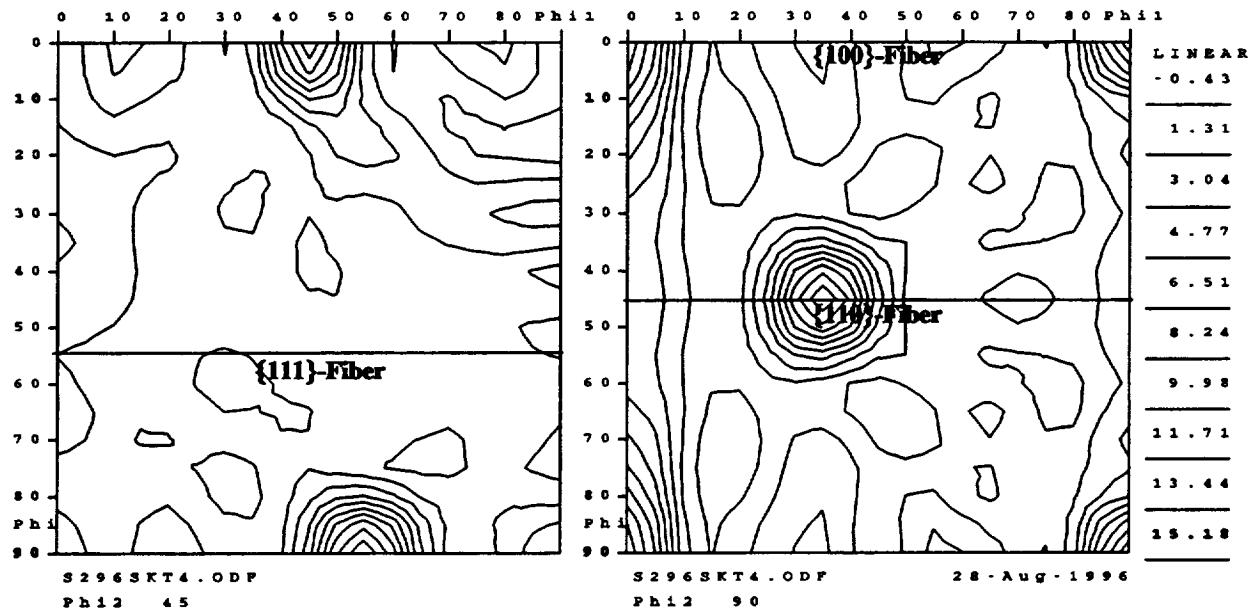


Figure 83. CODF sections for the 2096-T3 extrusion in the skin @ $t/4$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

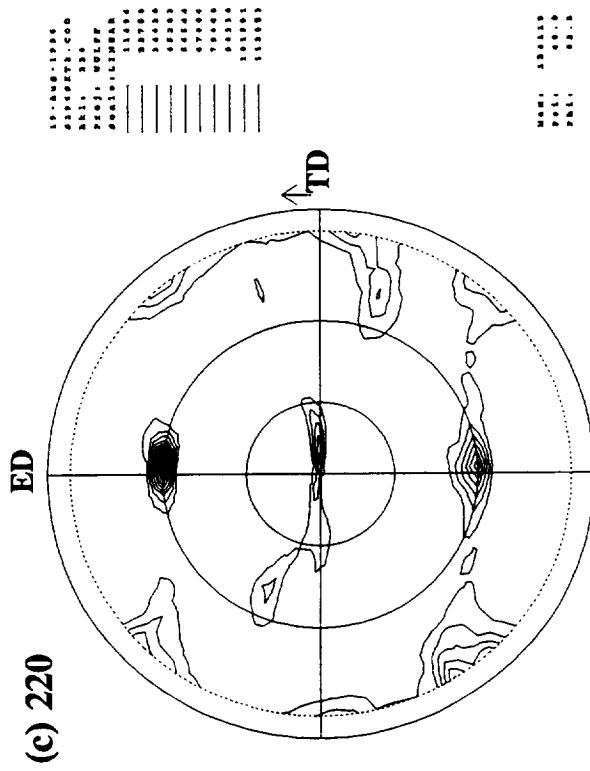
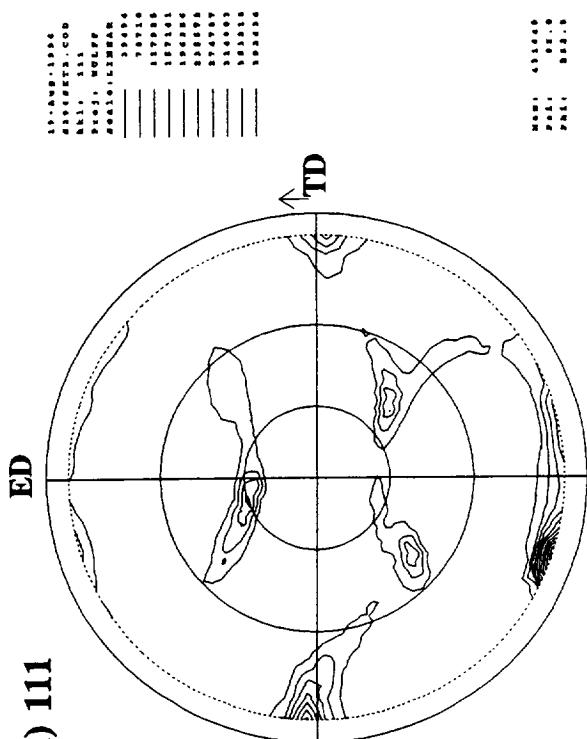
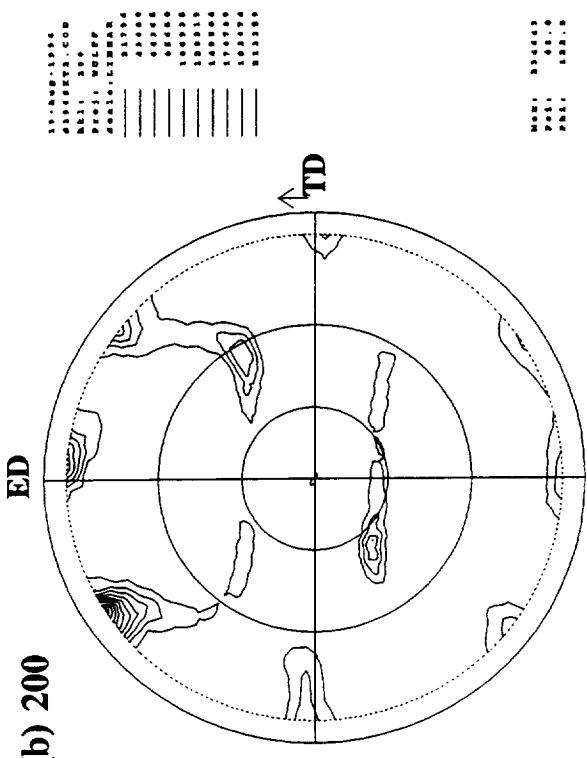
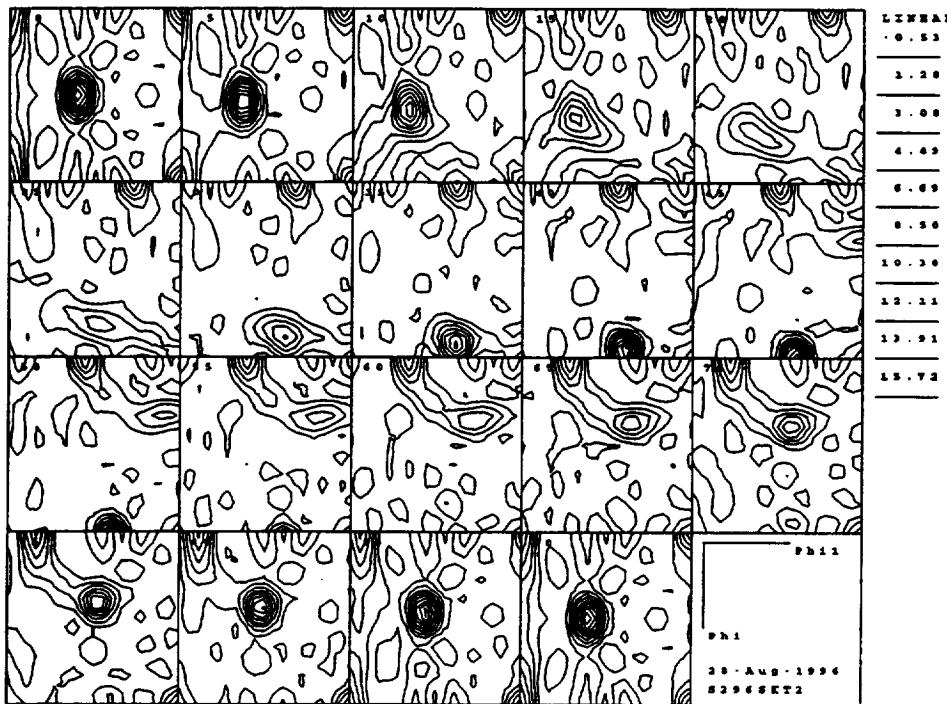


Figure 84.
Partial pole figures for the 2096-T3 extrusion in
the skin @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

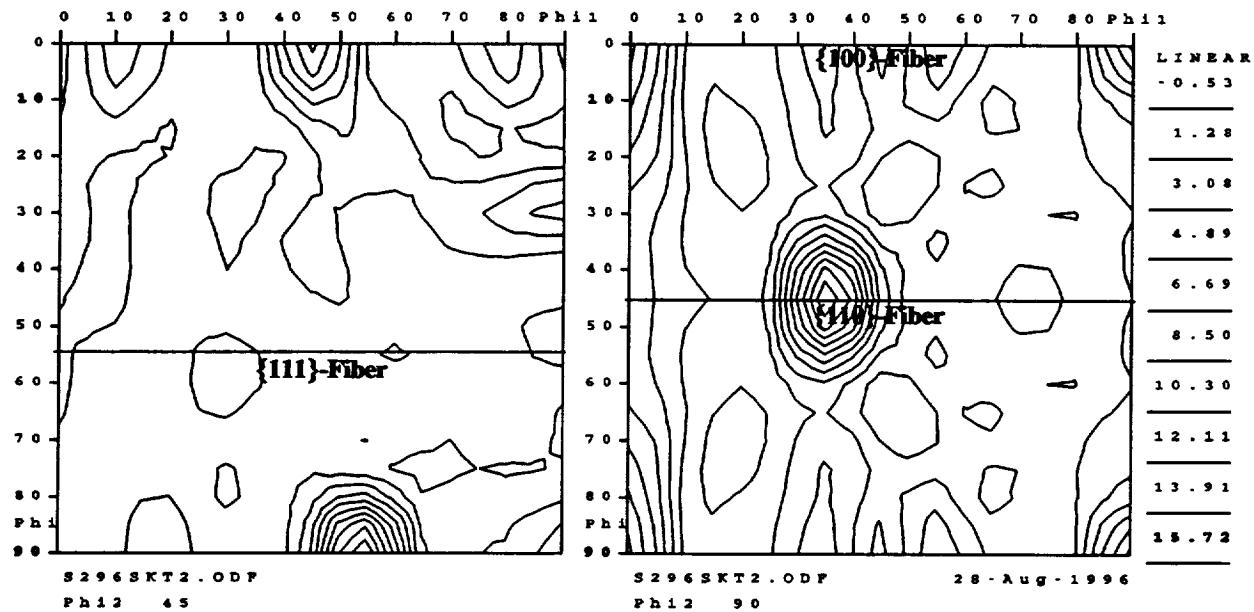


Figure 85. CODF sections for the 2096-T3 extrusion in the skin @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

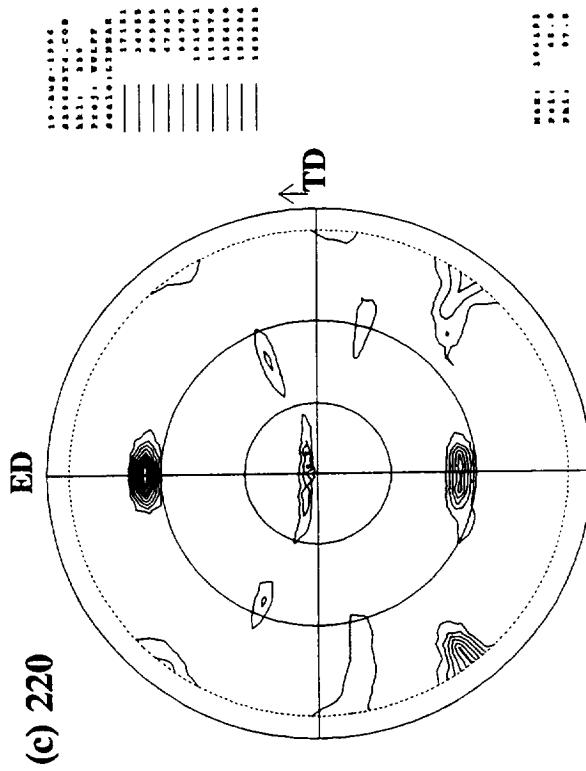
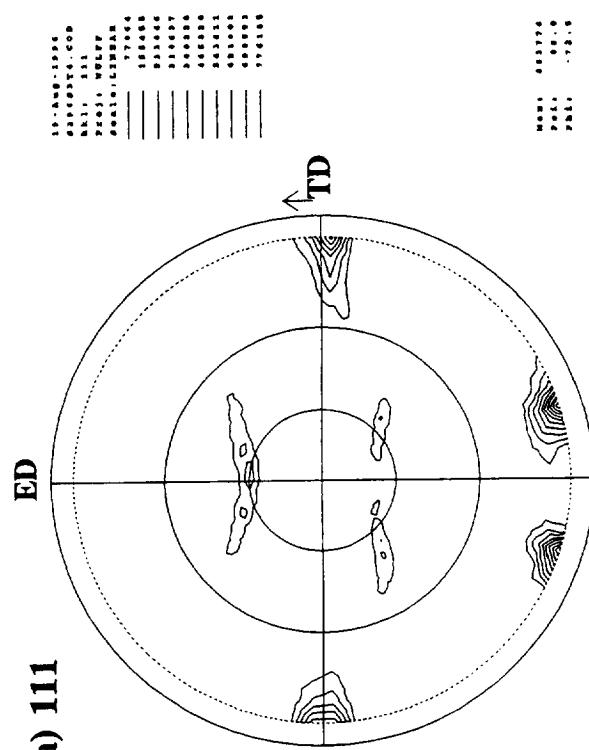
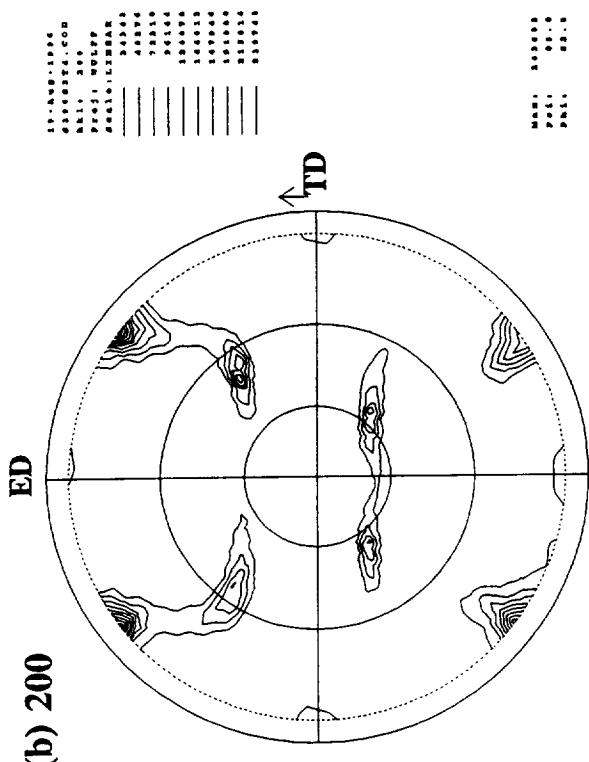
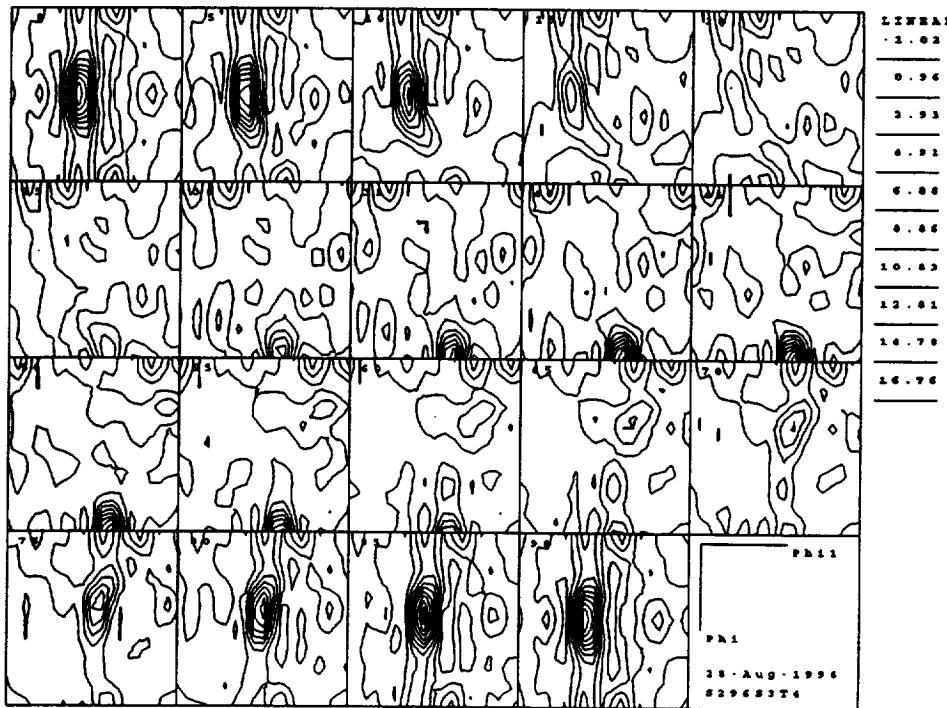


Figure 86.
Partial pole figures for the 2096-T3 extrusion in
the skin @ $3t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

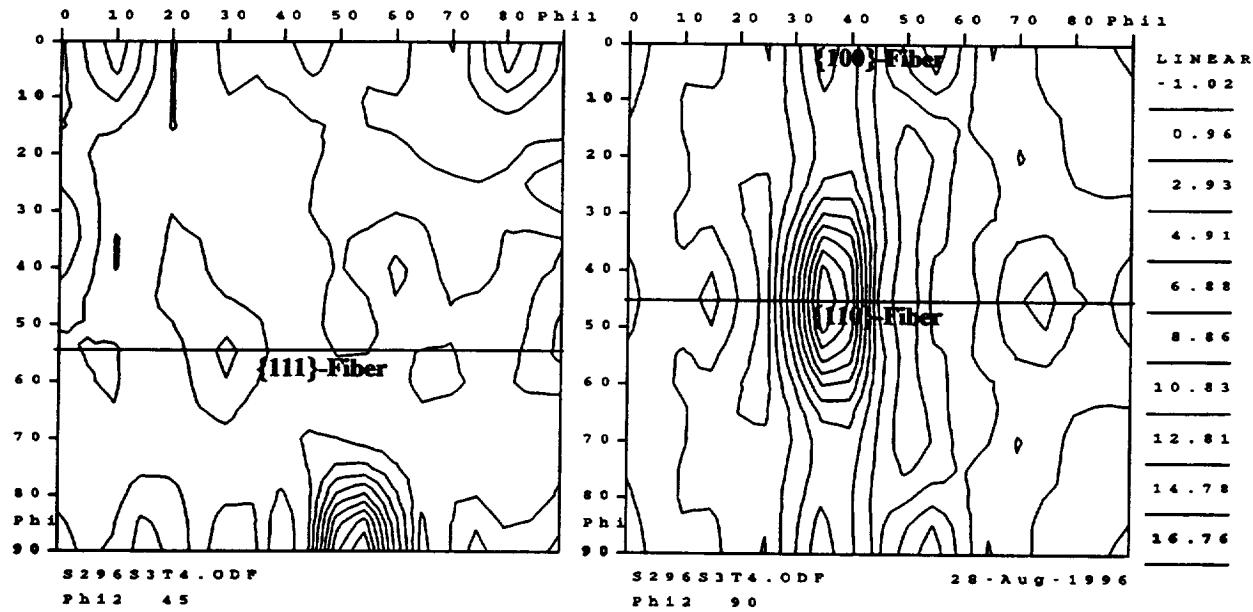


Figure 87. CODF sections for the 2096-T3 extrusion in the skin @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

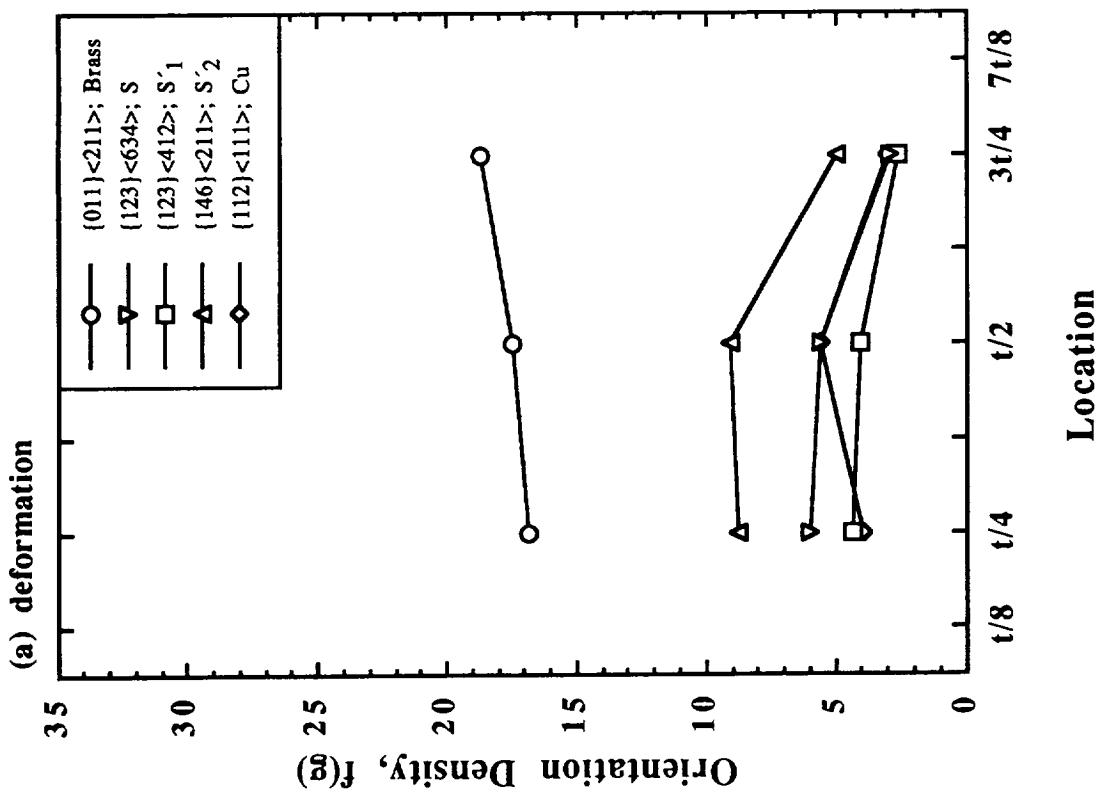


Figure 88. Orientation density, $f(g)$, as a function of location through the cross-section for the 2096-T3 extrusion in the skin region: (a) Deformation-related components; (b) Recrystallization-related components.

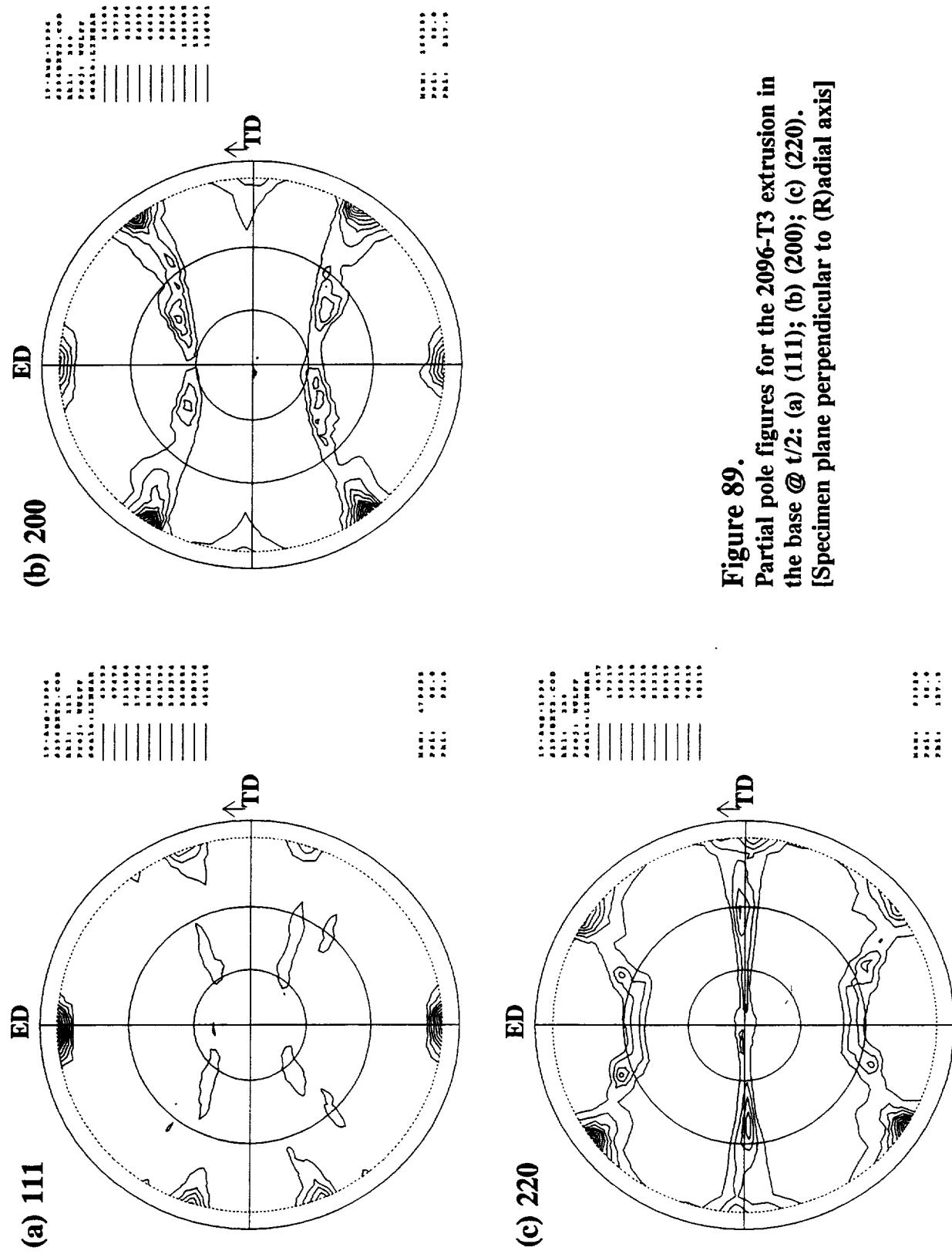
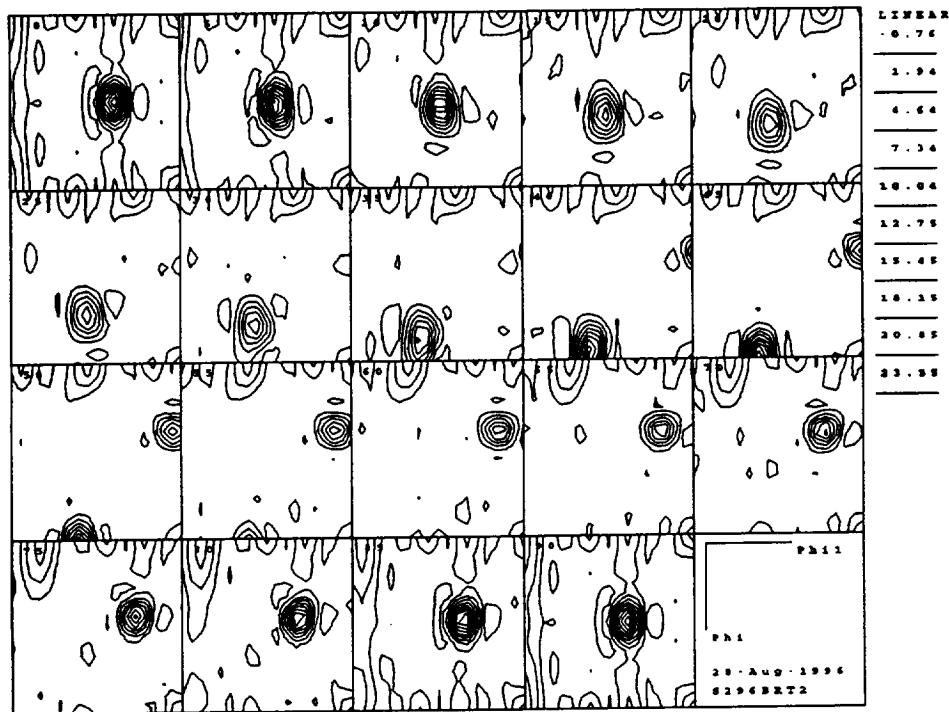


Figure 89.
Partial pole figures for the 2096-T3 extrusion in
the base @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

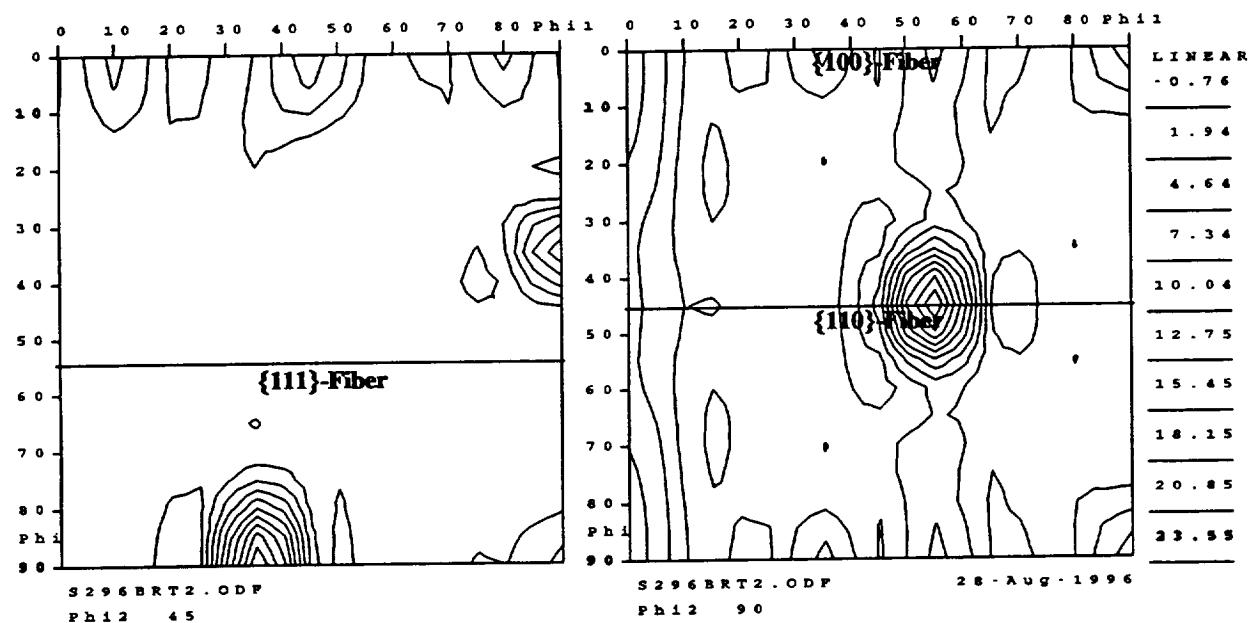


Figure 90. CODF sections for the 2096-T3 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

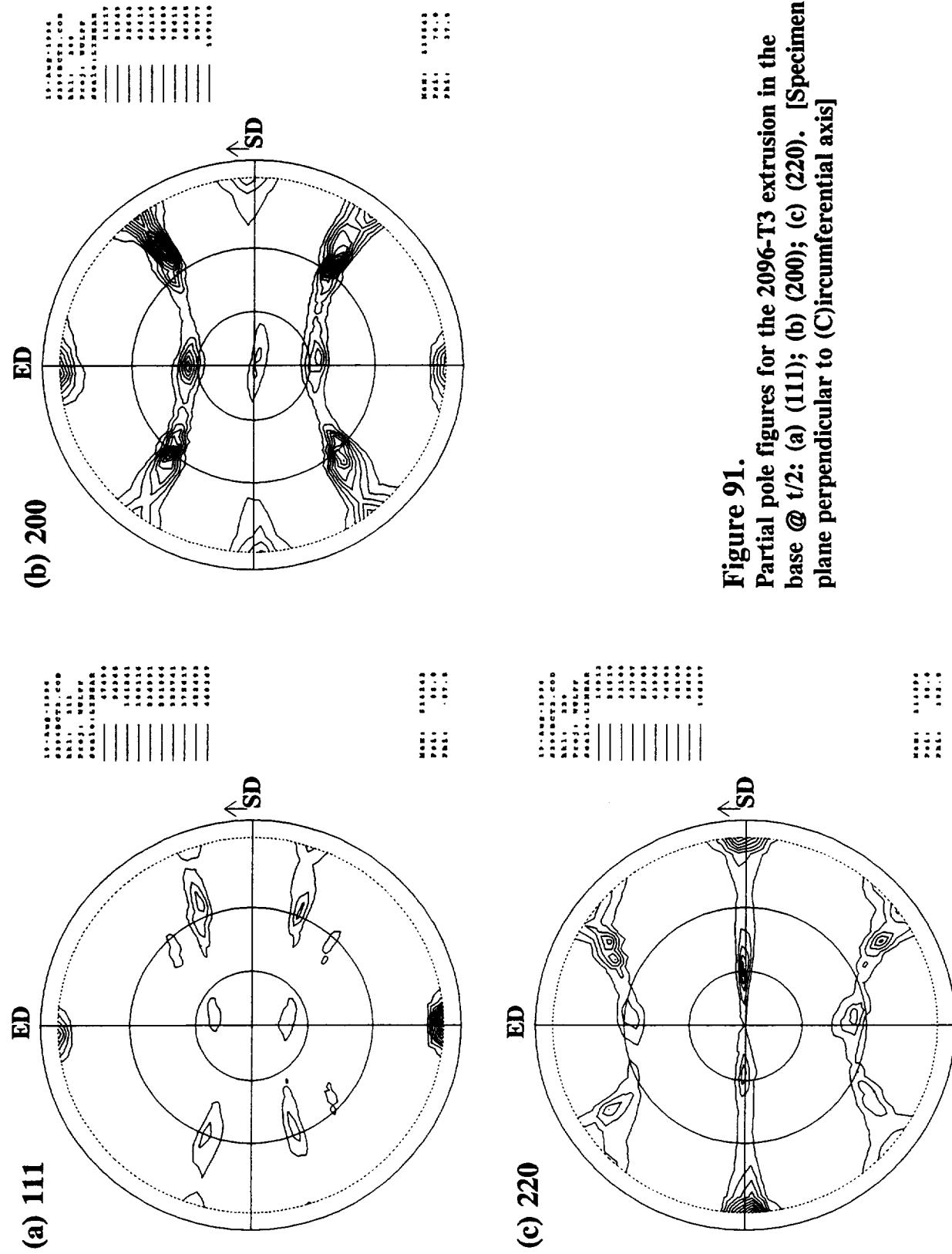
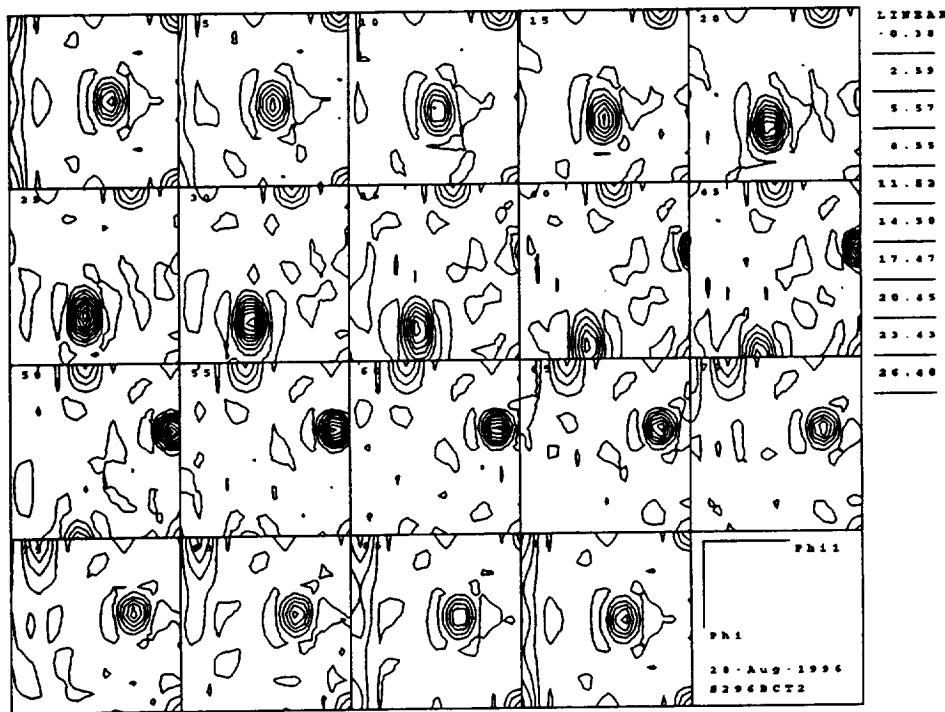


Figure 91.
Partial pole figures for the 2096-T3 extrusion in the
base @ $t/2$: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

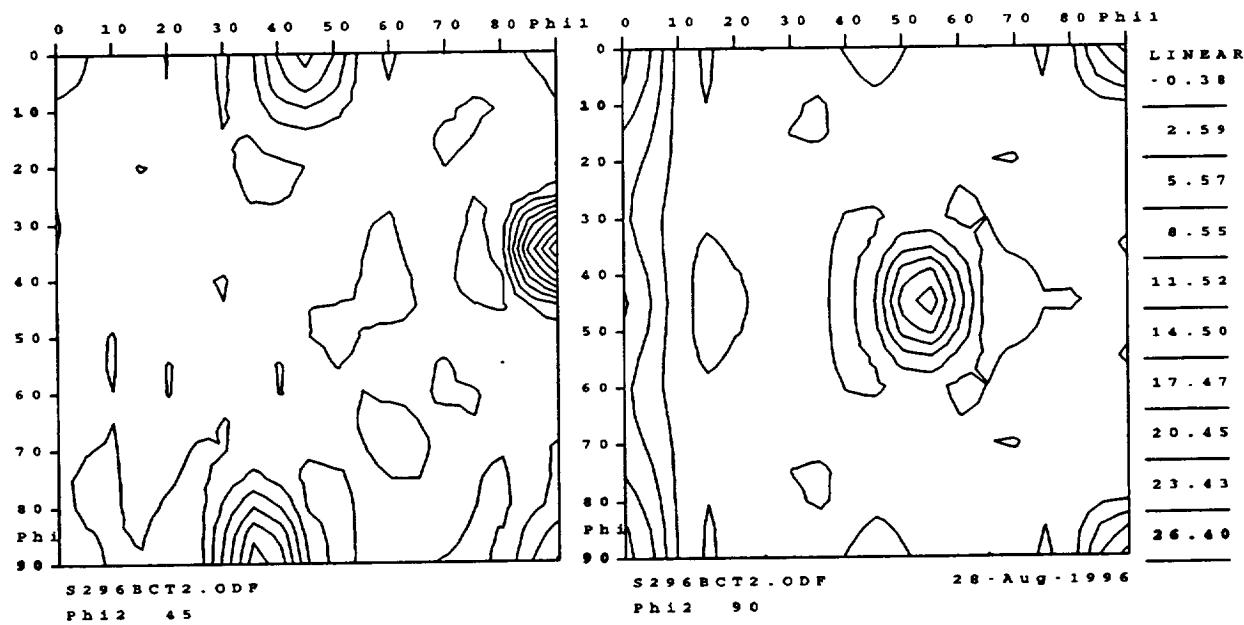


Figure 92. CODF sections for the 2096-T3 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

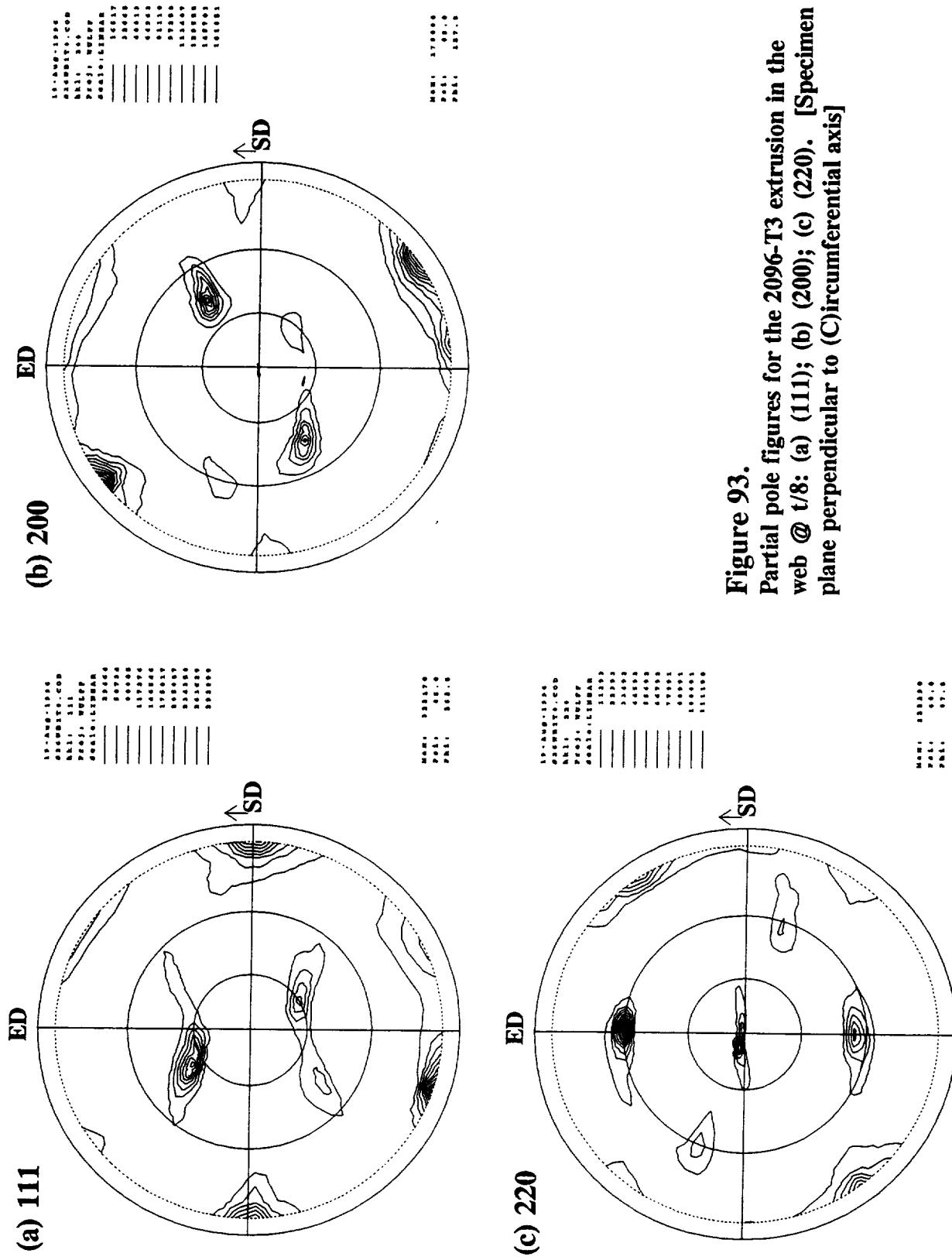
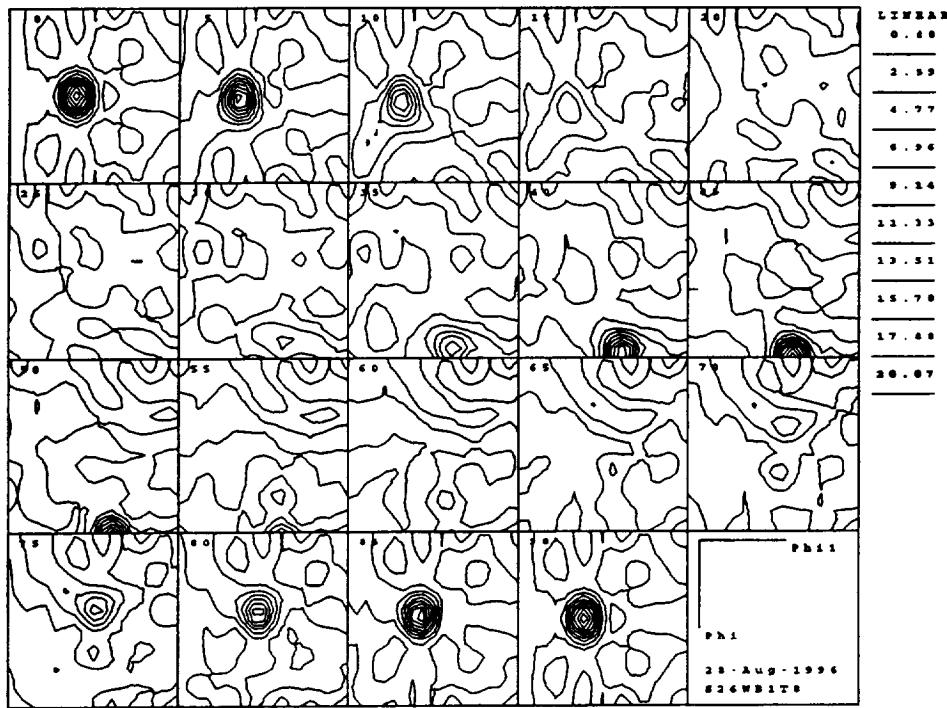


Figure 93.
Partial pole figures for the 2096-T3 extrusion in the
web @ t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

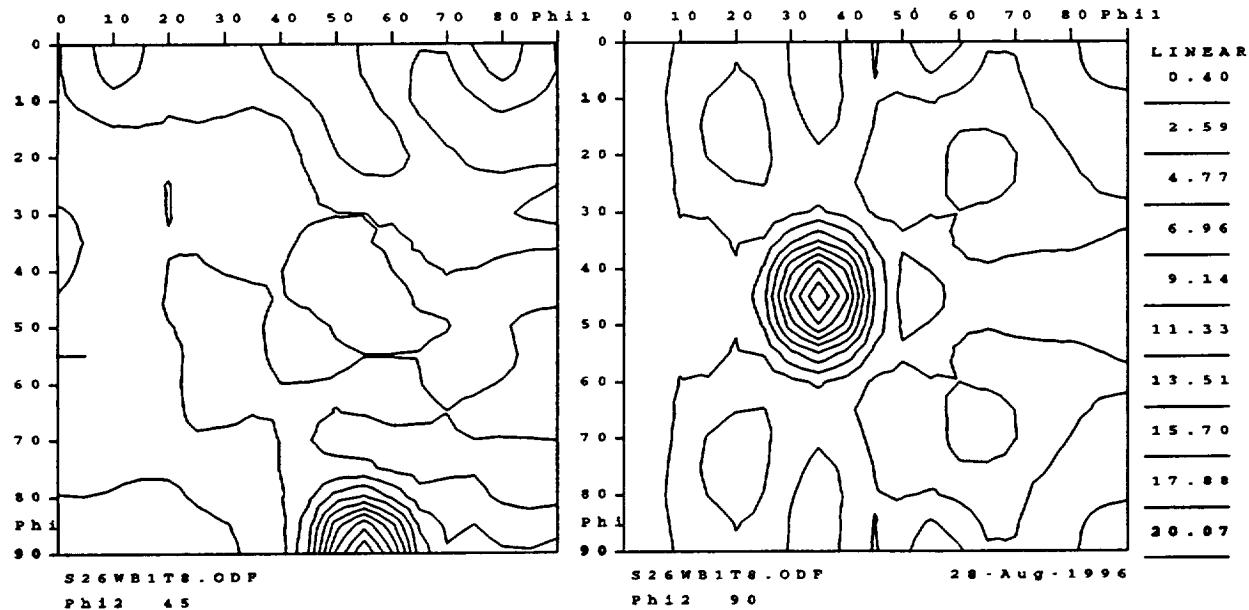


Figure 94. CODF sections for the 2096-T3 extrusion in the web @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

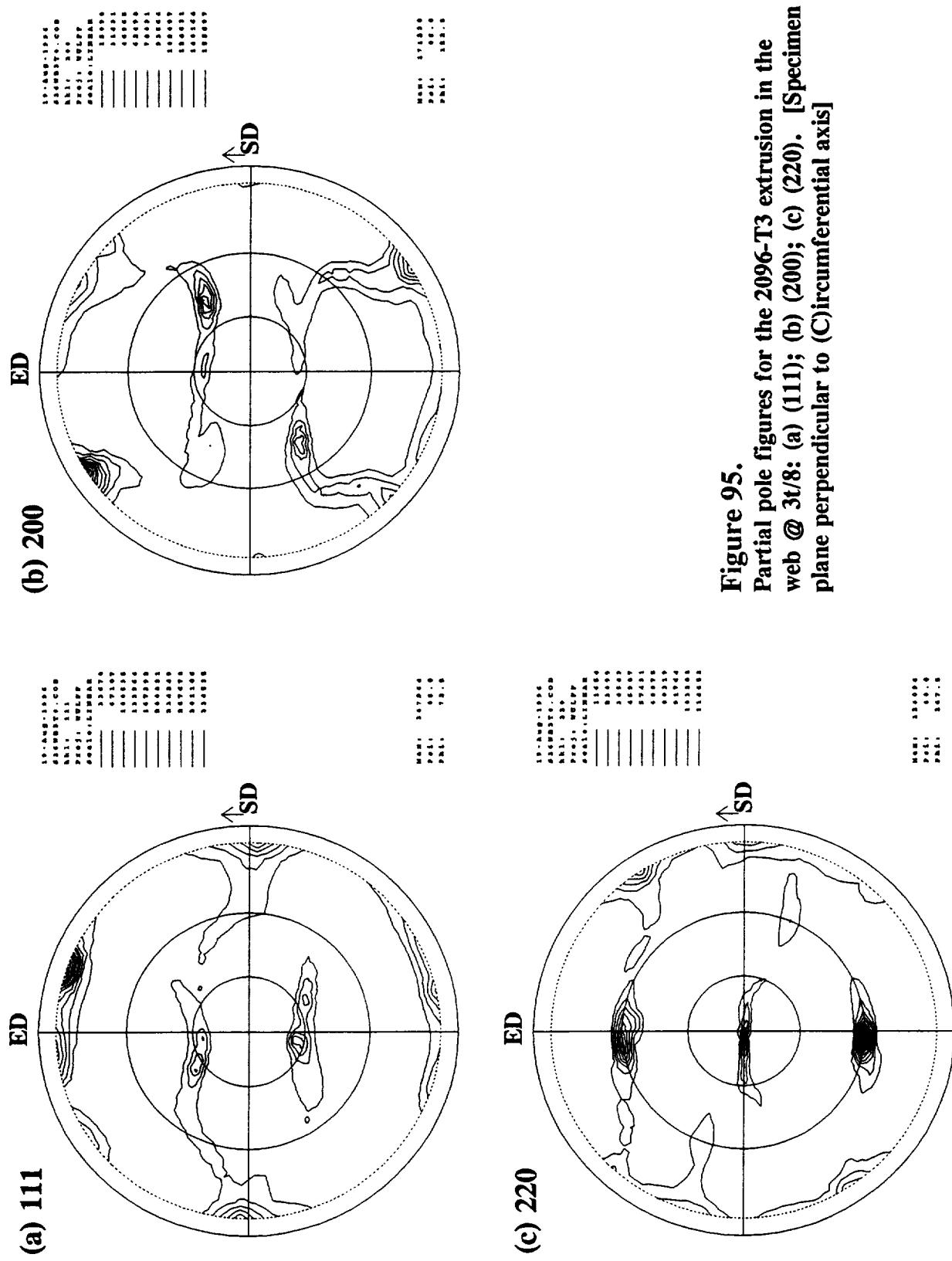
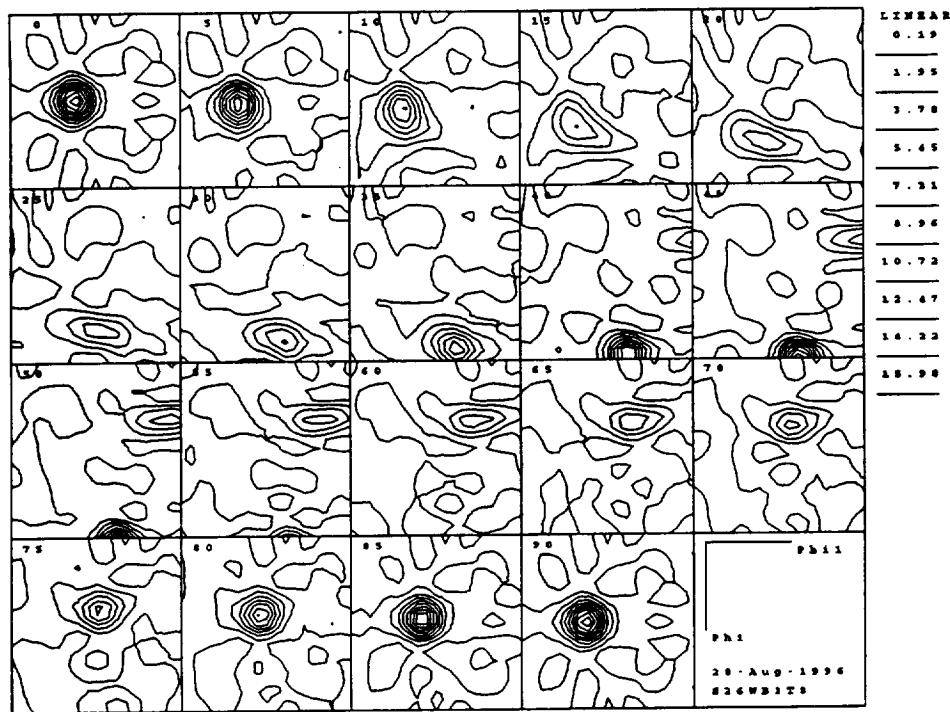


Figure 95.
Partial pole figures for the 2096-T3 extrusion in the
web @ 3t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

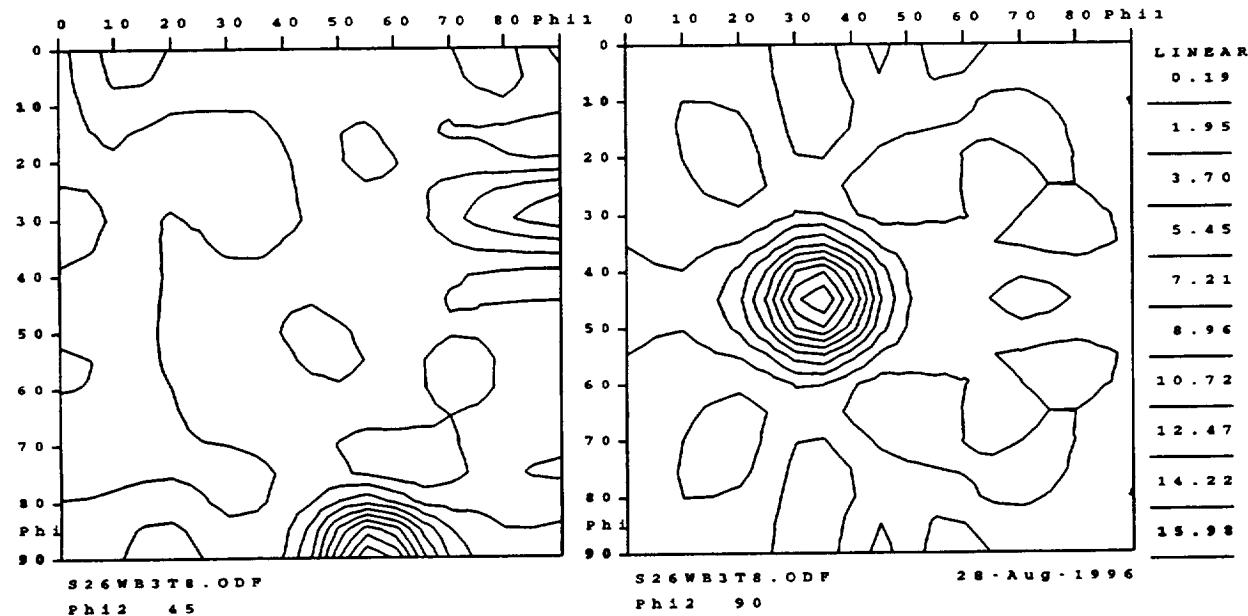


Figure 96. CODF sections for the 2096-T3 extrusion in the web @ 3t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

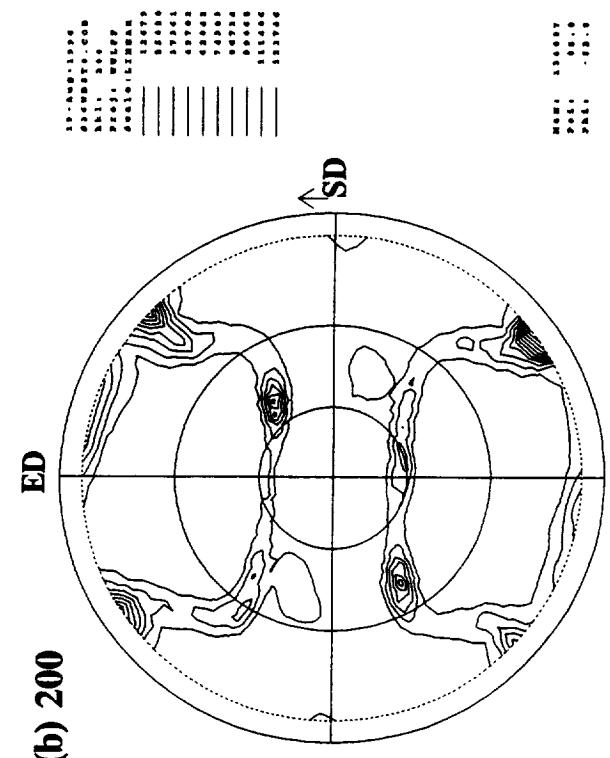
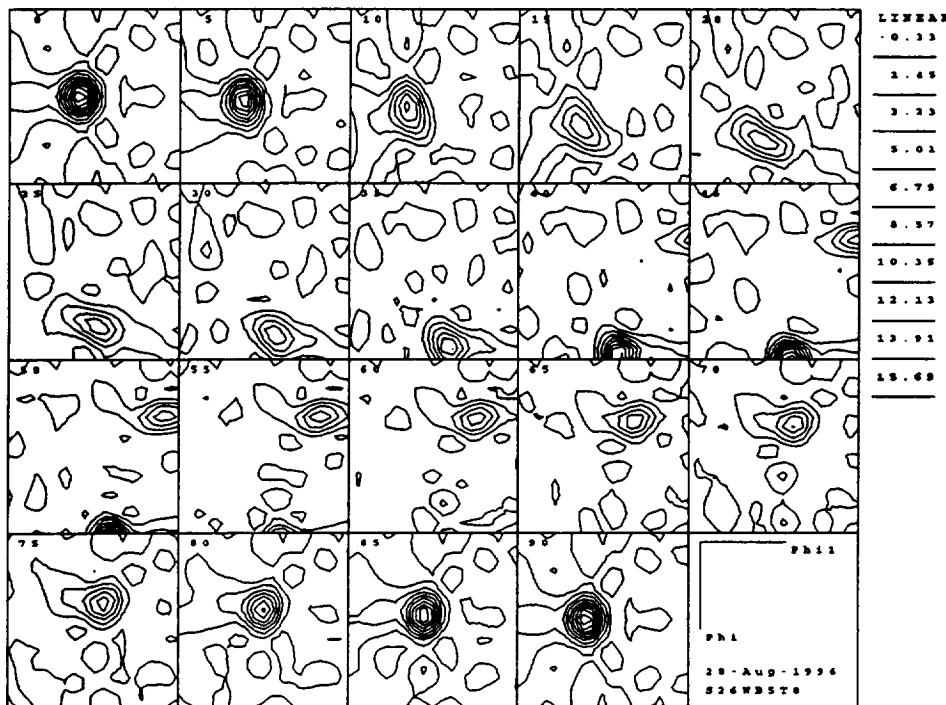


Figure 97.
Partial pole figures for the 2096-T3 extrusion in the
web @ 5t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

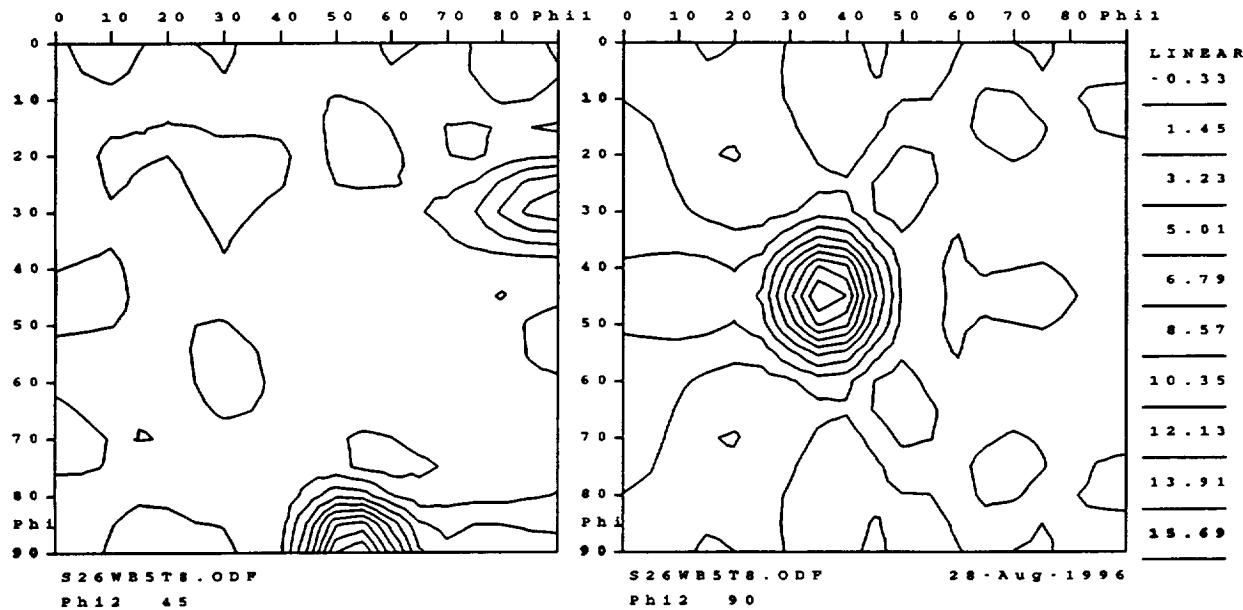


Figure 98. CODF sections for the 2096-T3 extrusion in the web @ 5t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

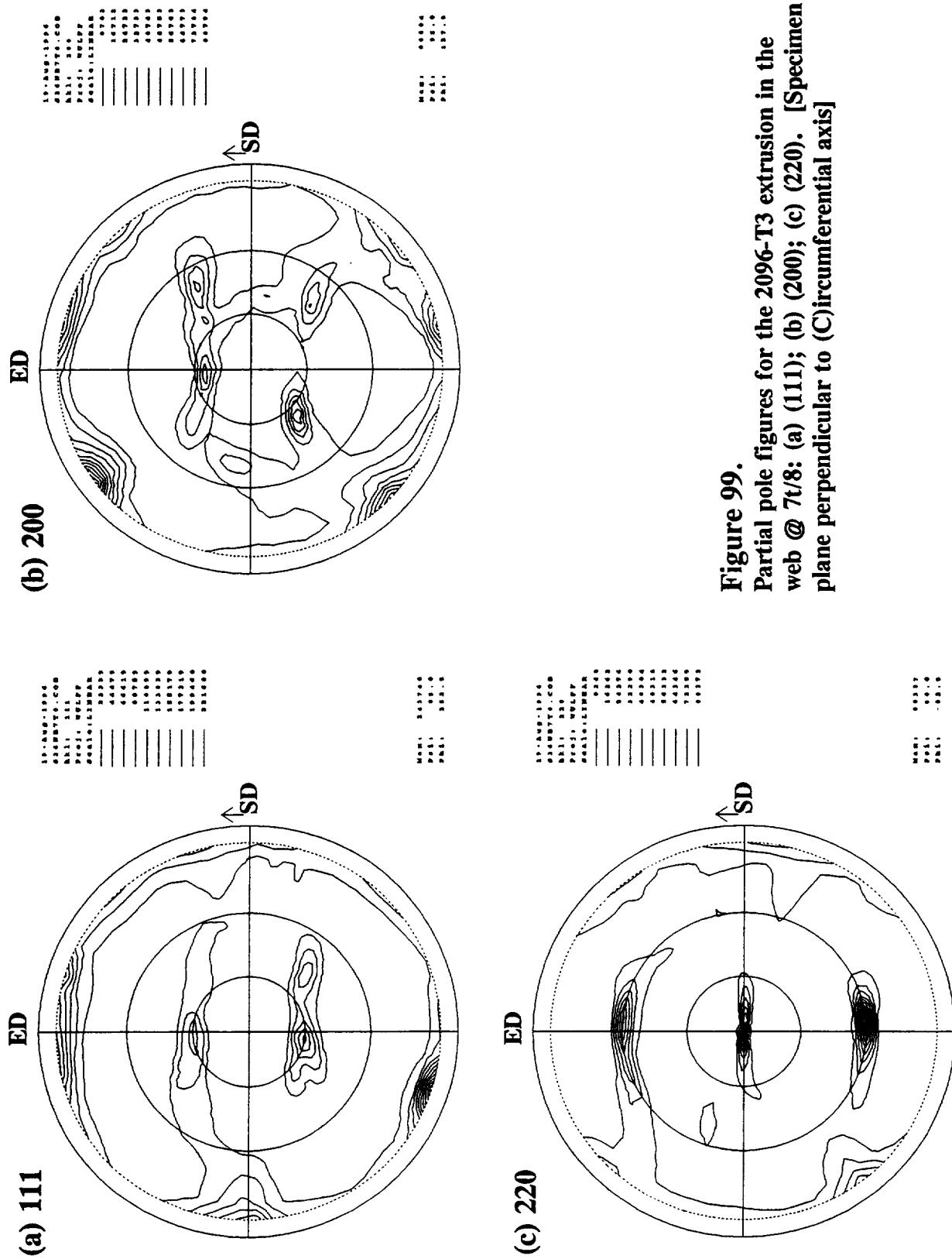
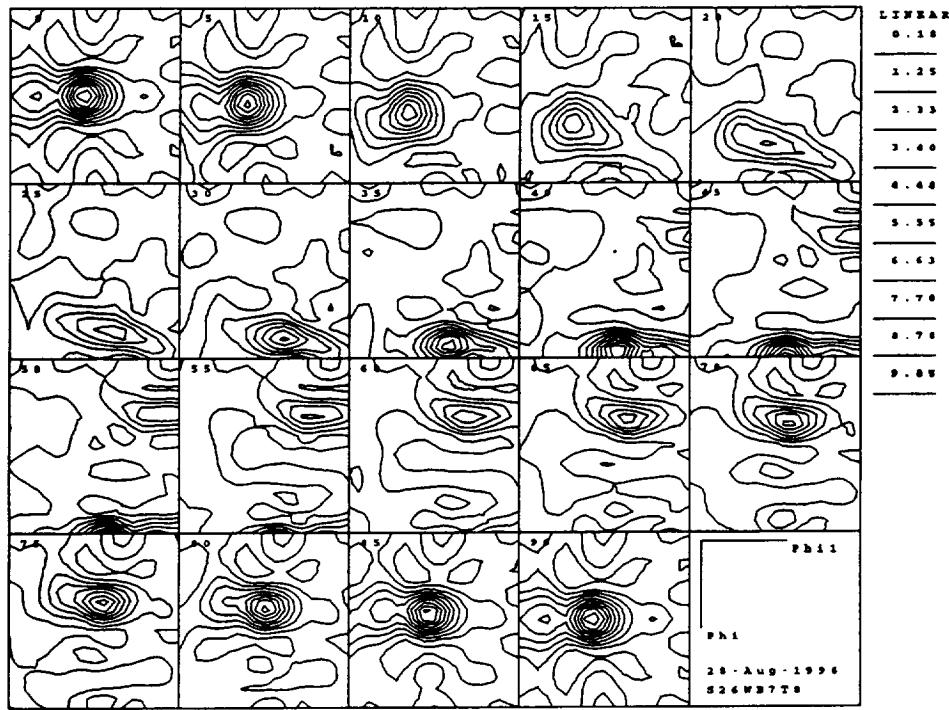


Figure 99.
Partial pole figures for the 2096-T3 extrusion in the
web @ 7/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

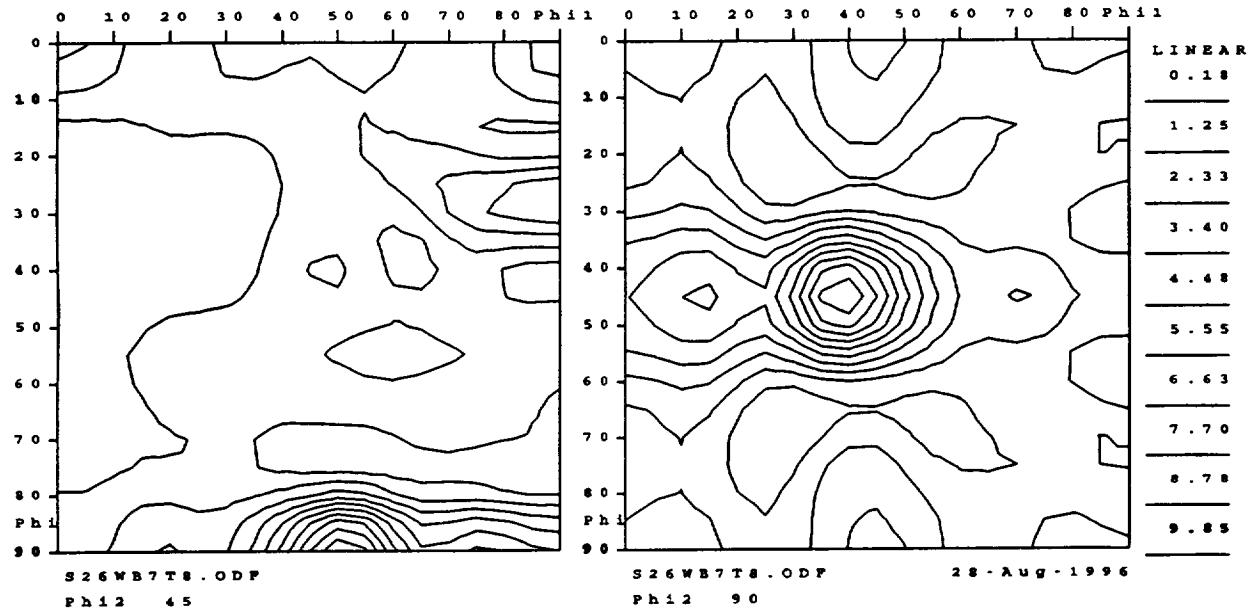


Figure 100. CODF sections for the 2096-T3 extrusion in the web @ 7t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

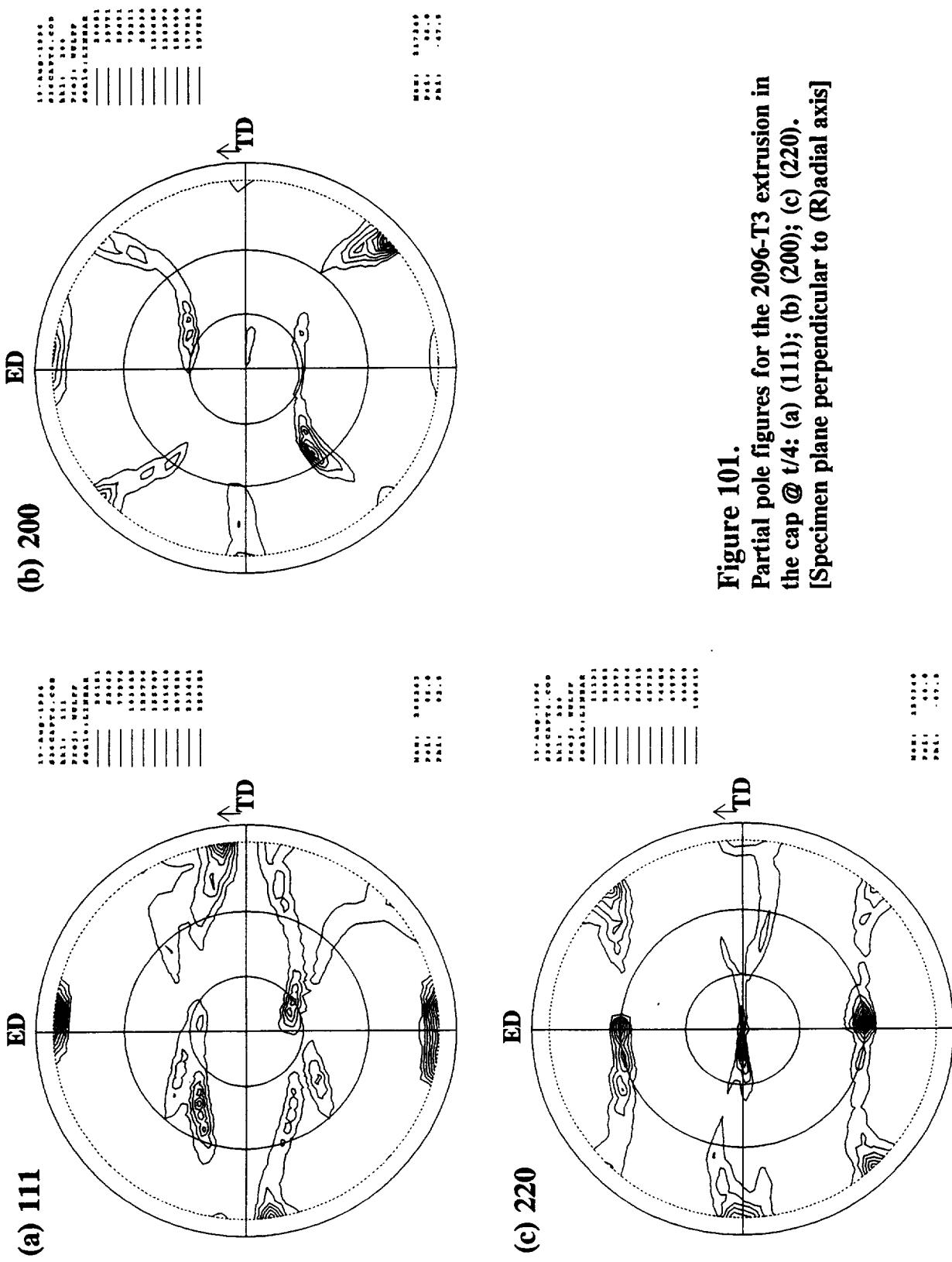
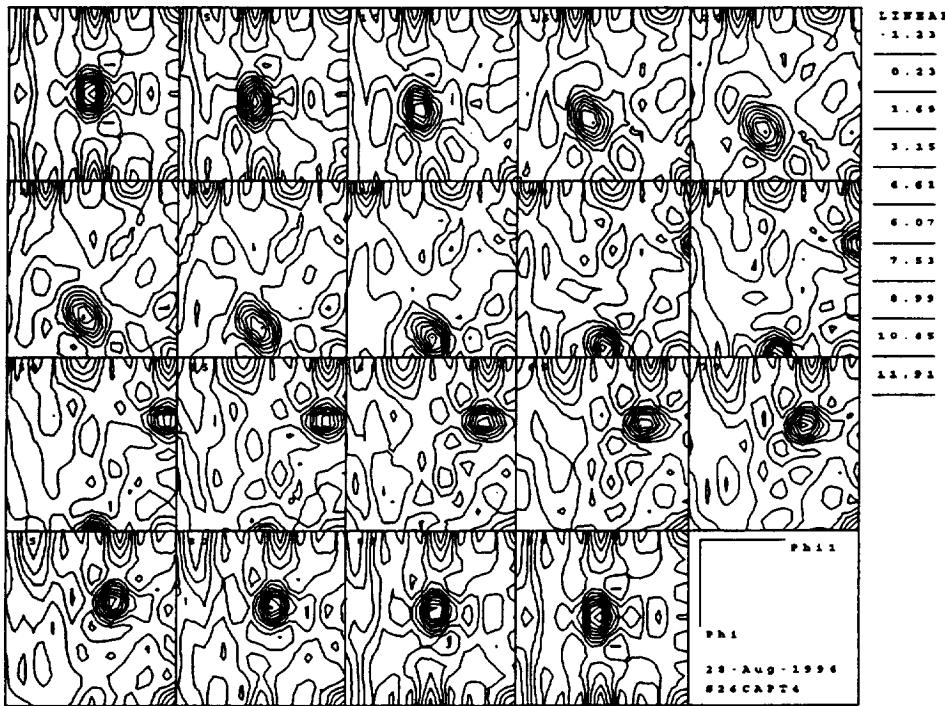


Figure 101.
Partial pole figures for the 2096-T3 extrusion in
the cap @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

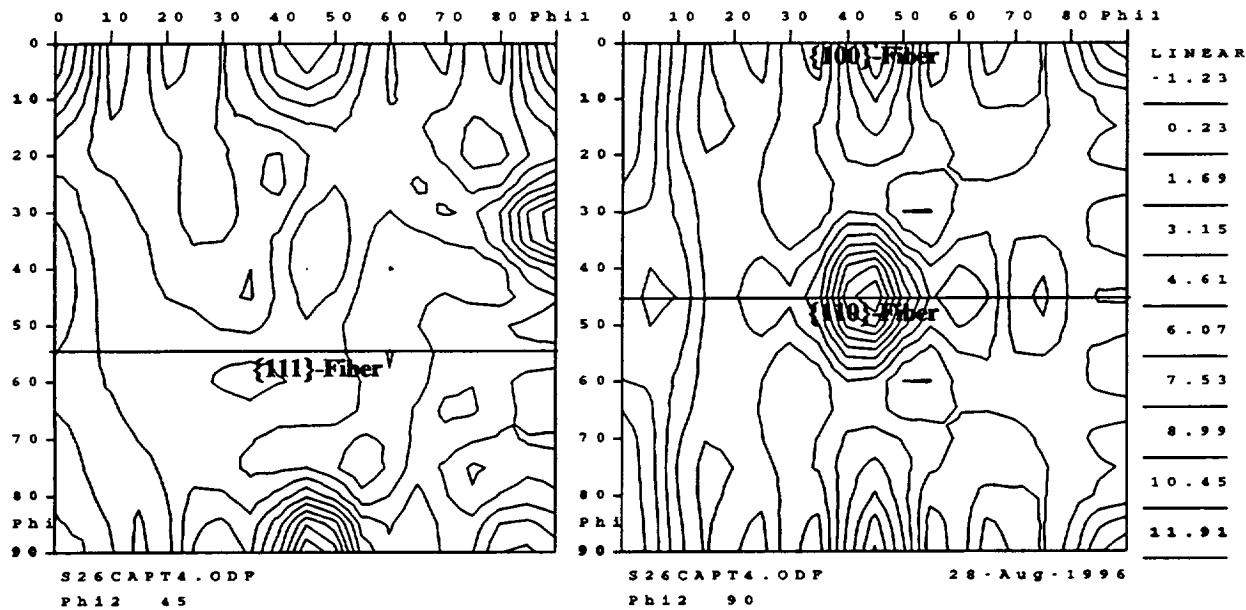


Figure 102. CODF sections for the 2096-T3 extrusion in the cap @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

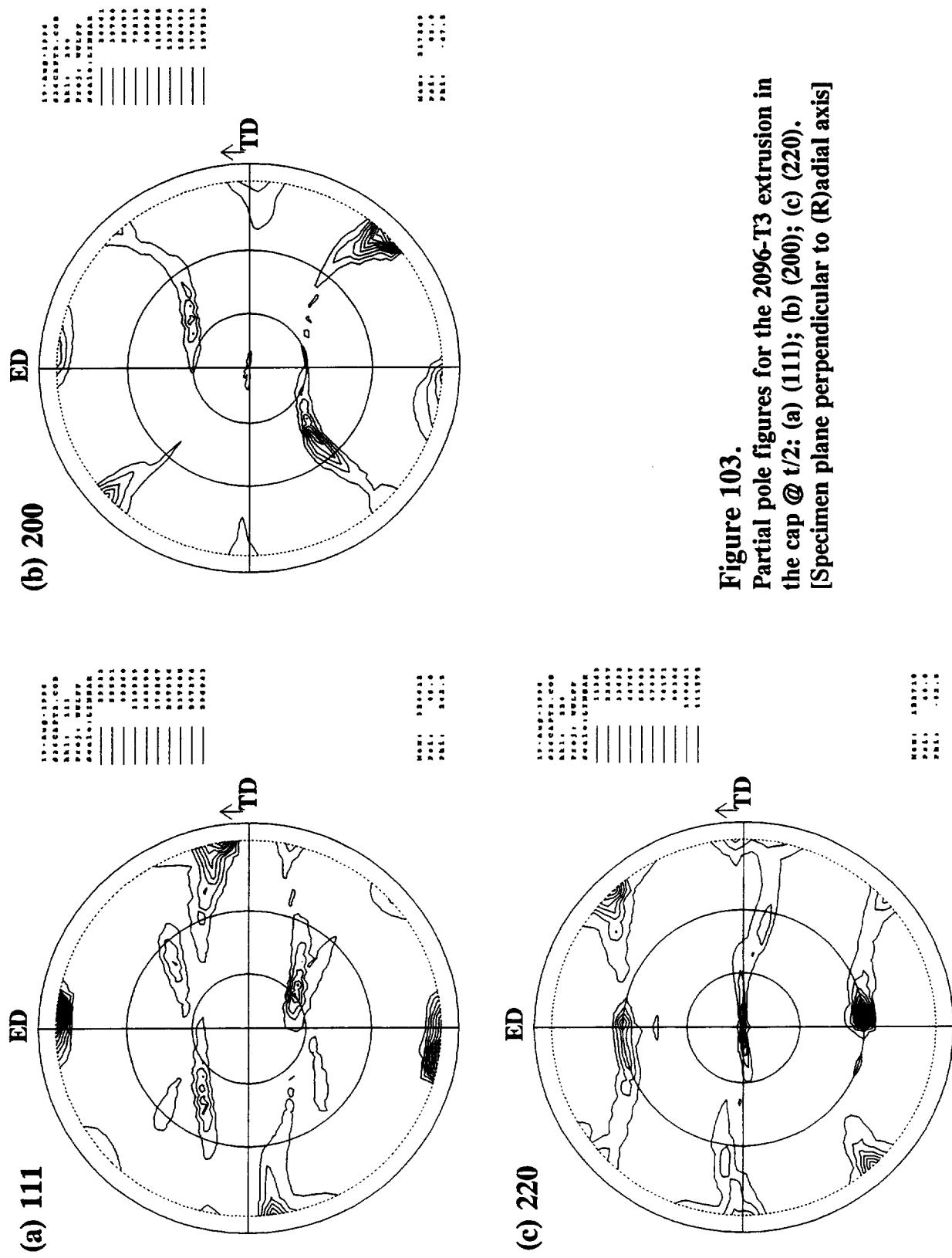
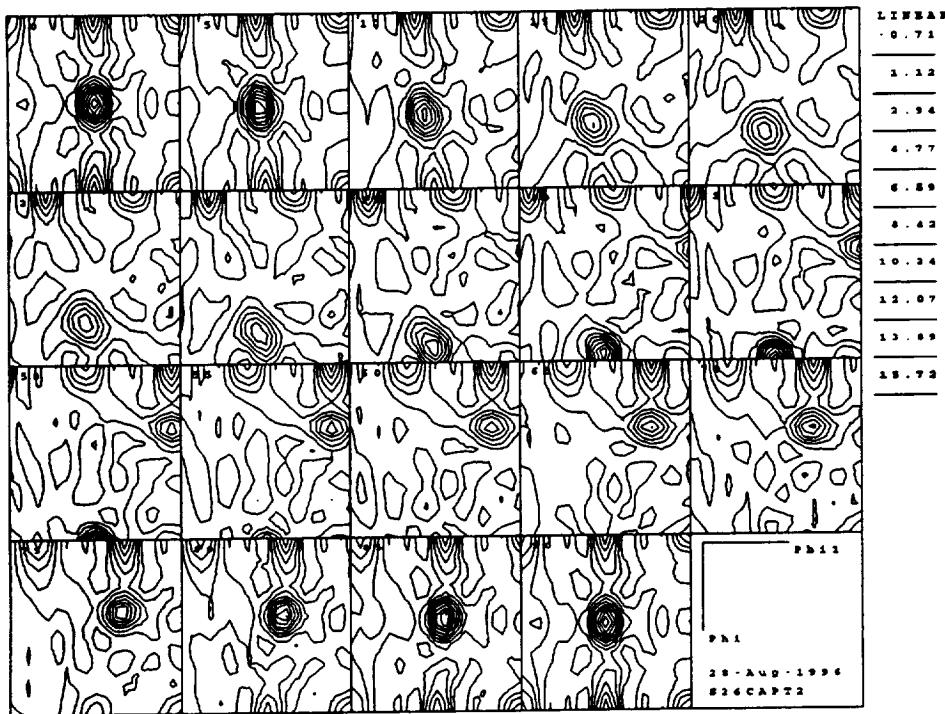


Figure 103.
Partial pole figures for the 2096-T3 extrusion in
the cap @ t/2: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

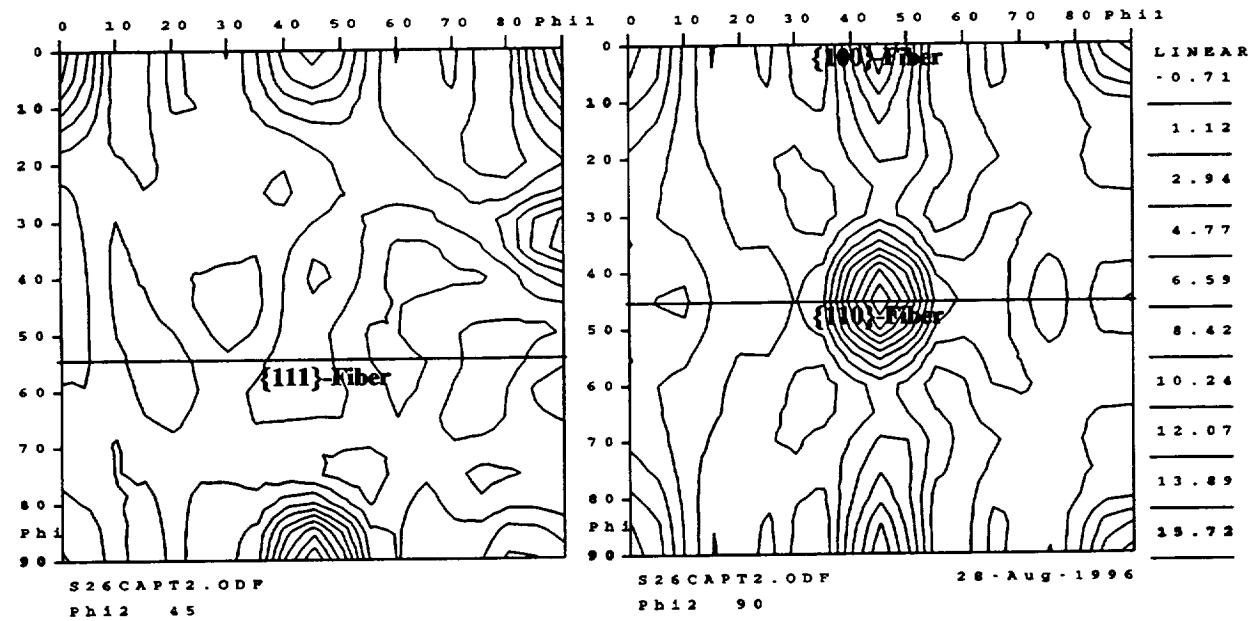


Figure 104. CODF sections for the 2096-T3 extrusion in the cap @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

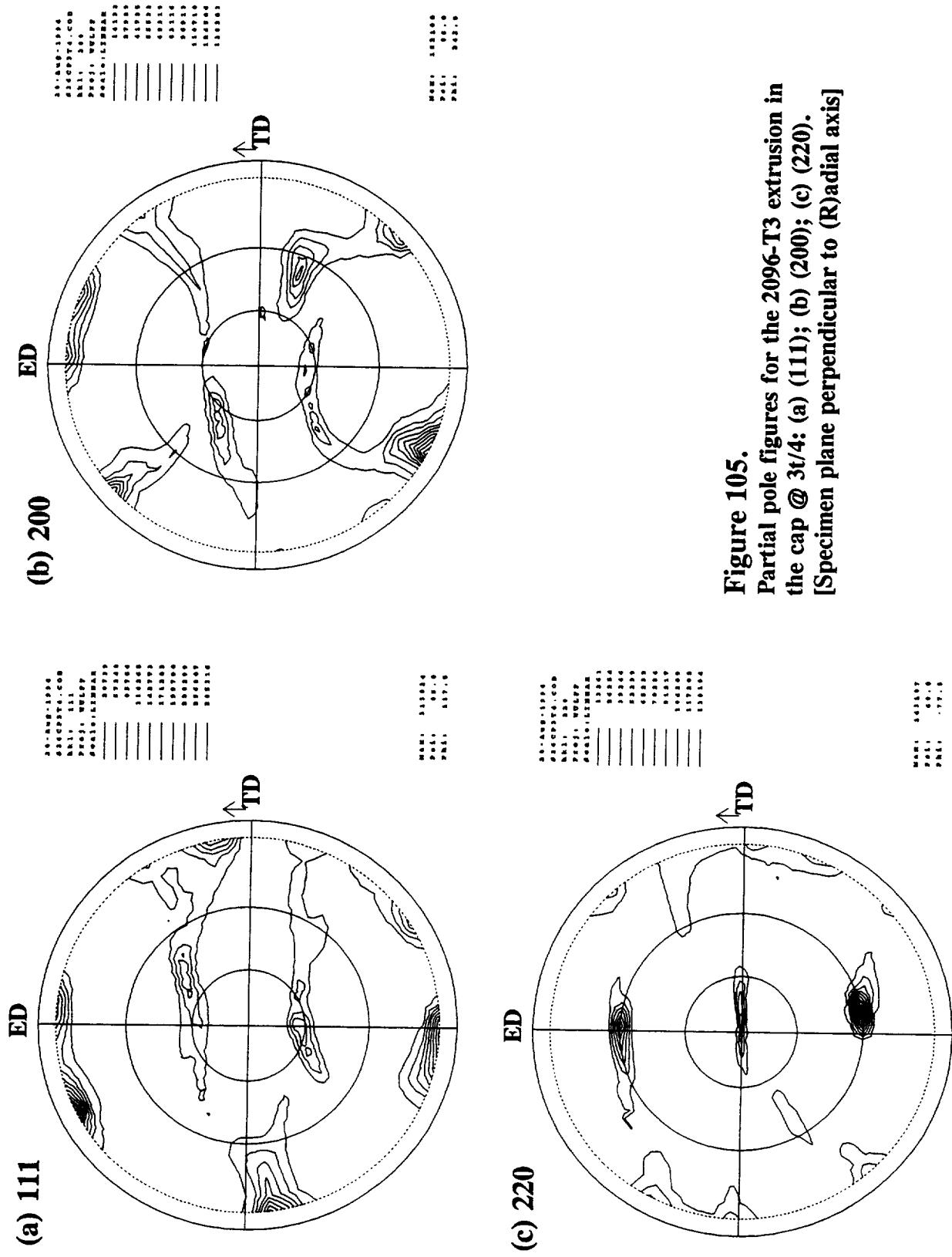


Figure 105.
Partial pole figures for the 2096-T3 extrusion in
the cap @ $3t/4$: (a) $\langle 111 \rangle$; (b) $\langle 200 \rangle$; (c) $\langle 220 \rangle$.
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

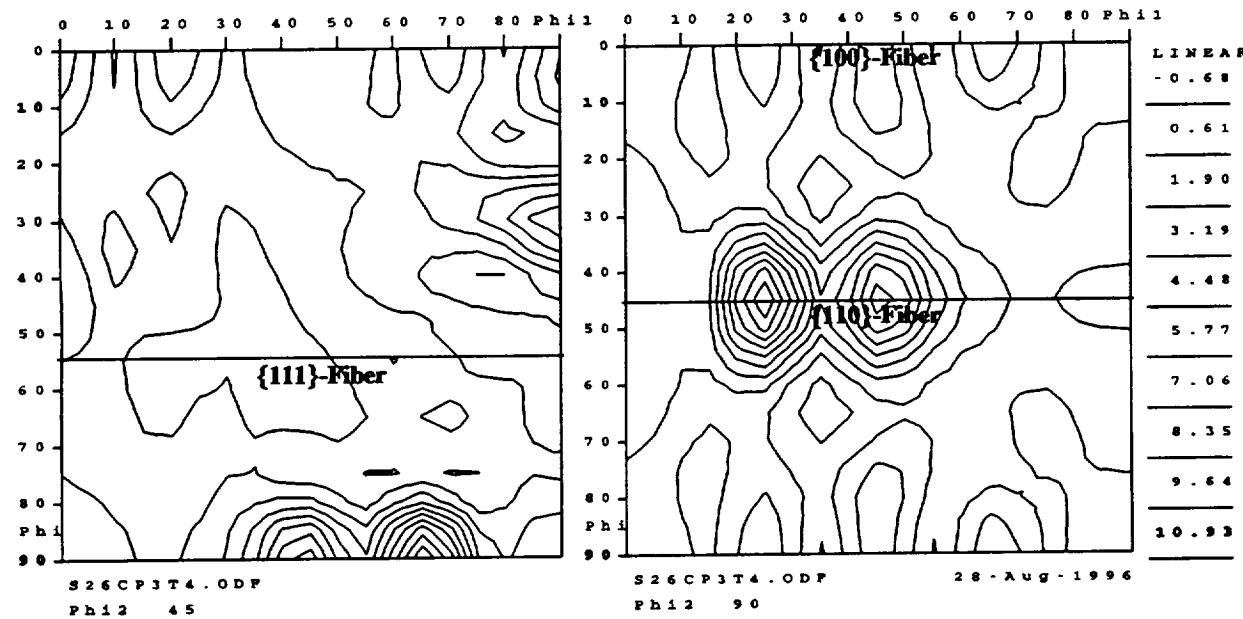


Figure 106. CODF sections for the 2096-T3 extrusion in the cap @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10, \dots, 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

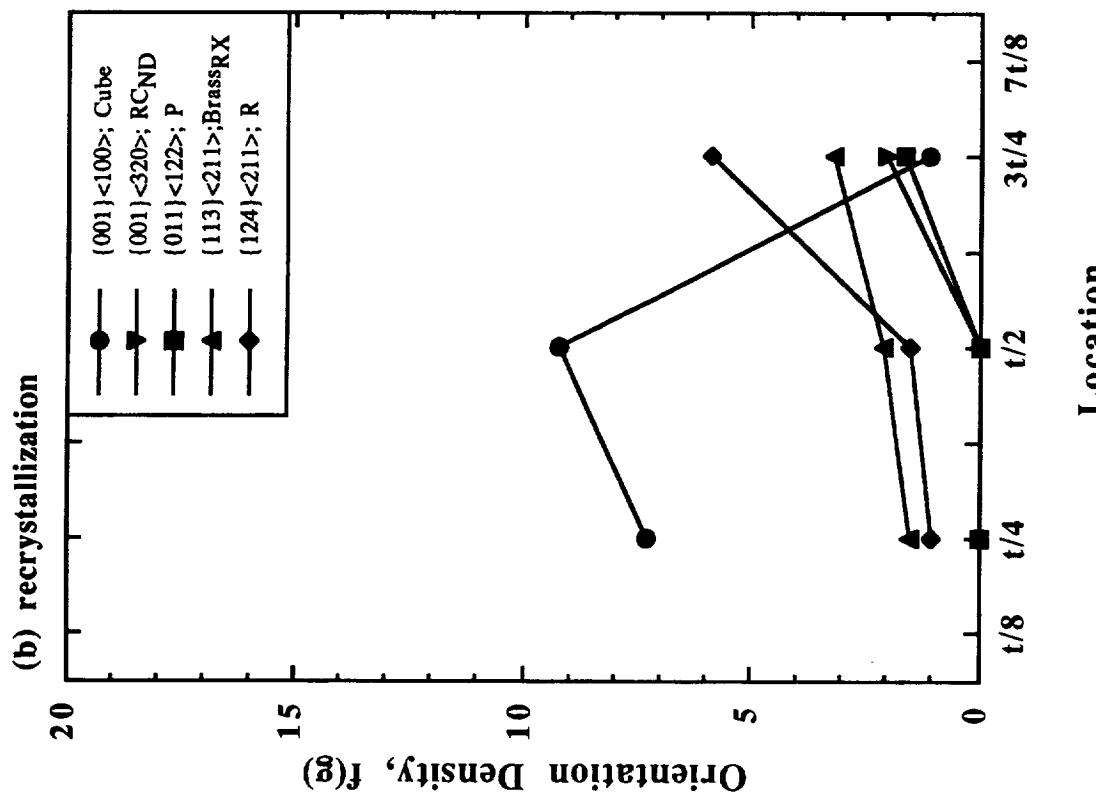
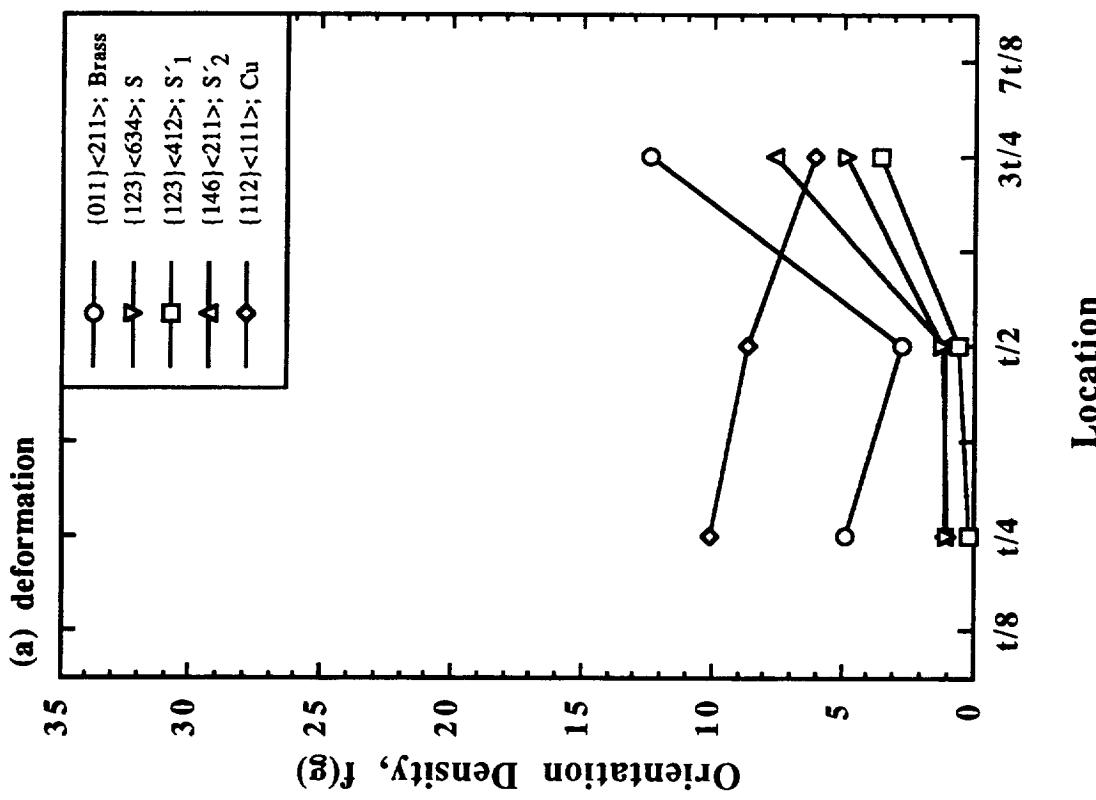


Figure 107. Orientation density, $f(g)$, as a function of location through the cross-section for the 2096-T3 extrusion in the cap region: (a) Deformation-related components; (b) Recrystallization-related components.

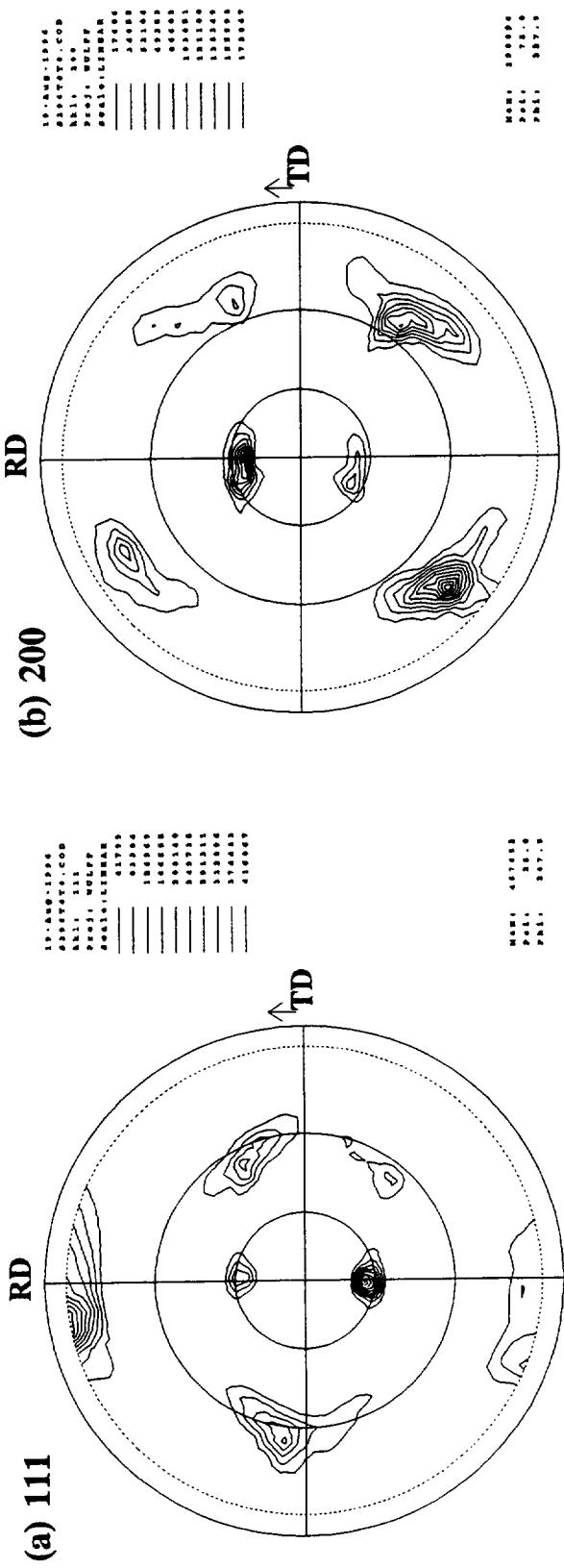
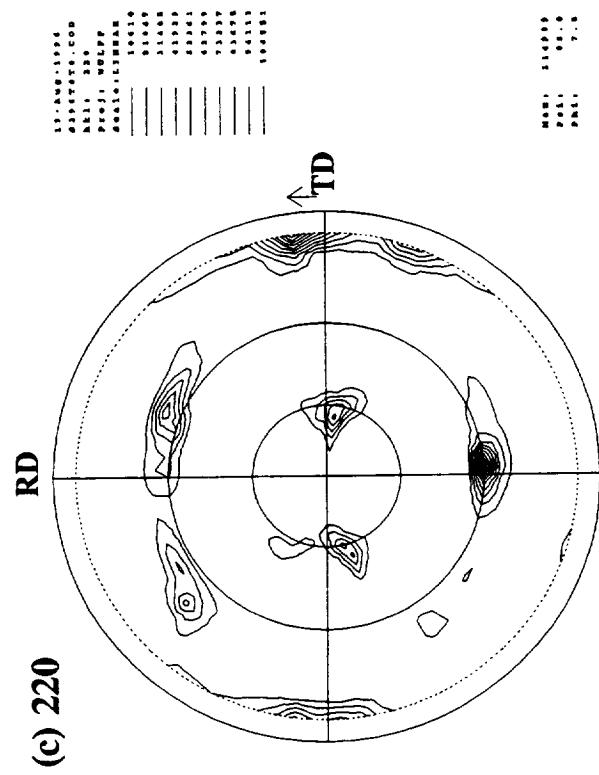
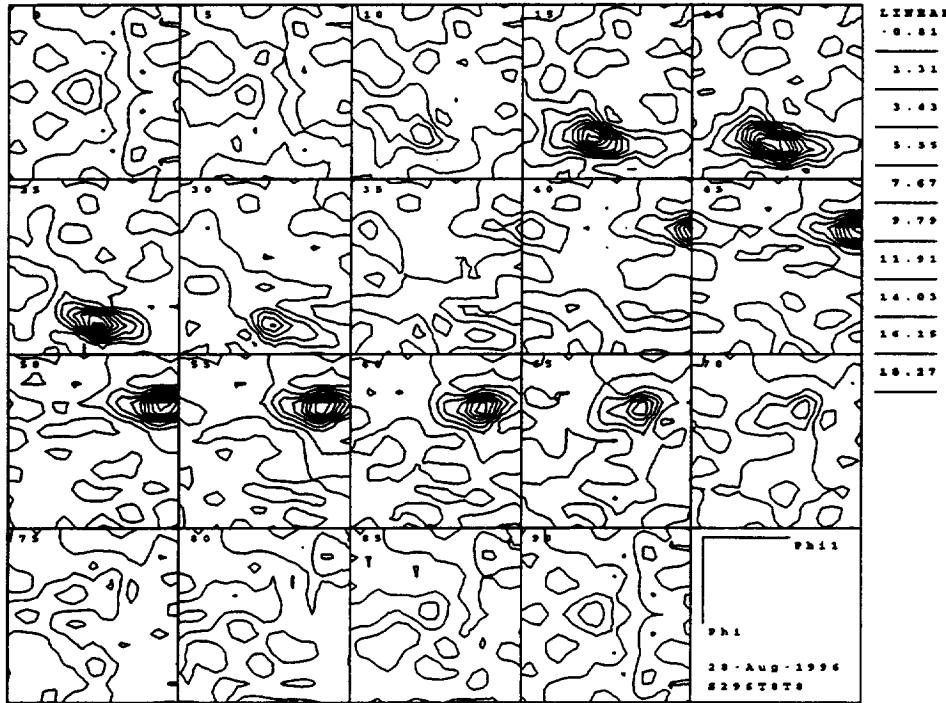


Figure 108.
Partial pole figures for 2096-T8 sheet @ t/8:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]



(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

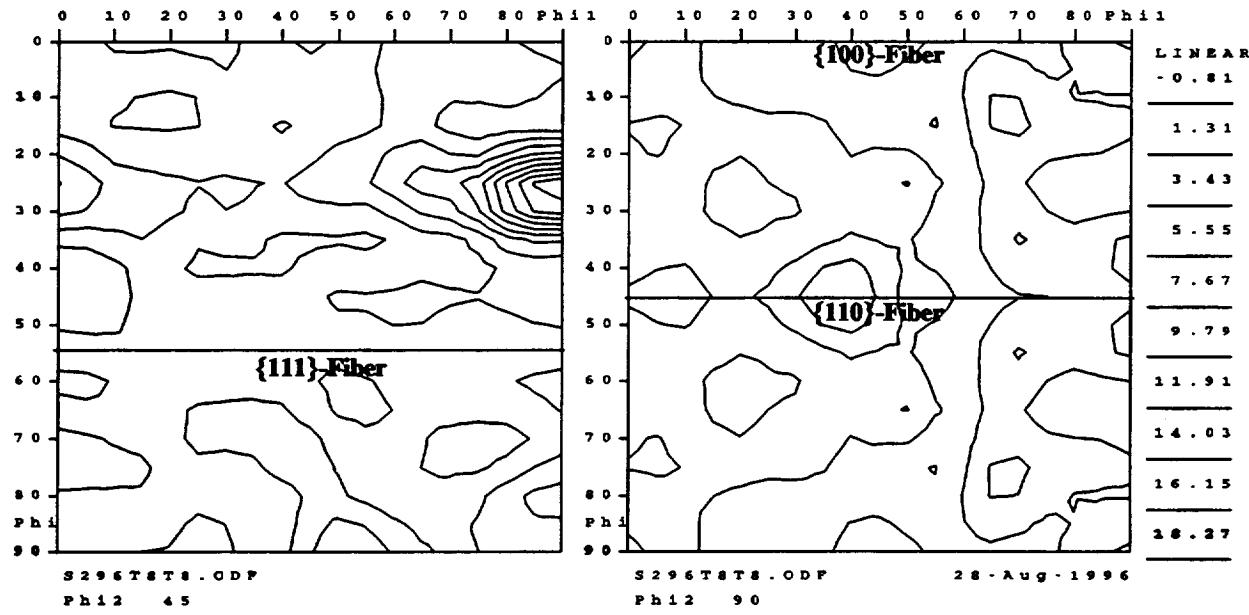


Figure 109. CODF sections for 2096-T8 sheet @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

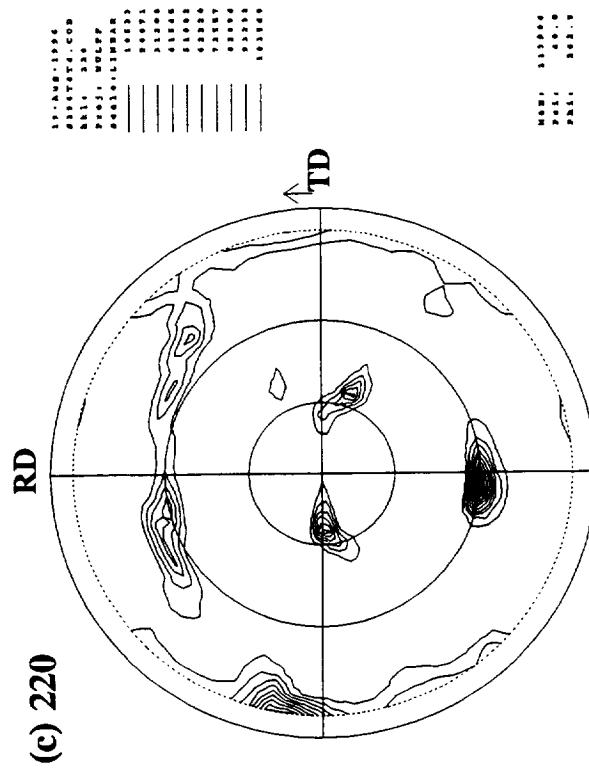
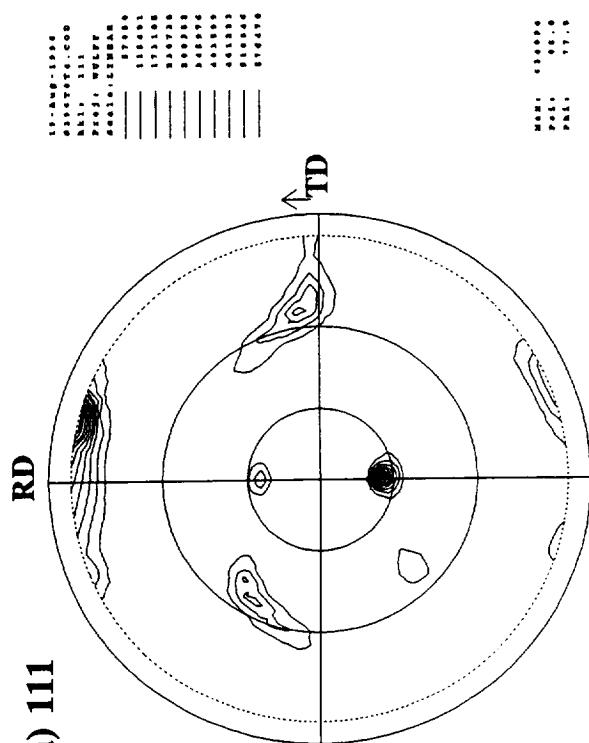
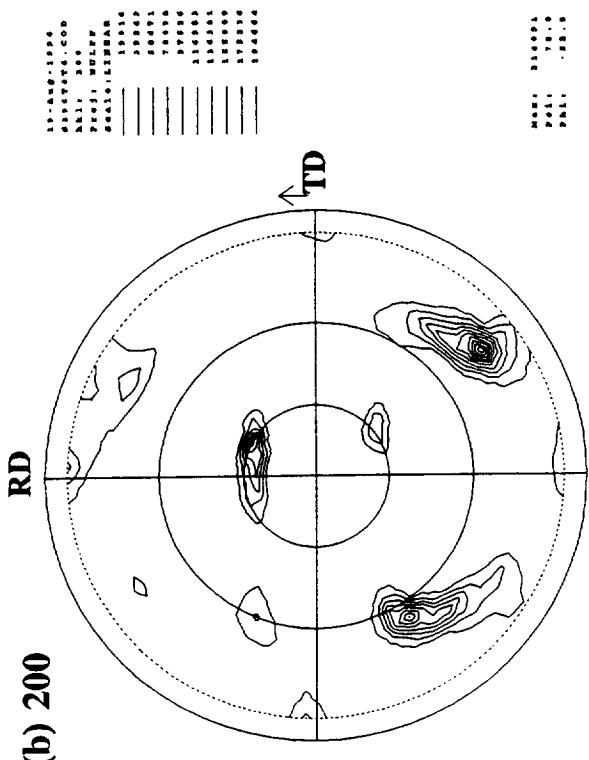
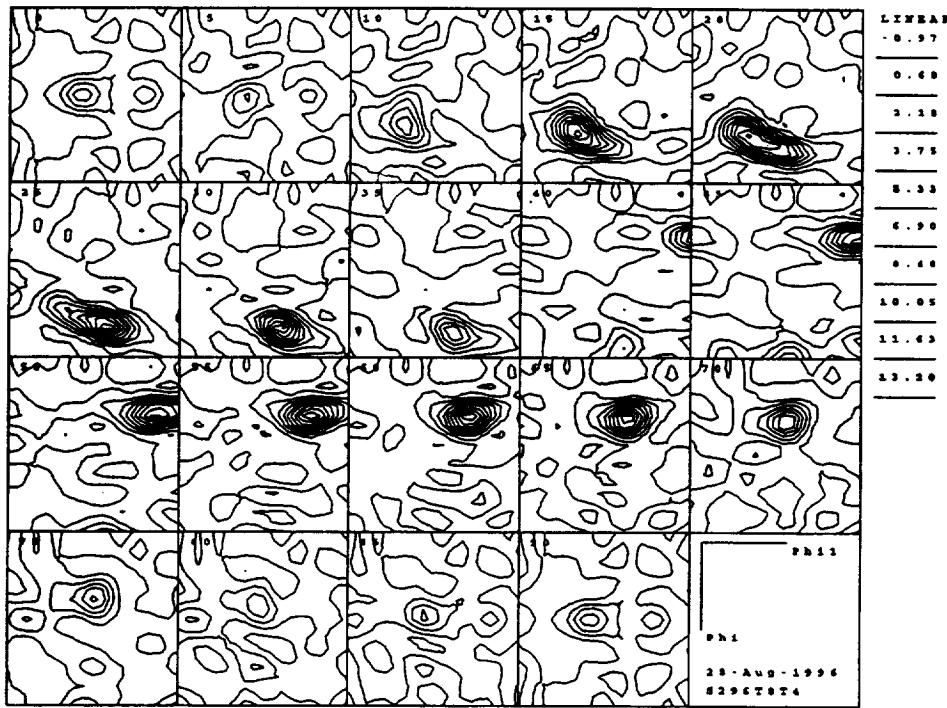


Figure 110.
Partial pole figures for 2096-T8 sheet @ t/4:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

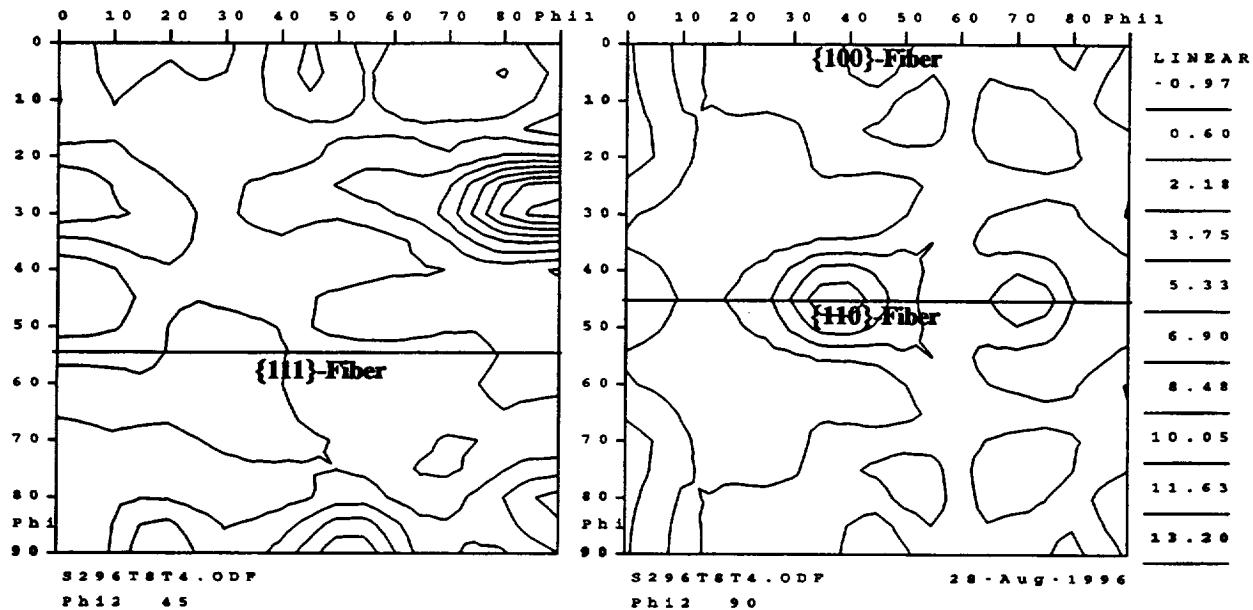


Figure 111. CODF sections for 2096-T8 sheet @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

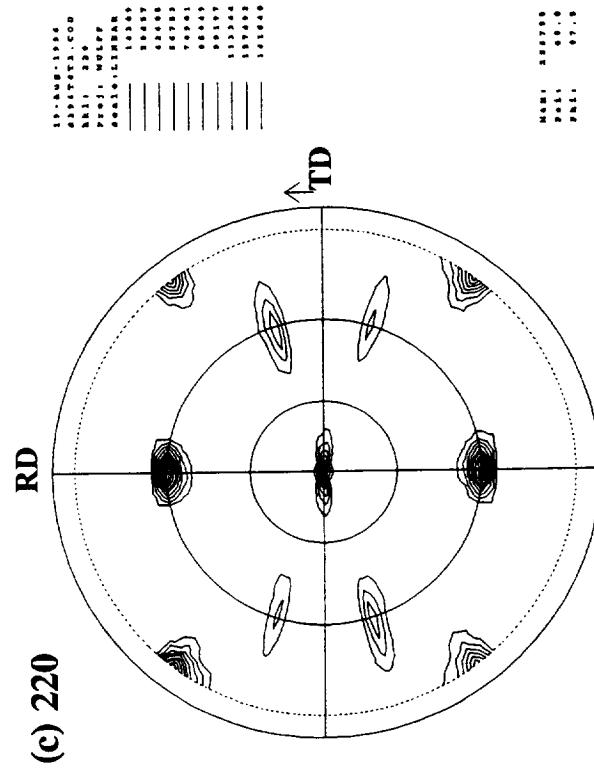
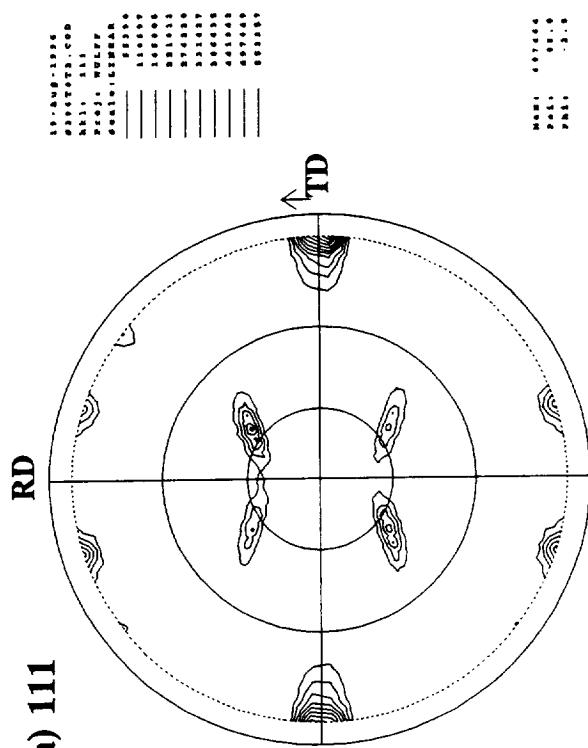
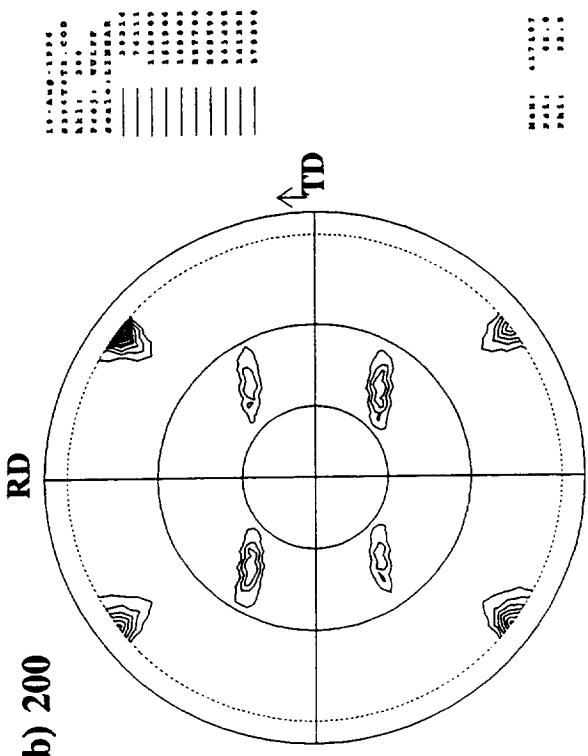
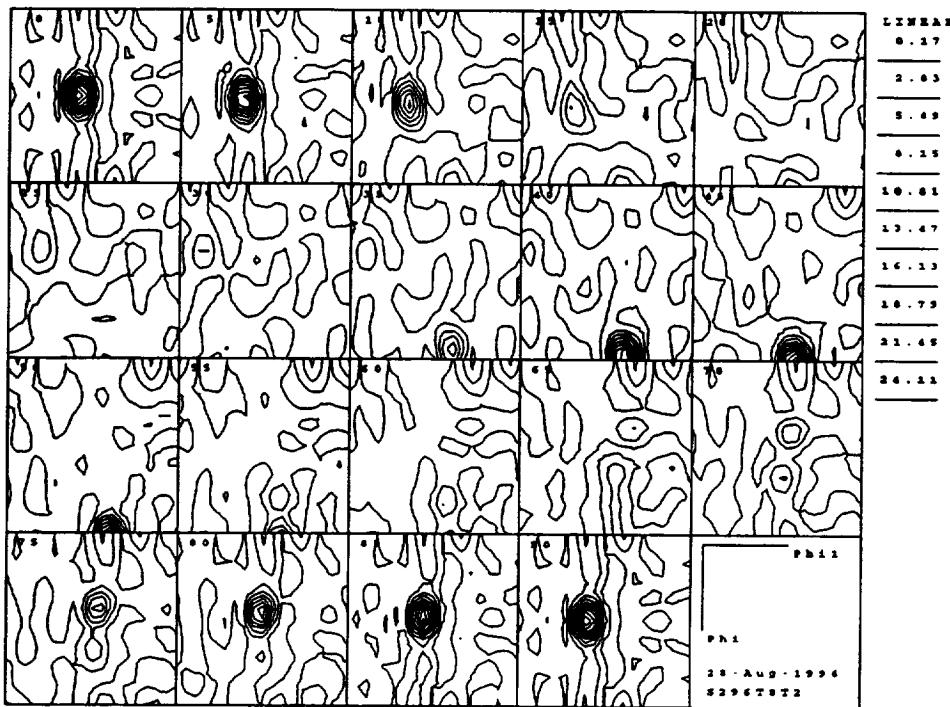


Figure 112.
Partial pole figures for 2096-T8 sheet @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

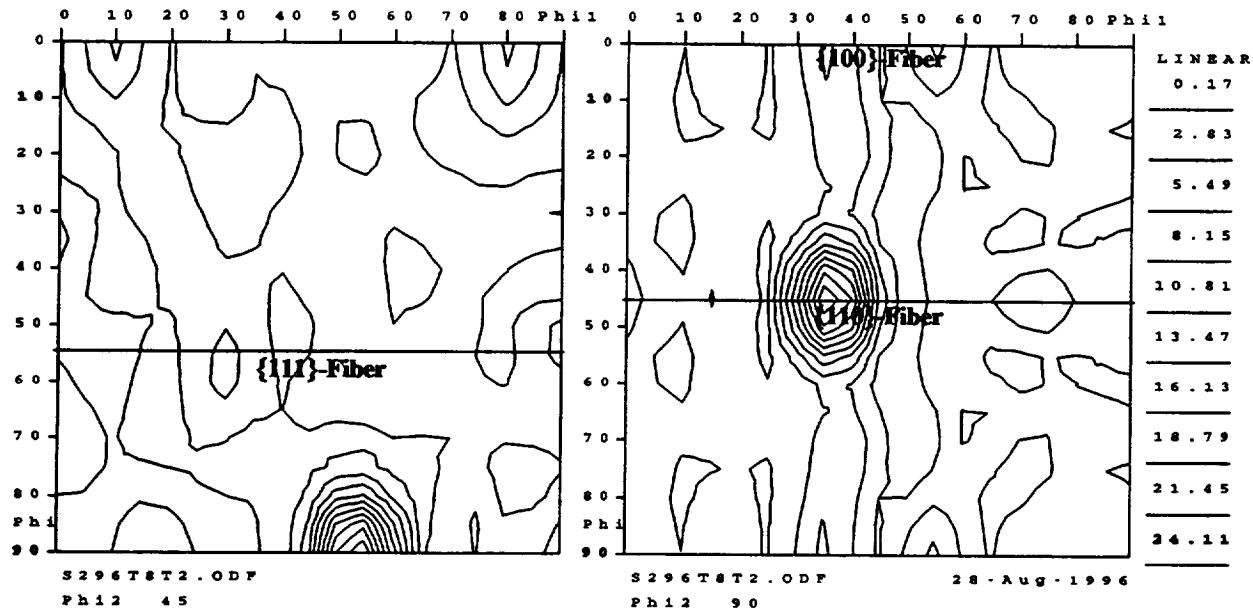


Figure 113. CODF sections for 2096-T8 sheet @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

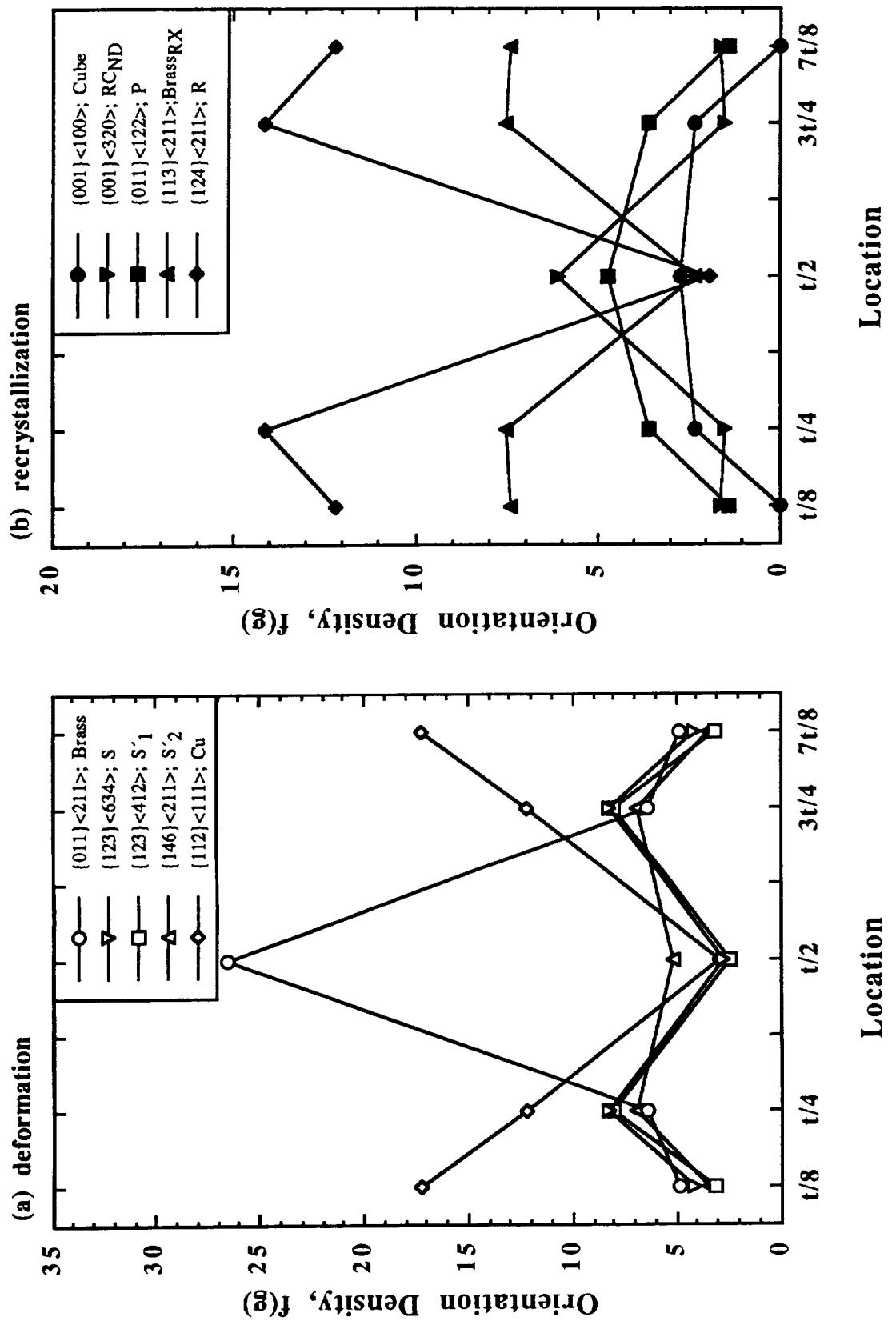


Figure 114. Orientation density, $f(g)$, as a function of location through the cross-section for the 2096-T8 sheet:
(a) Deformation-related components; (b) Recrystallization-related components.

4.4 Alloy 2195

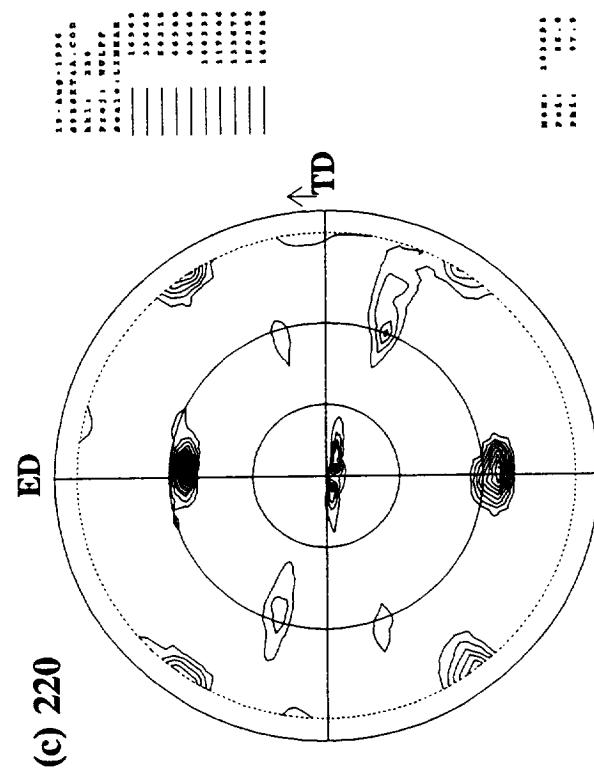
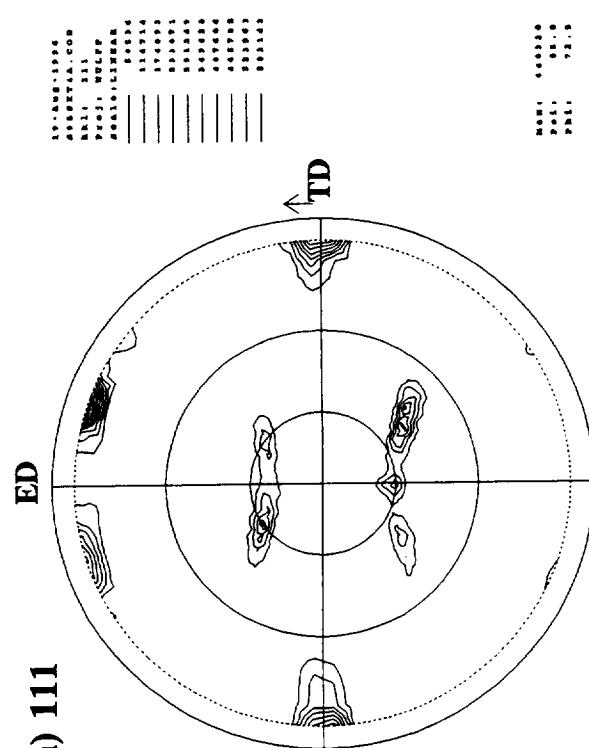
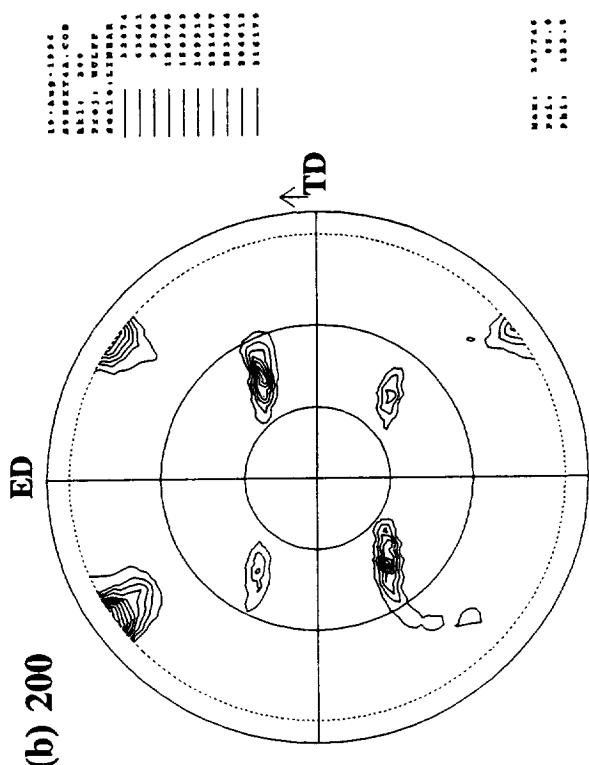
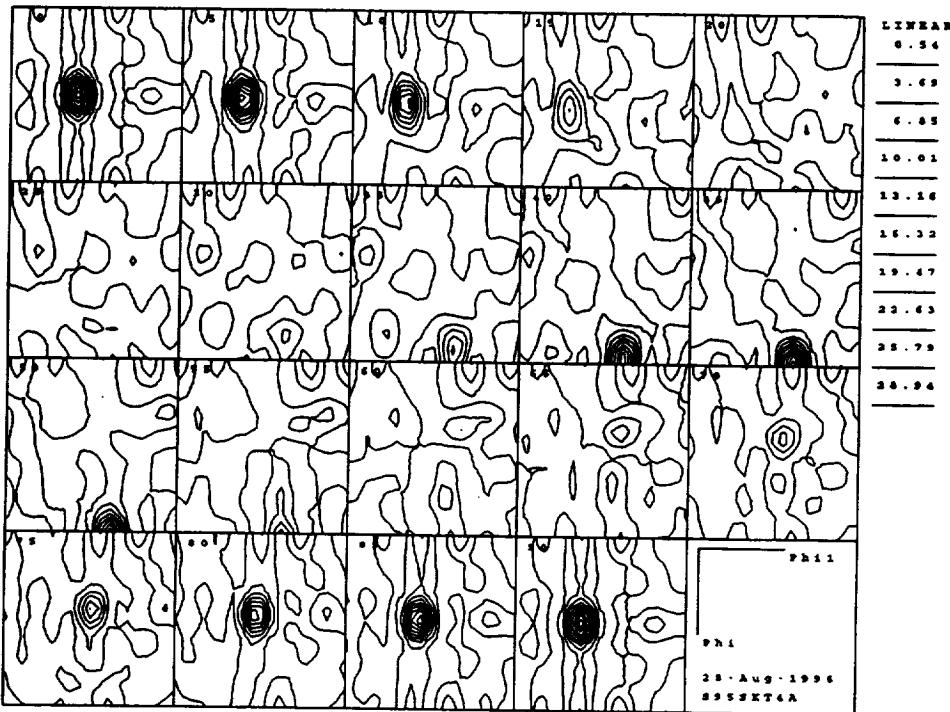


Figure 115.
Partial pole figures for the 2195-T3 extrusion in
the skin @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R) radial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

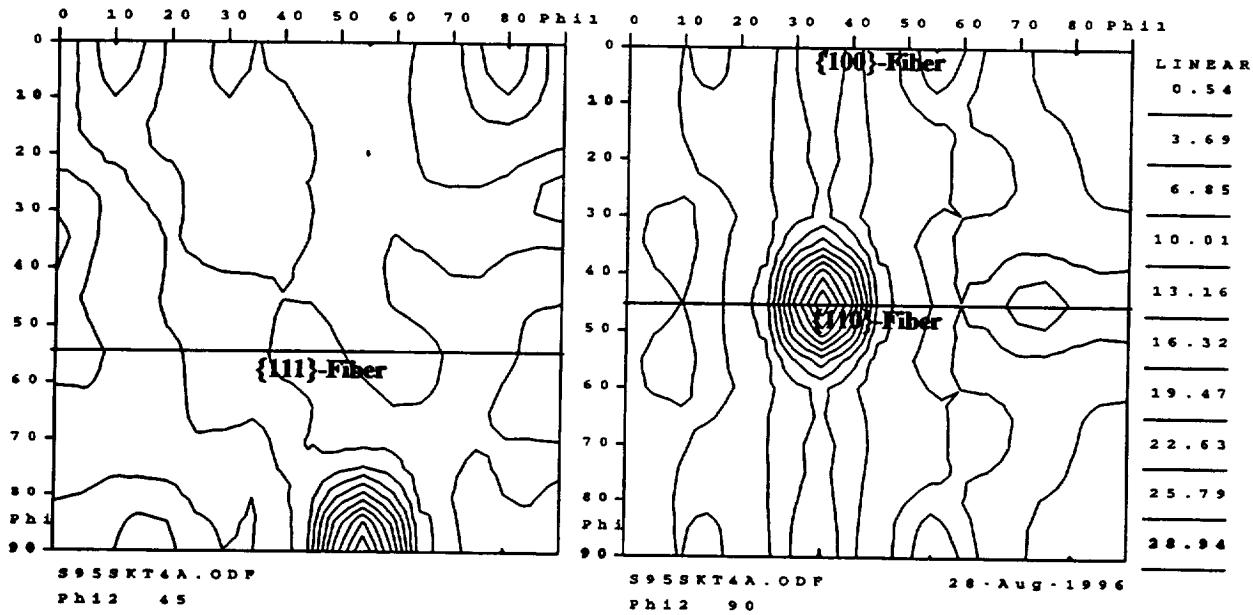


Figure 116. CODF sections for the 2195-T3 extrusion in the skin @ $t/4$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

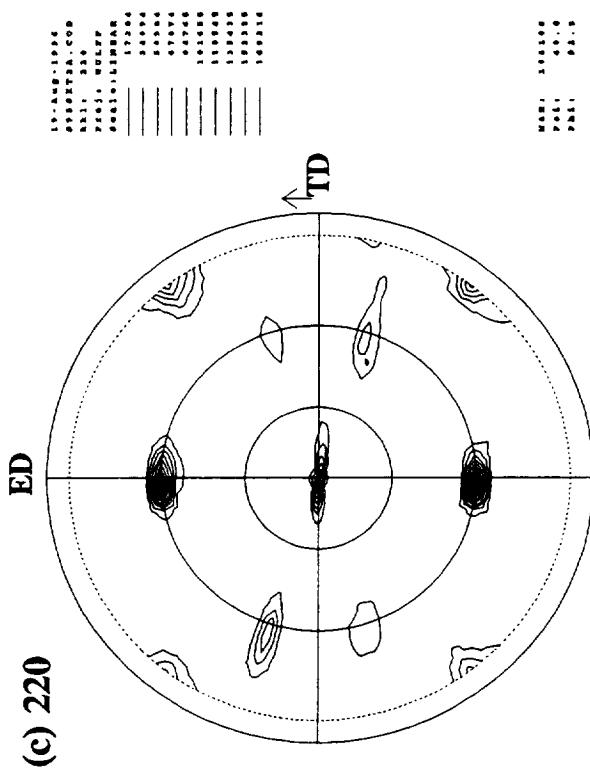
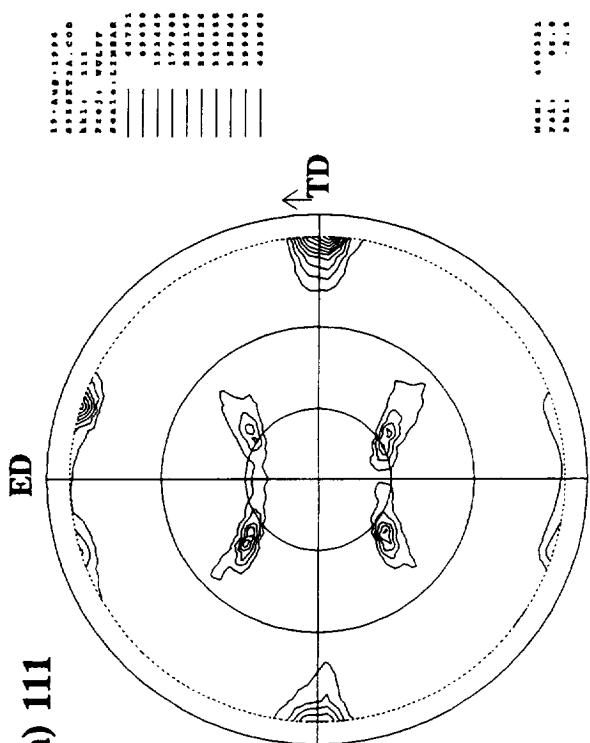
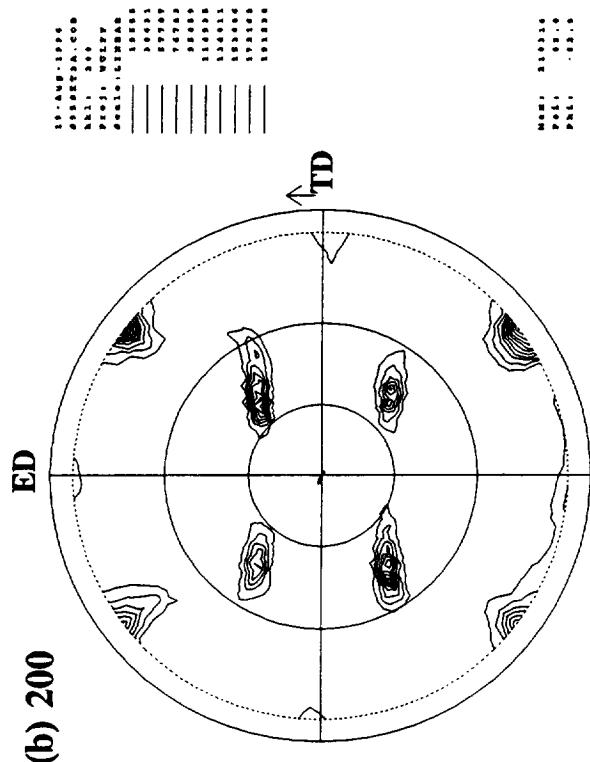
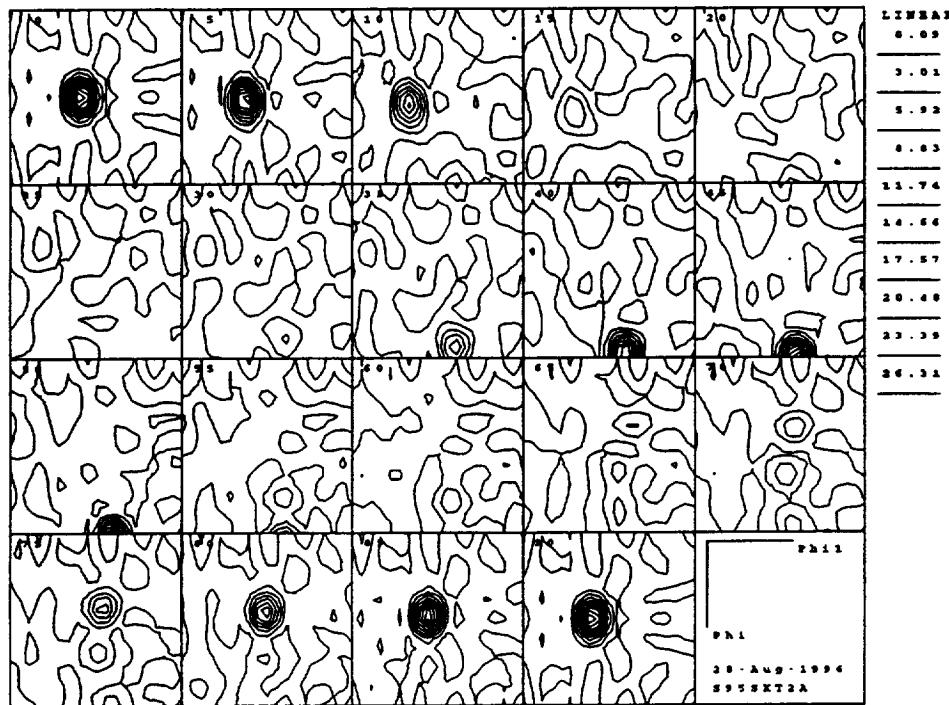


Figure 117.
Partial pole figures for the 2195-T3 extrusion in
the skin @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R) radial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

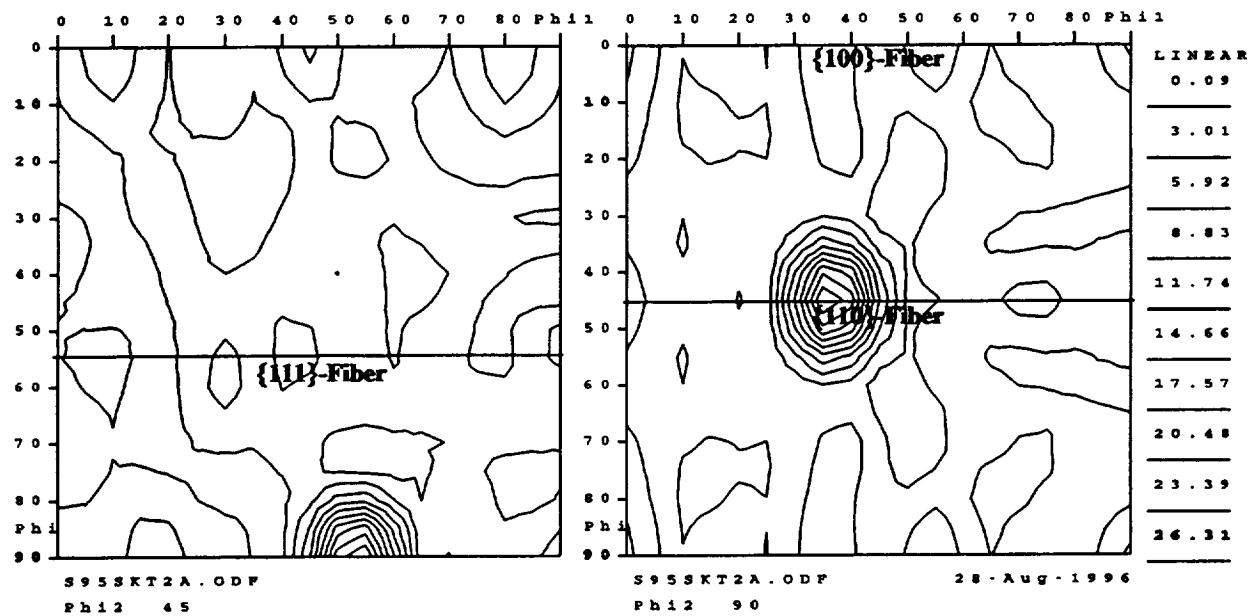


Figure 118. CODF sections for the 2195-T3 extrusion in the skin @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

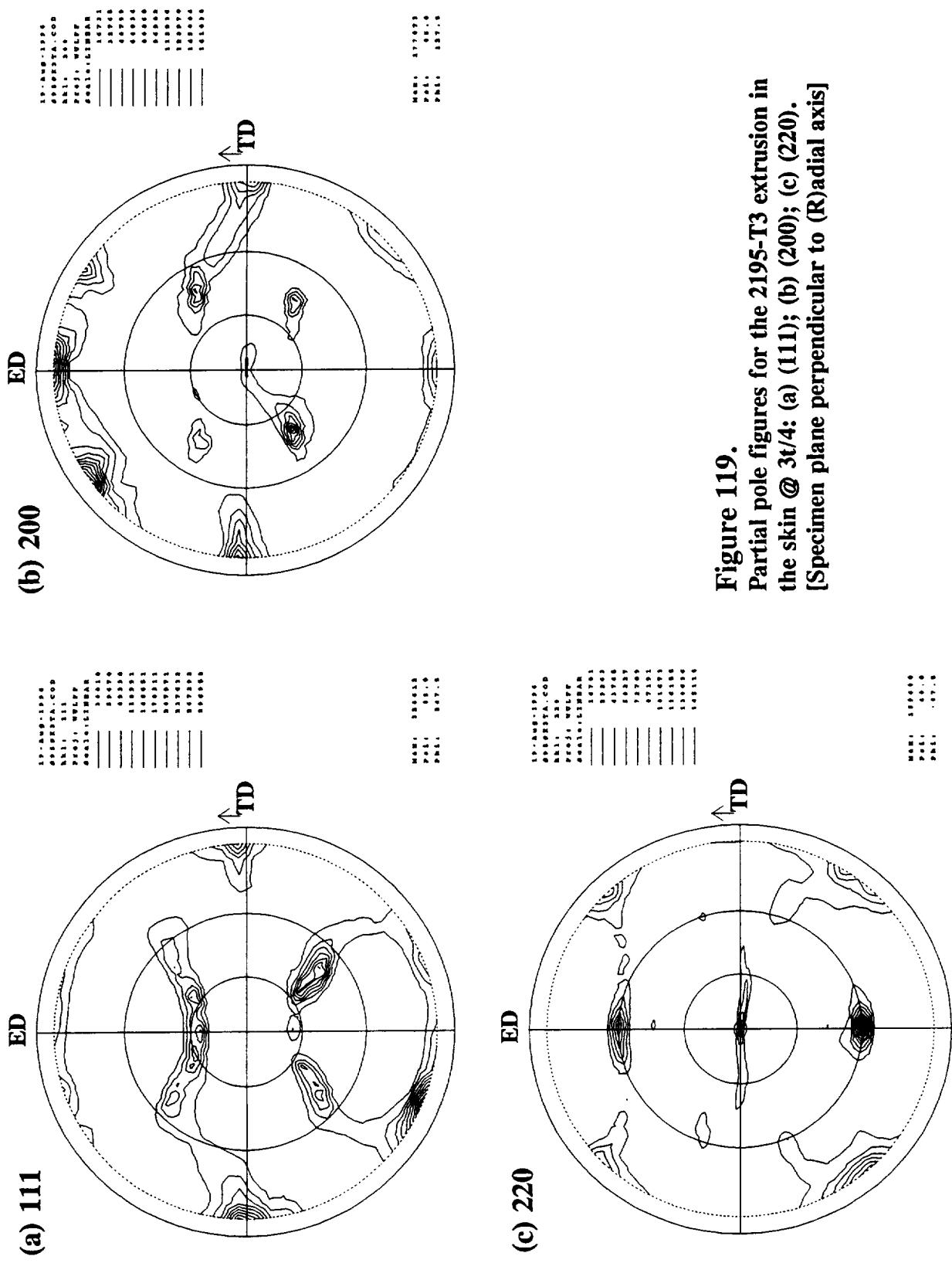
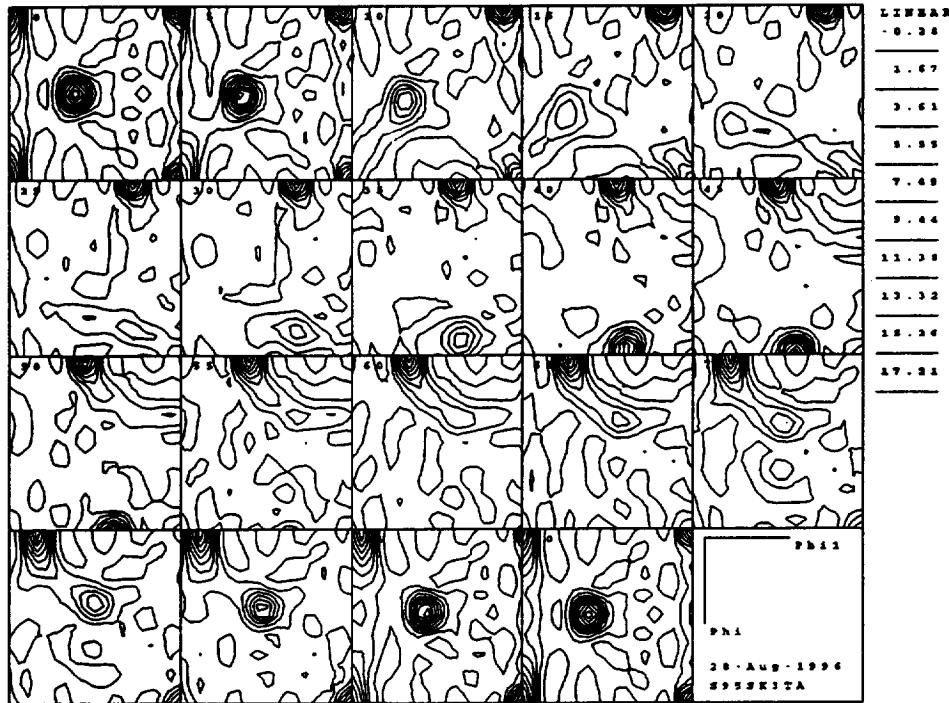


Figure 119.
Partial pole figures for the 2195-T3 extrusion in
the skin @ $3t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

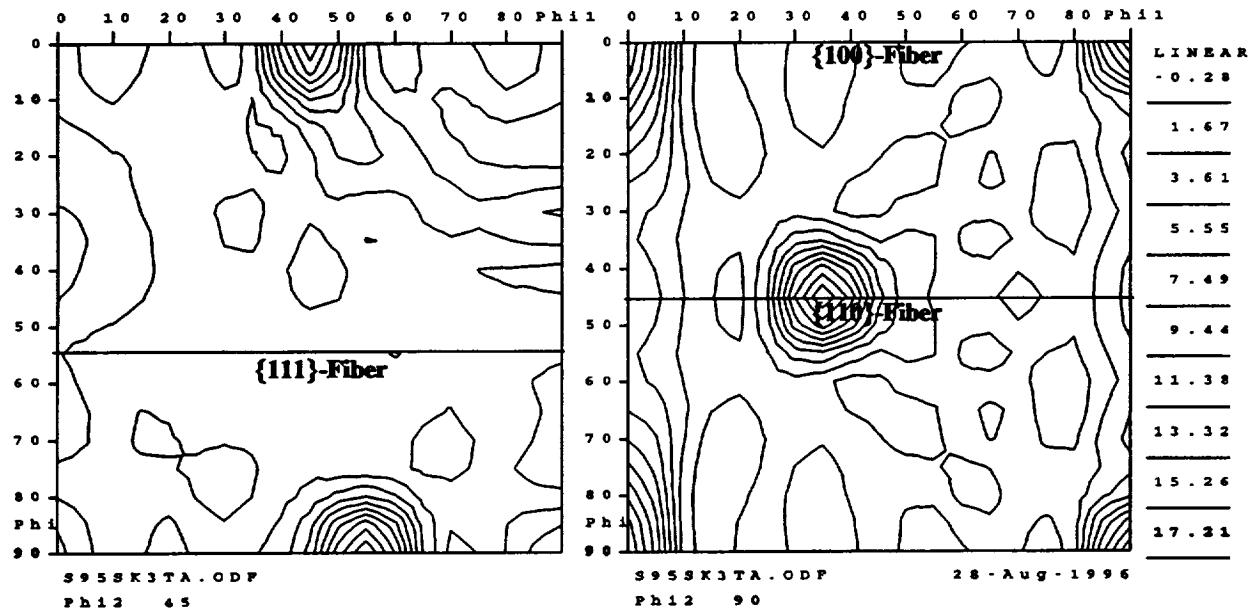


Figure 120. CODF sections for the 2195-T3 extrusion in the skin @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

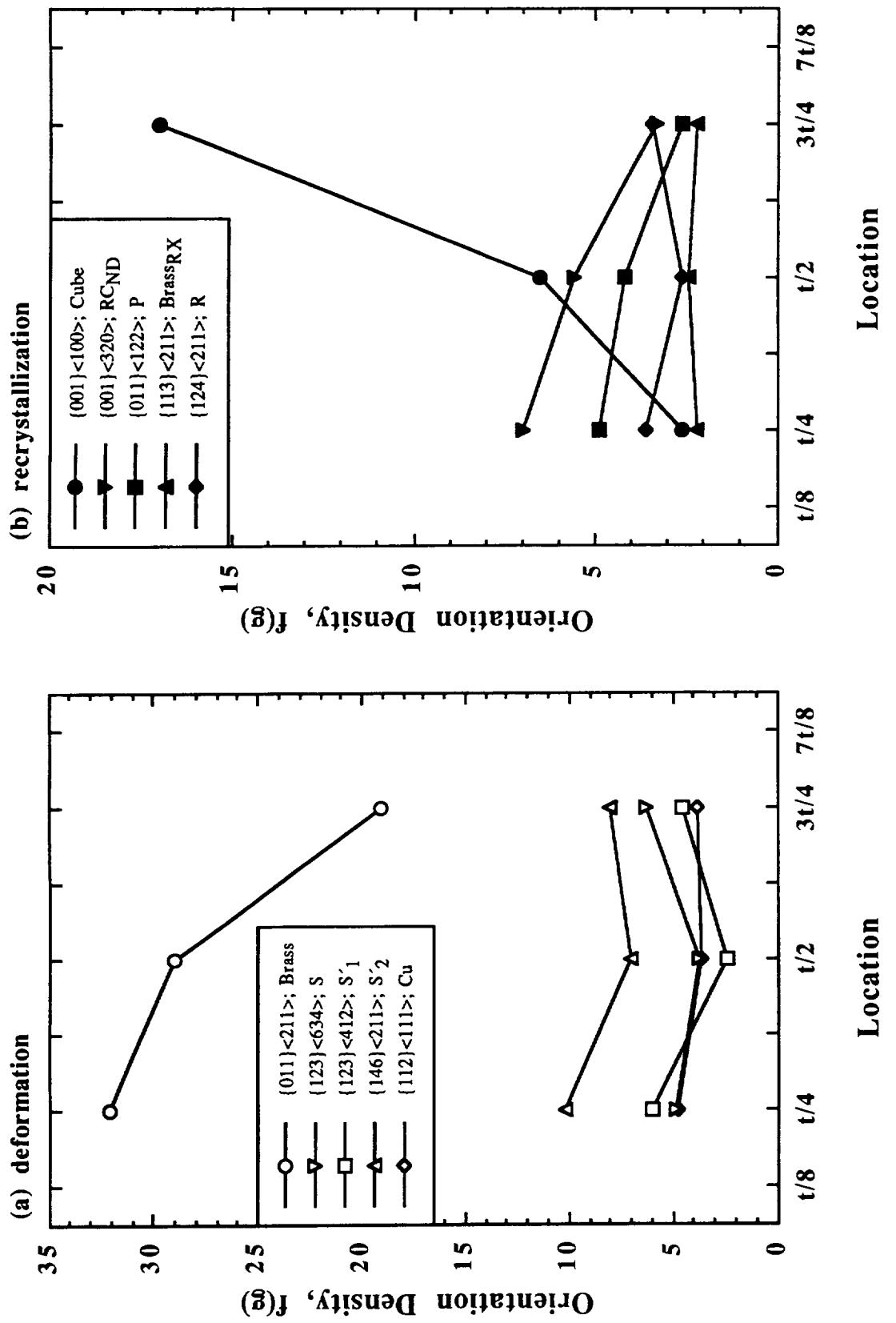


Figure 121. Orientation density, $f(g)$, as a function of location through the cross-section for the 2195-T3 extrusion in the skin region: (a) Deformation-related components; (b) Recrystallization-related components.

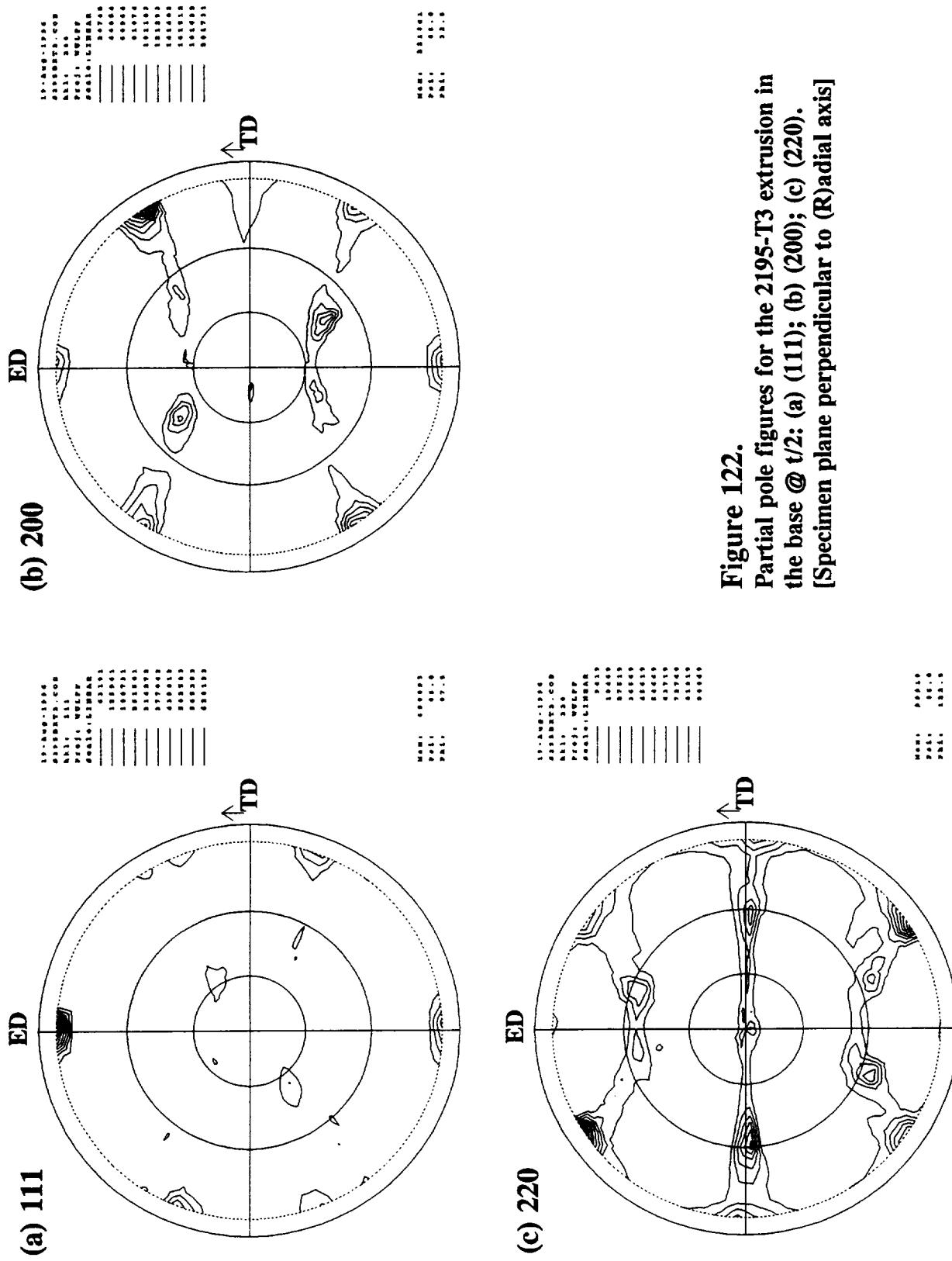
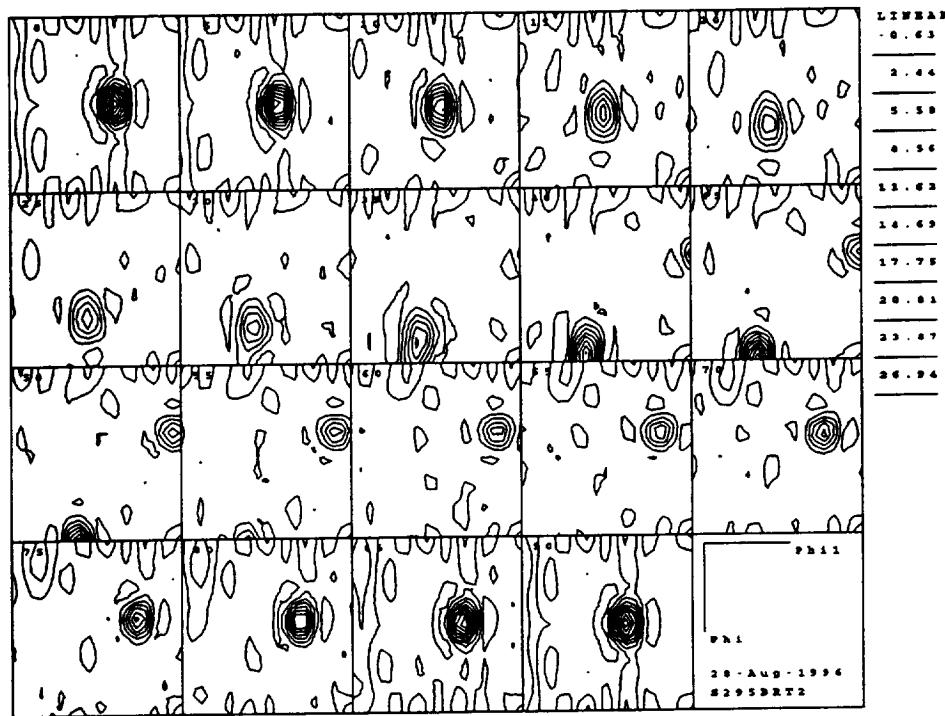


Figure 122.
Partial pole figures for the 2195-T3 extrusion in
the base @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

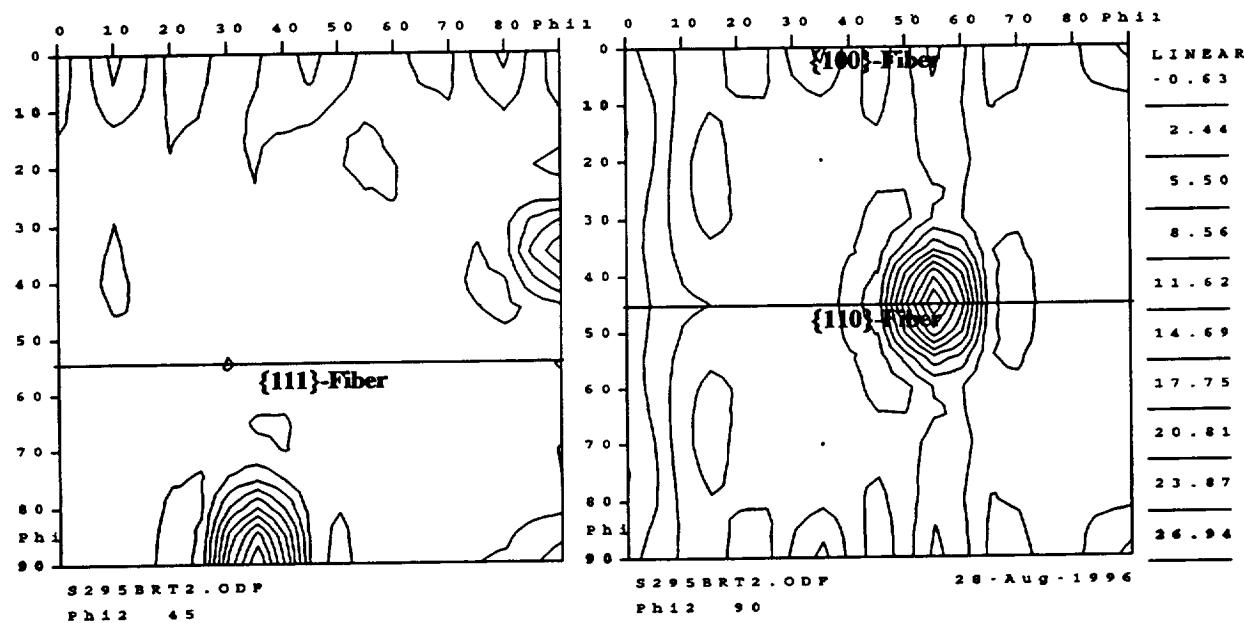


Figure 123. CODF sections for the 2195-T3 extrusion in the base @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

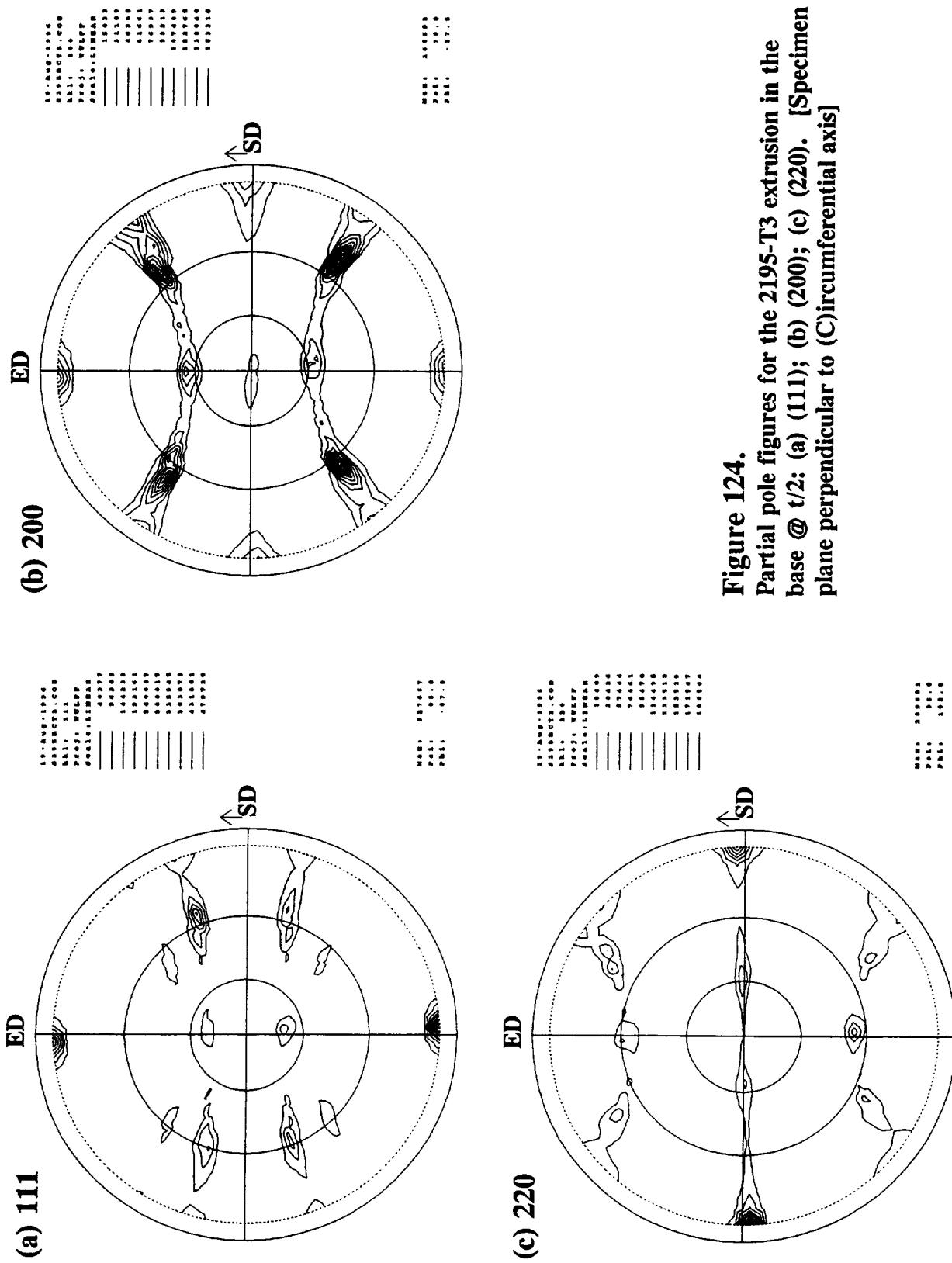
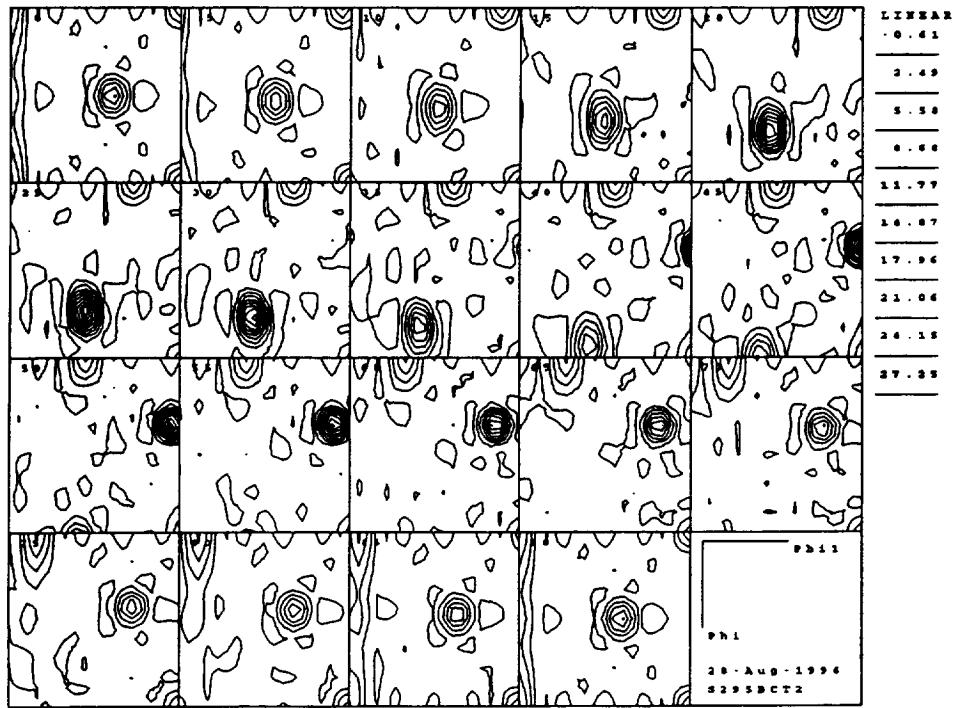


Figure 124.
Partial pole figures for the 2195-T3 extrusion in the
base @ $t/2$: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

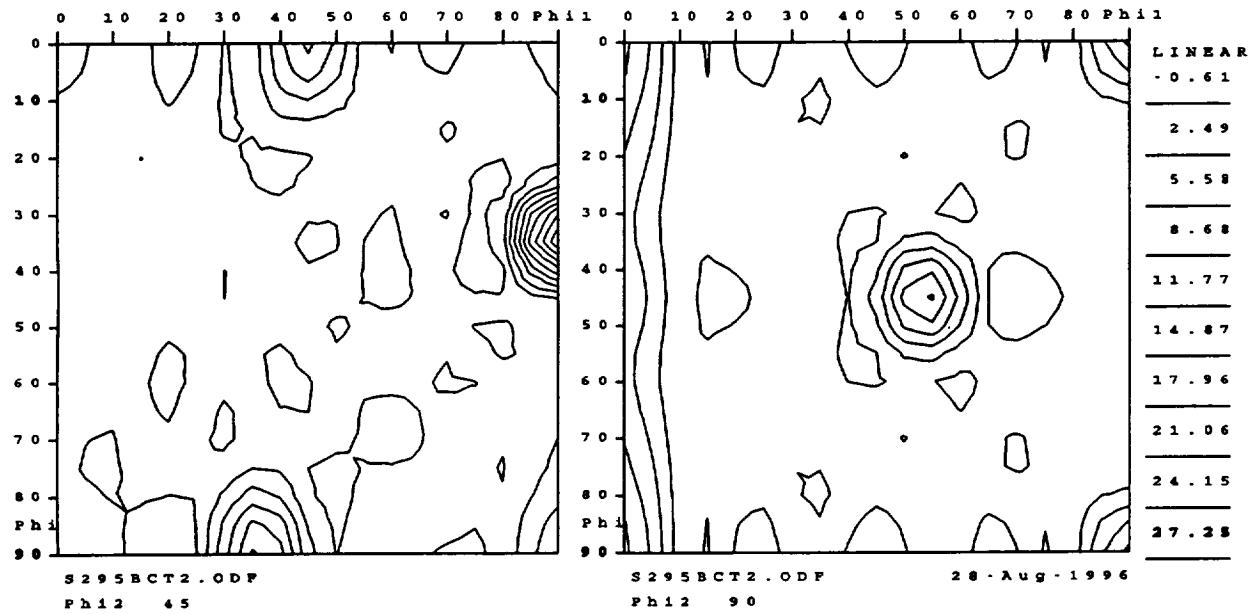


Figure 125. CODF sections for the 2195-T3 extrusion in the base @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

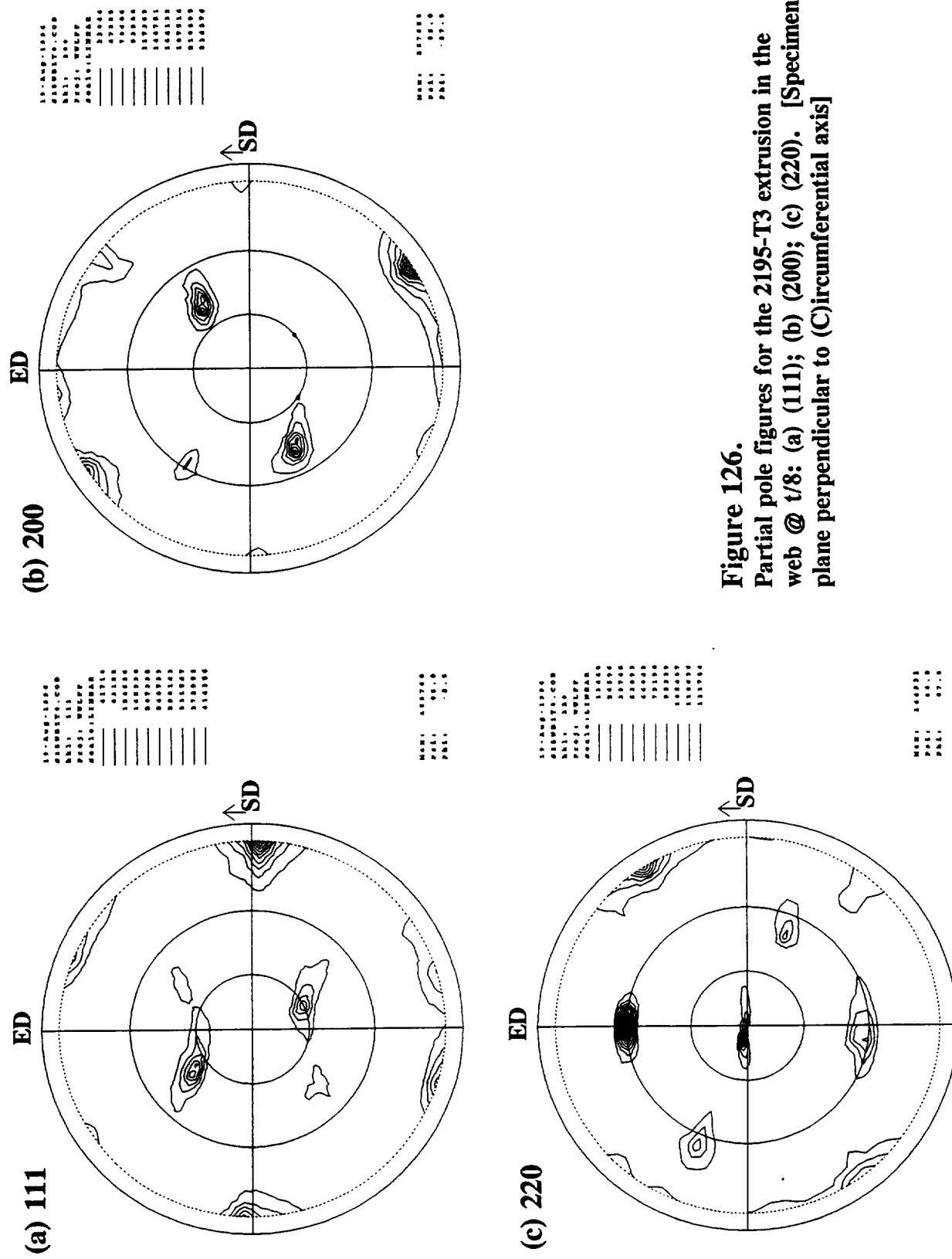
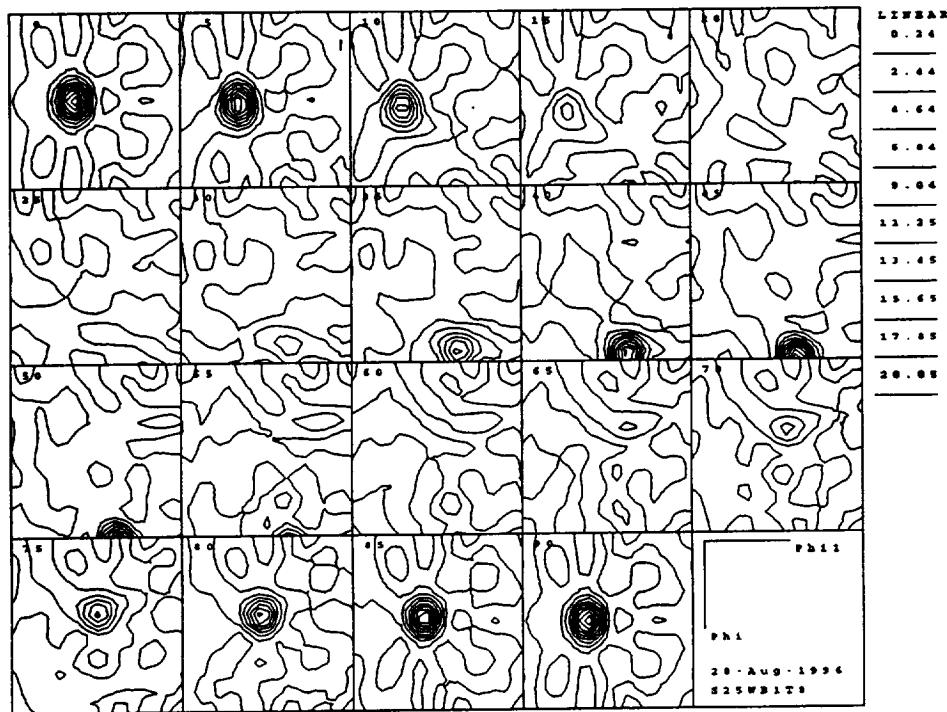


Figure 126.
Partial pole figures for the 2195-T3 extrusion in the
web @ $t/8$: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C) circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

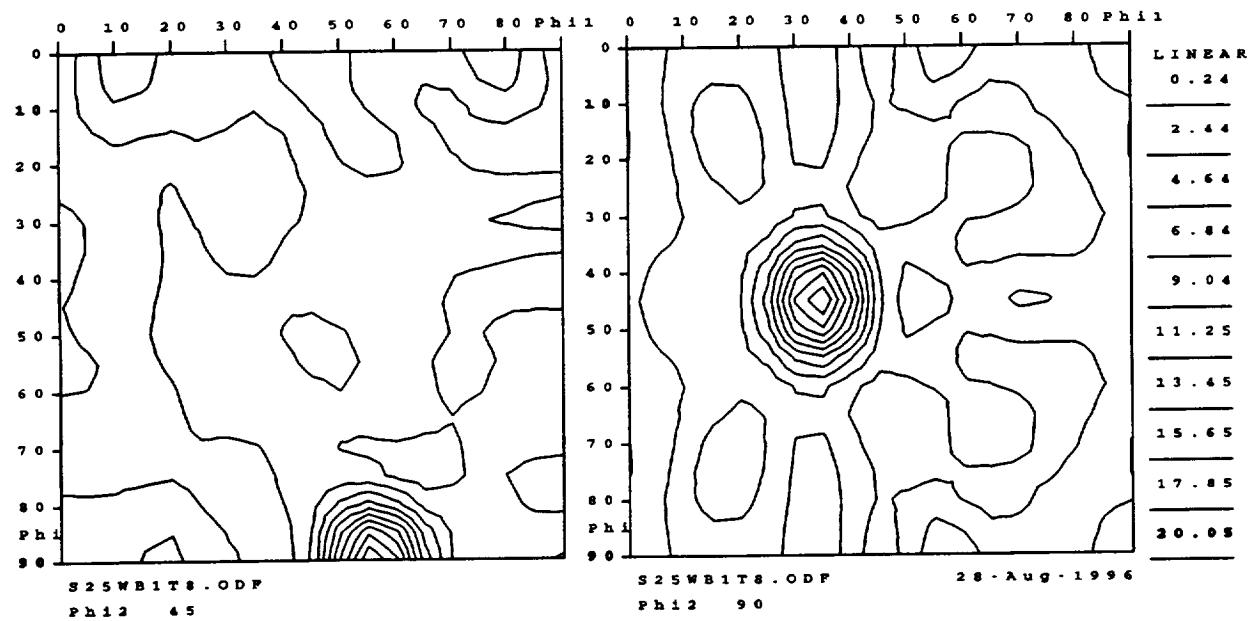


Figure 127. CODF sections for the 2195-T3 extrusion in the web @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

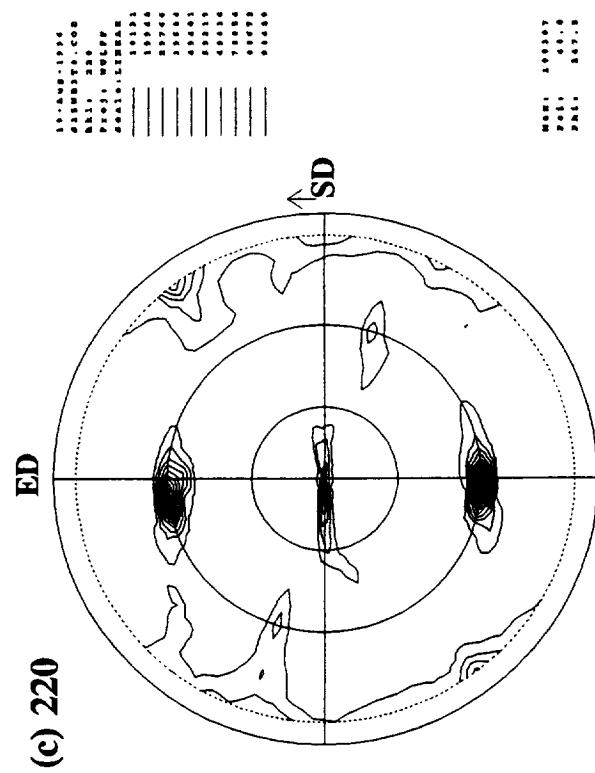
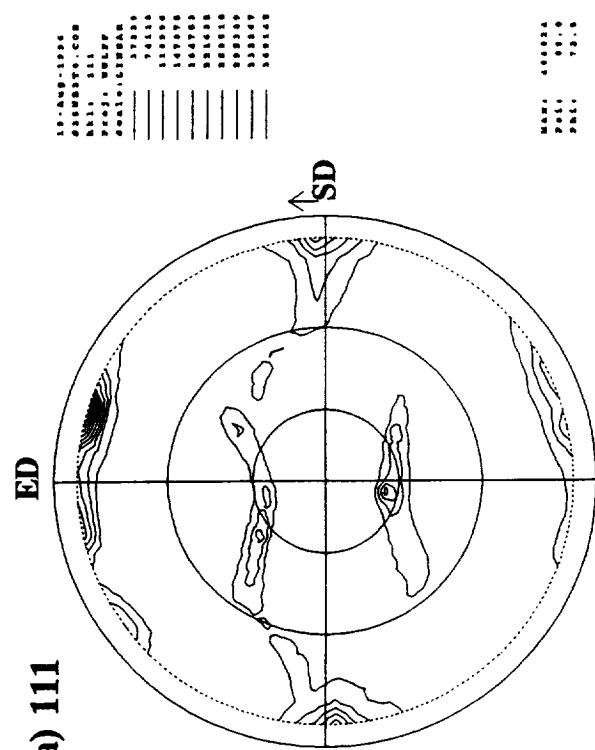
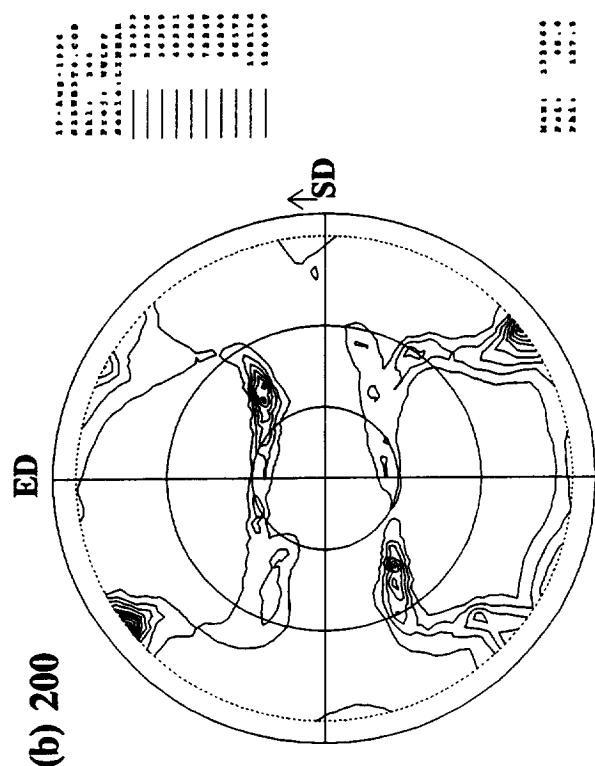
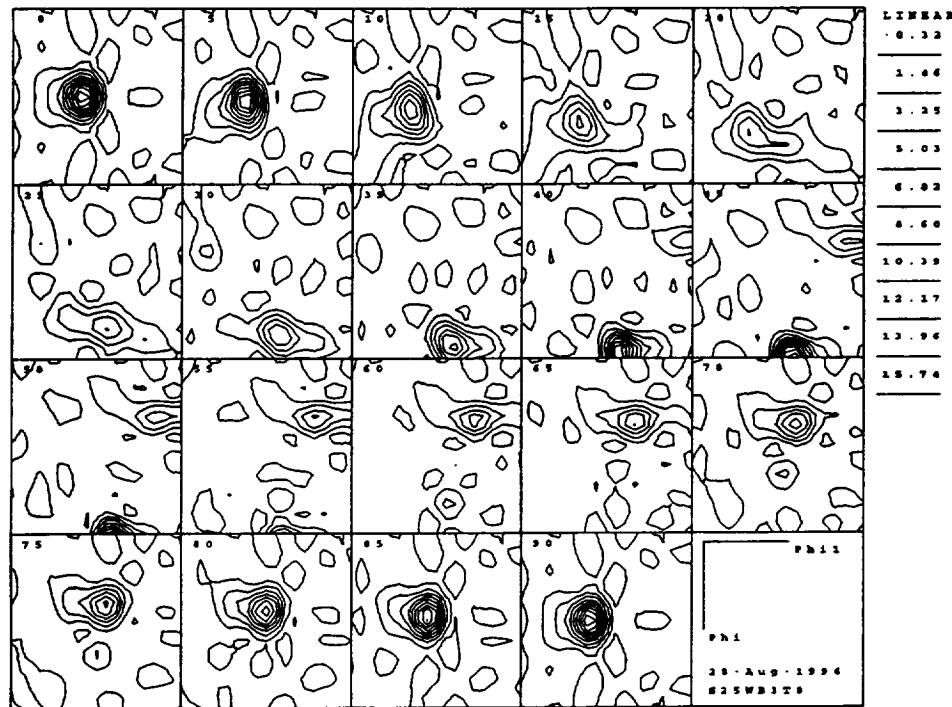


Figure 128.
Partial pole figures for the 2195-T3 extrusion in the
web @ 3t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

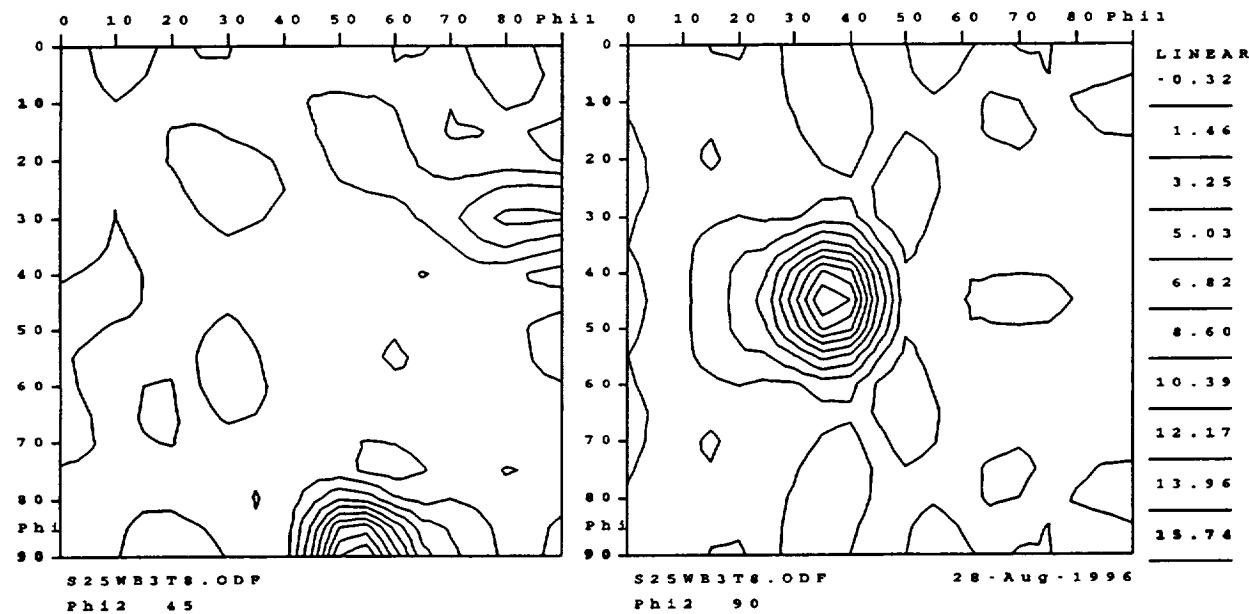


Figure 129. CODF sections for the 2195-T3 extrusion in the web @ 3t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

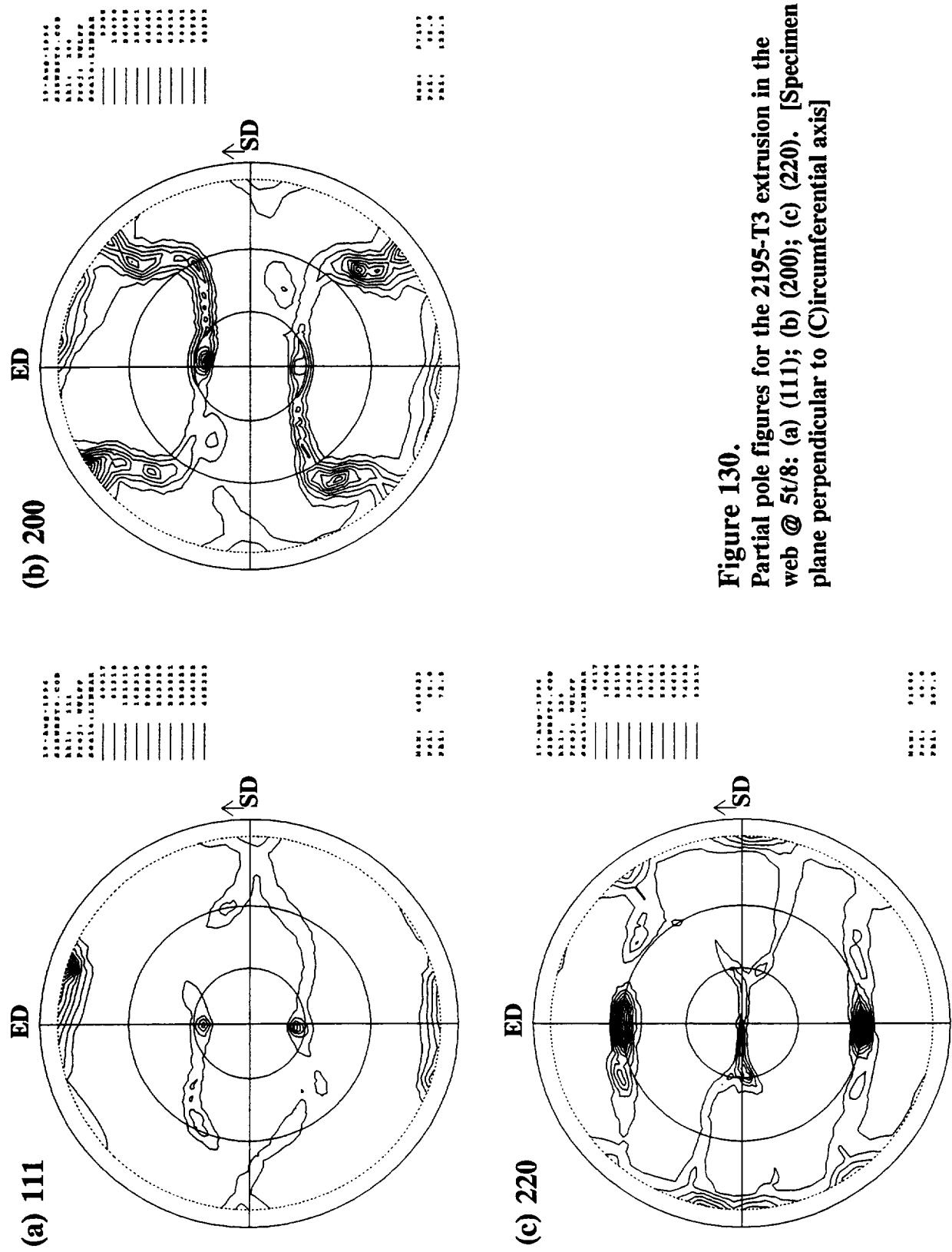
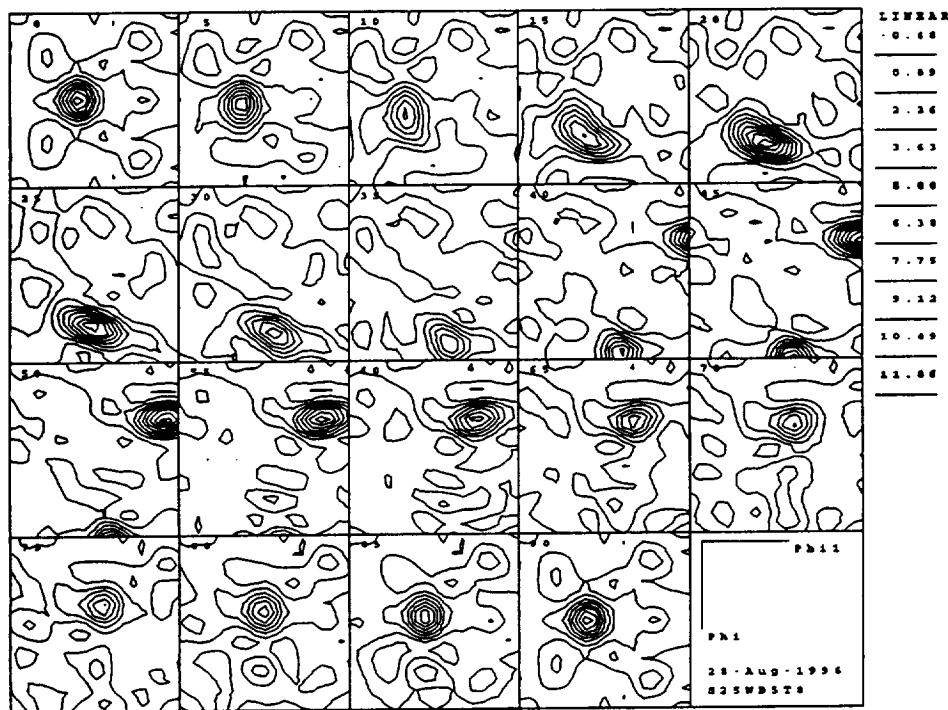


Figure 130.
Partial pole figures for the 2195-T3 extrusion in the
web @ 5t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)ircumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

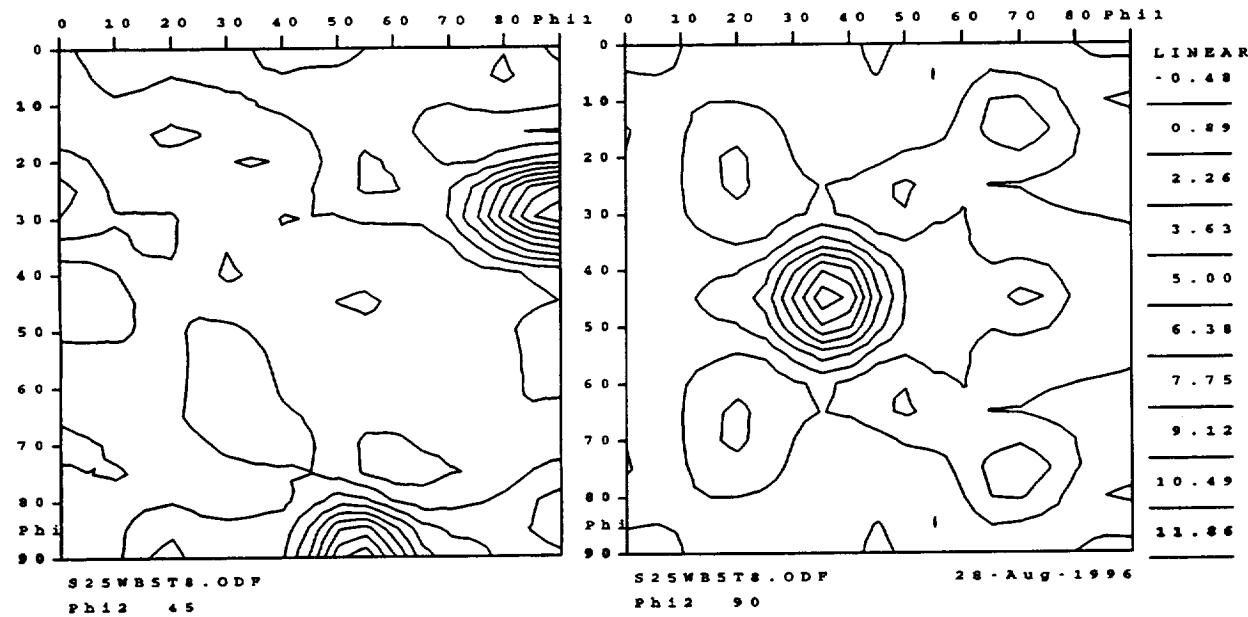


Figure 131. CODF sections for the 2195-T3 extrusion in the web @ 5t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

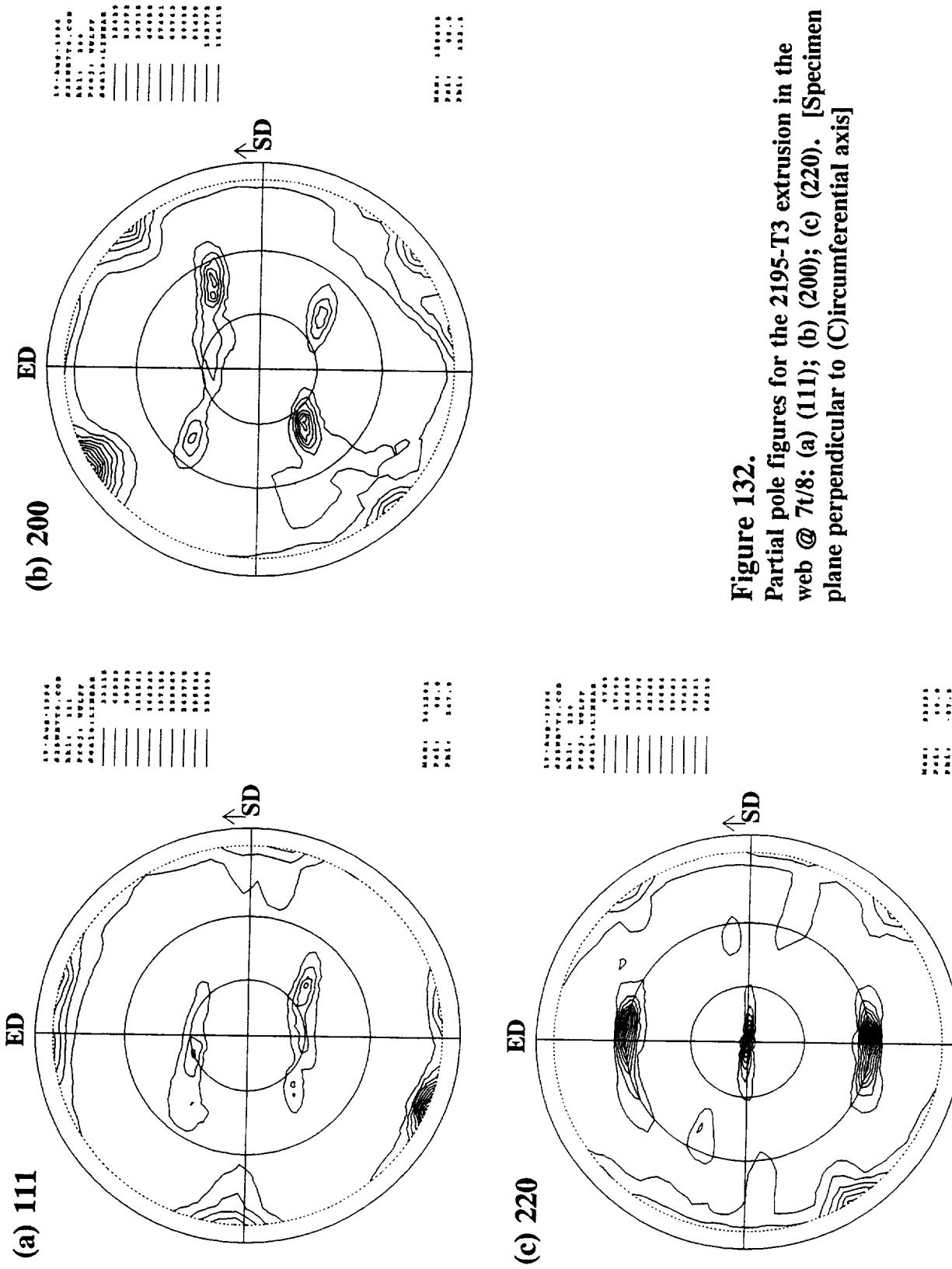
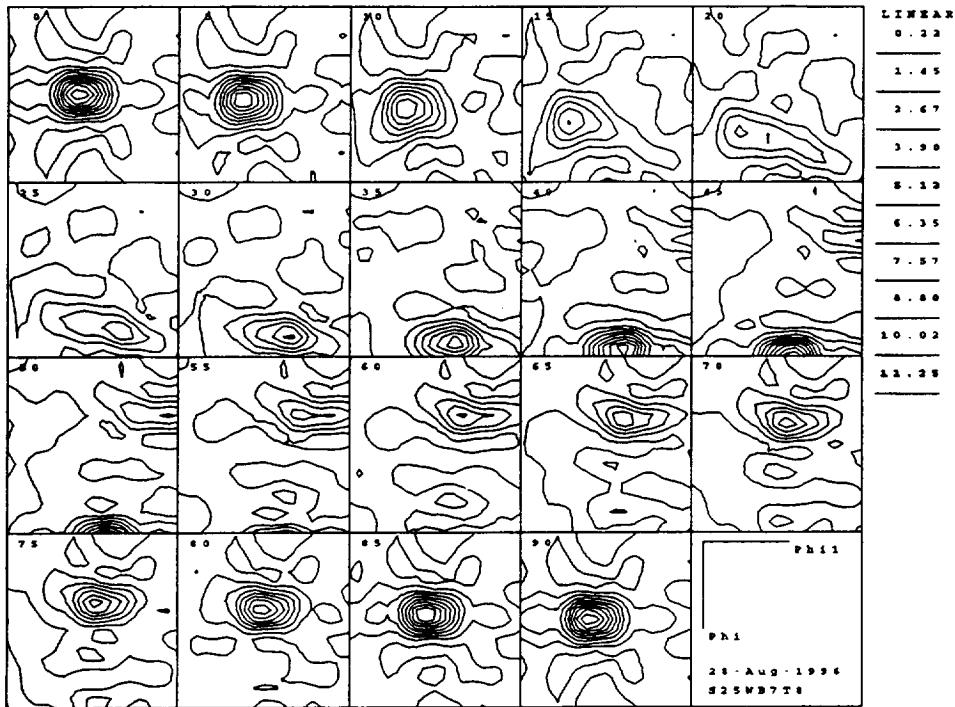


Figure 132.
Partial pole figures for the 2195-T3 extrusion in the
web @ 7t/8: (a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (C)circumferential axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

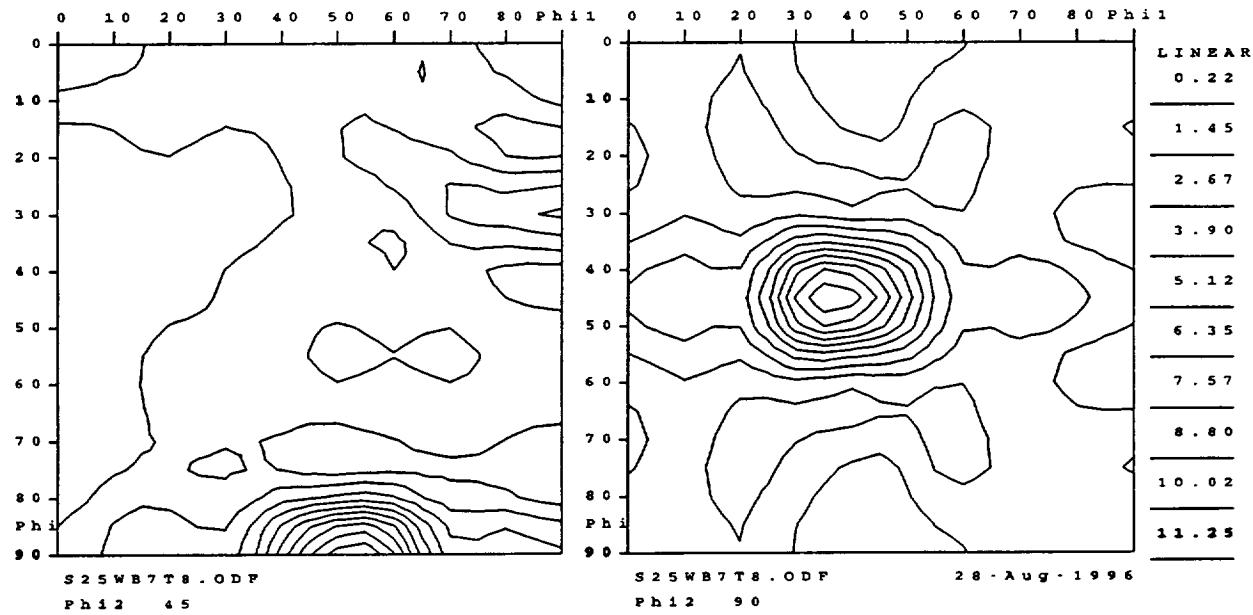


Figure 133. CODF sections for the 2195-T3 extrusion in the web @ 7t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections.
[Specimen plane perpendicular to (C)ircumferential axis]

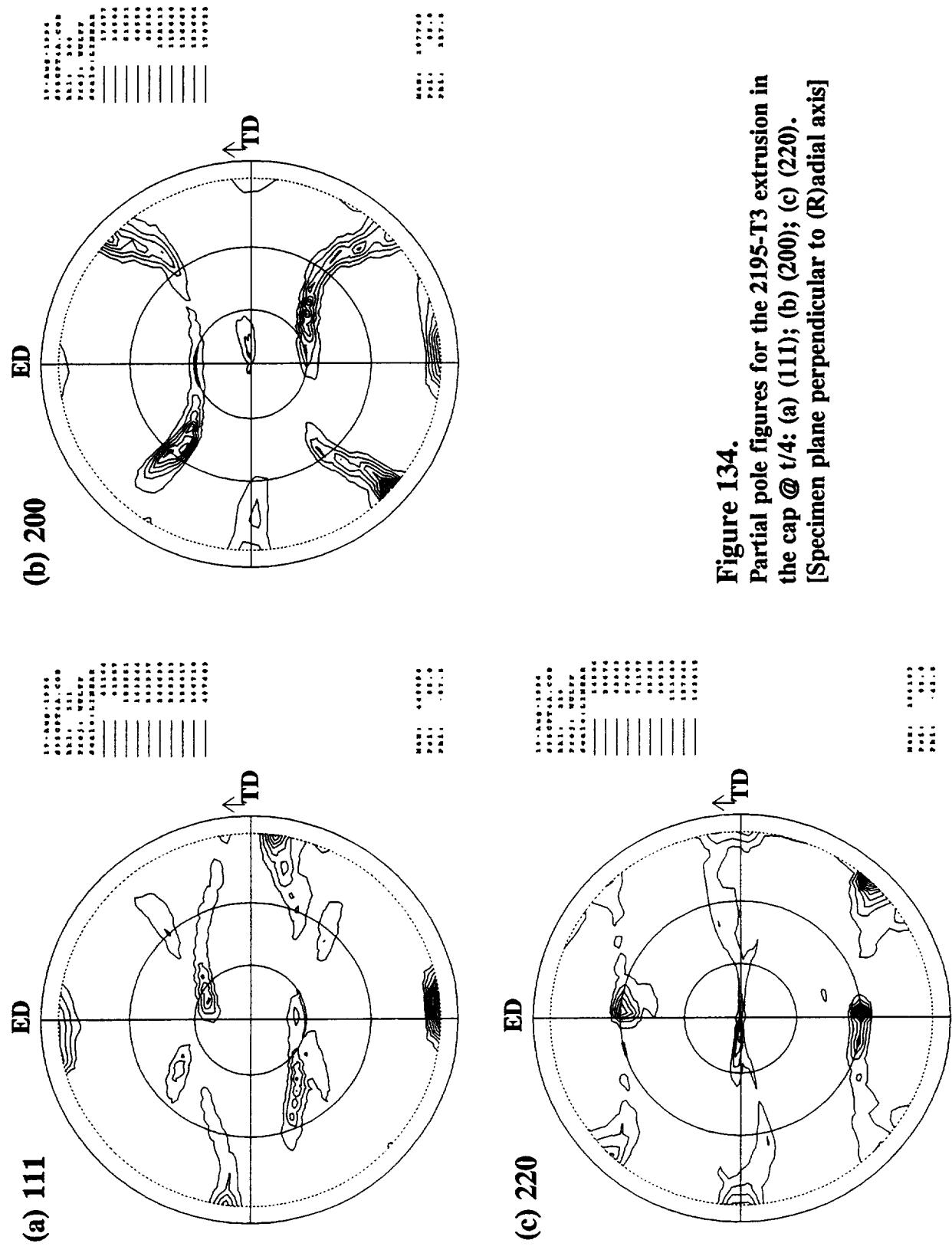
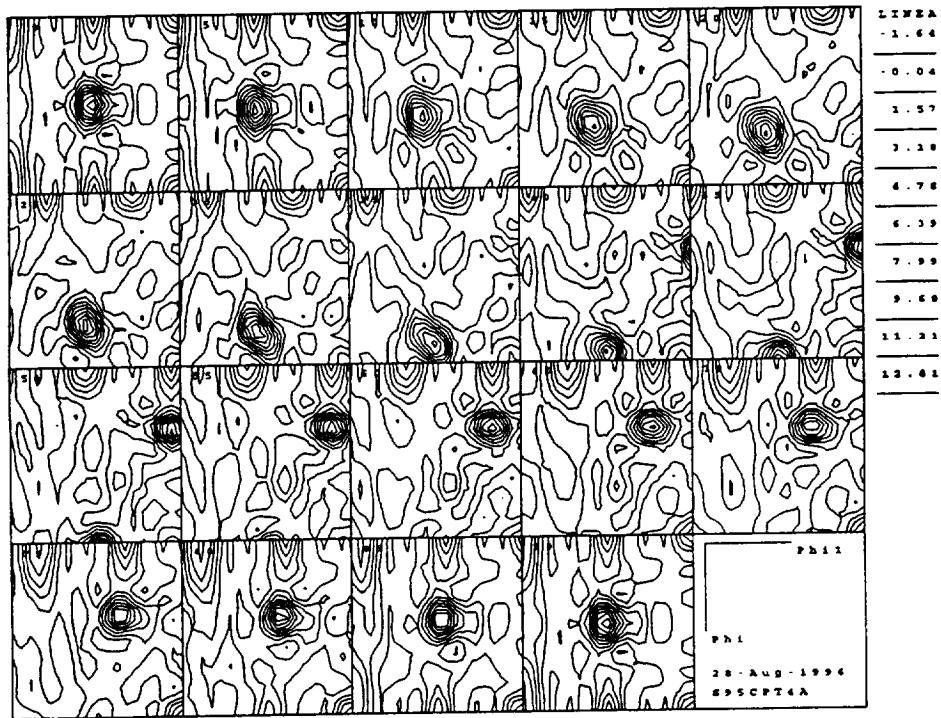


Figure 134.
Partial pole figures for the 2195-T3 extrusion in
the cap @ $t/4$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

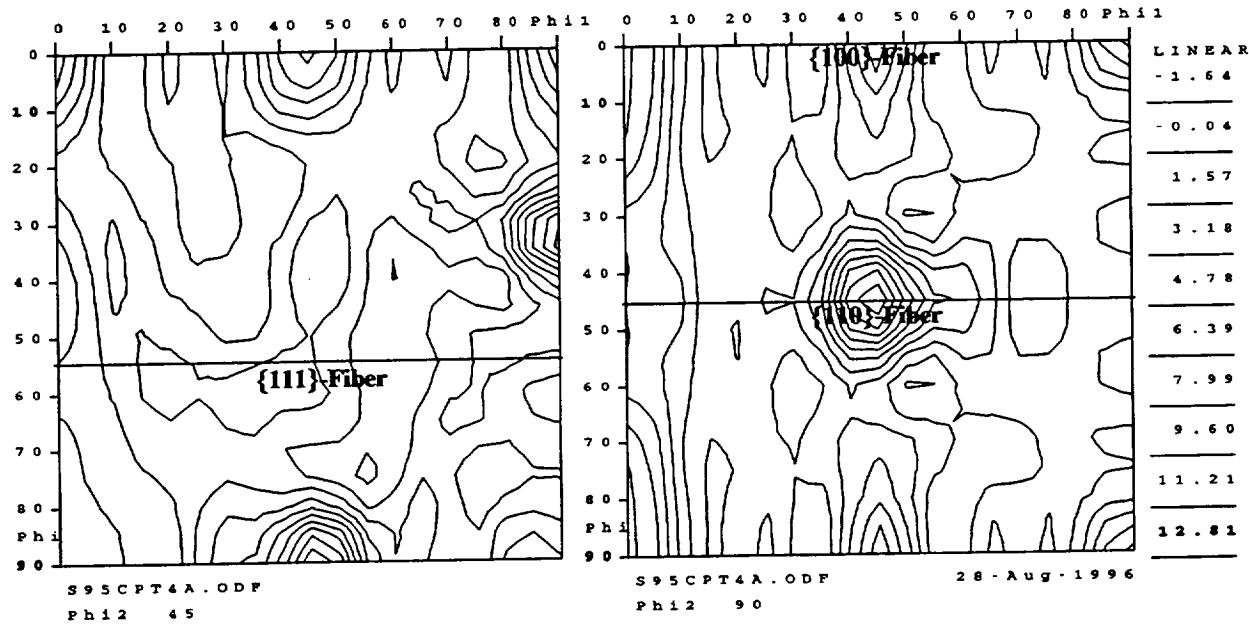


Figure 135. CODF sections for the 2195-T3 extrusion in the cap @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

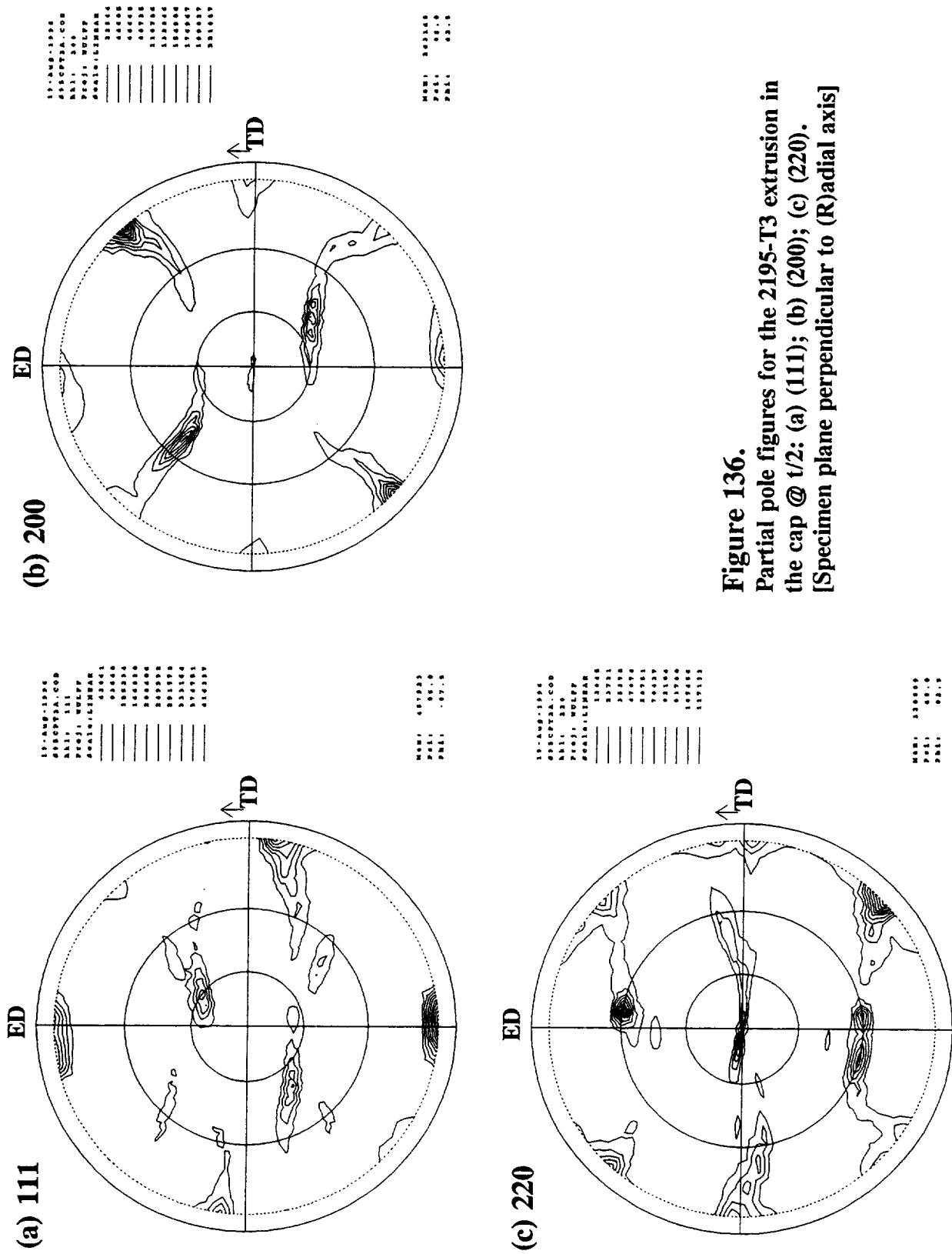
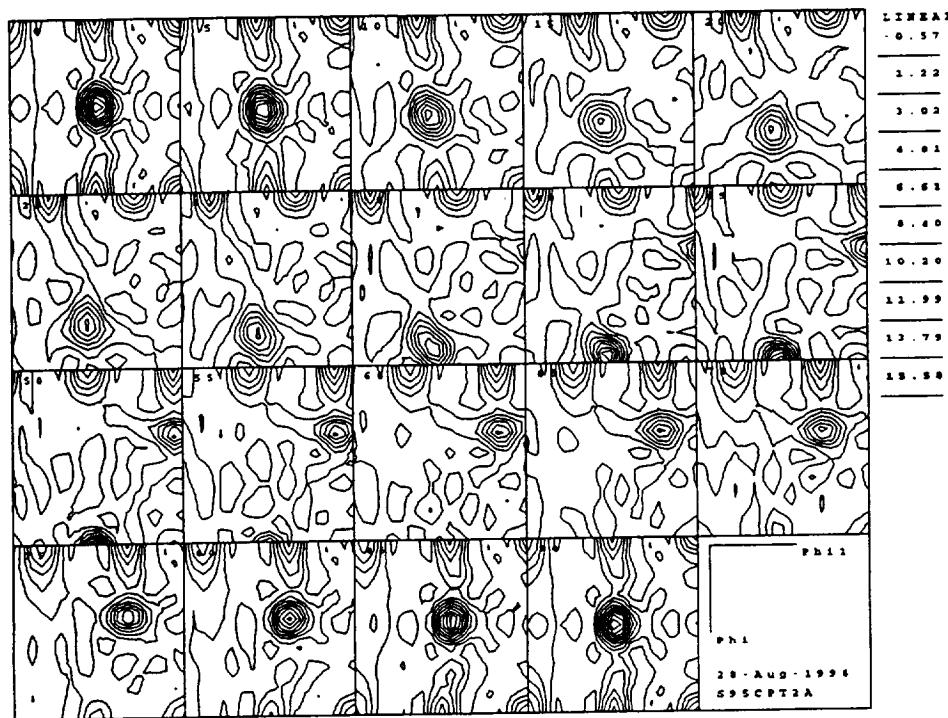


Figure 136.
Partial pole figures for the 2195-T3 extrusion in
the cap @ $t/2$: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

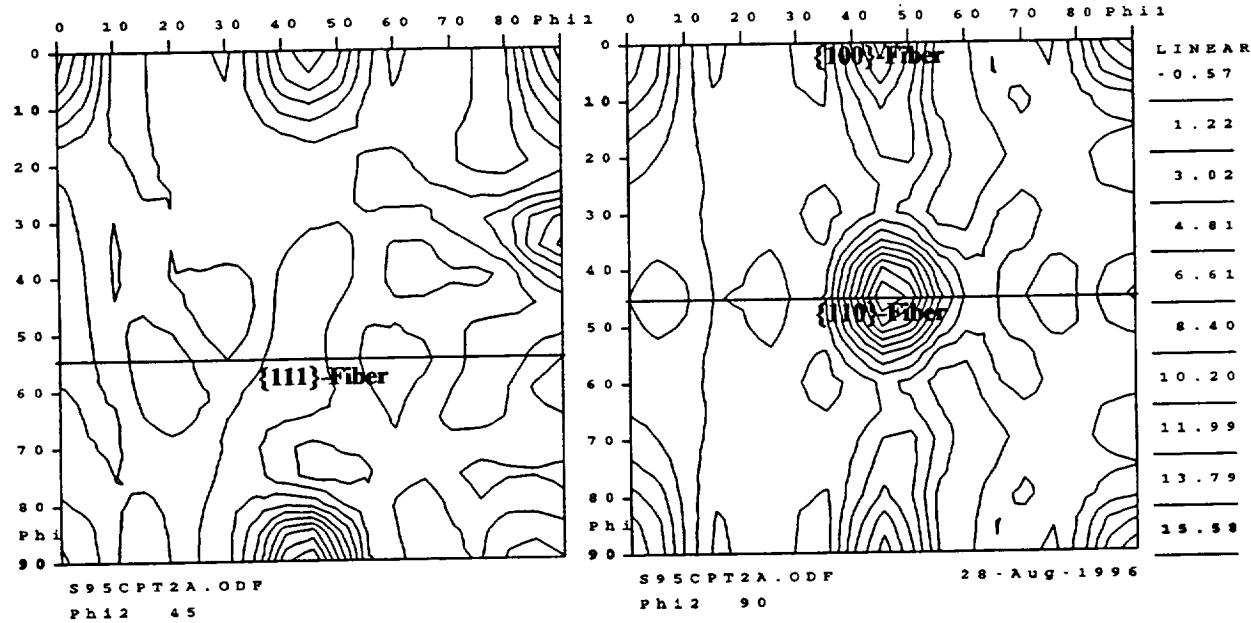


Figure 137. CODF sections for the 2195-T3 extrusion in the cap @ $t/2$; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

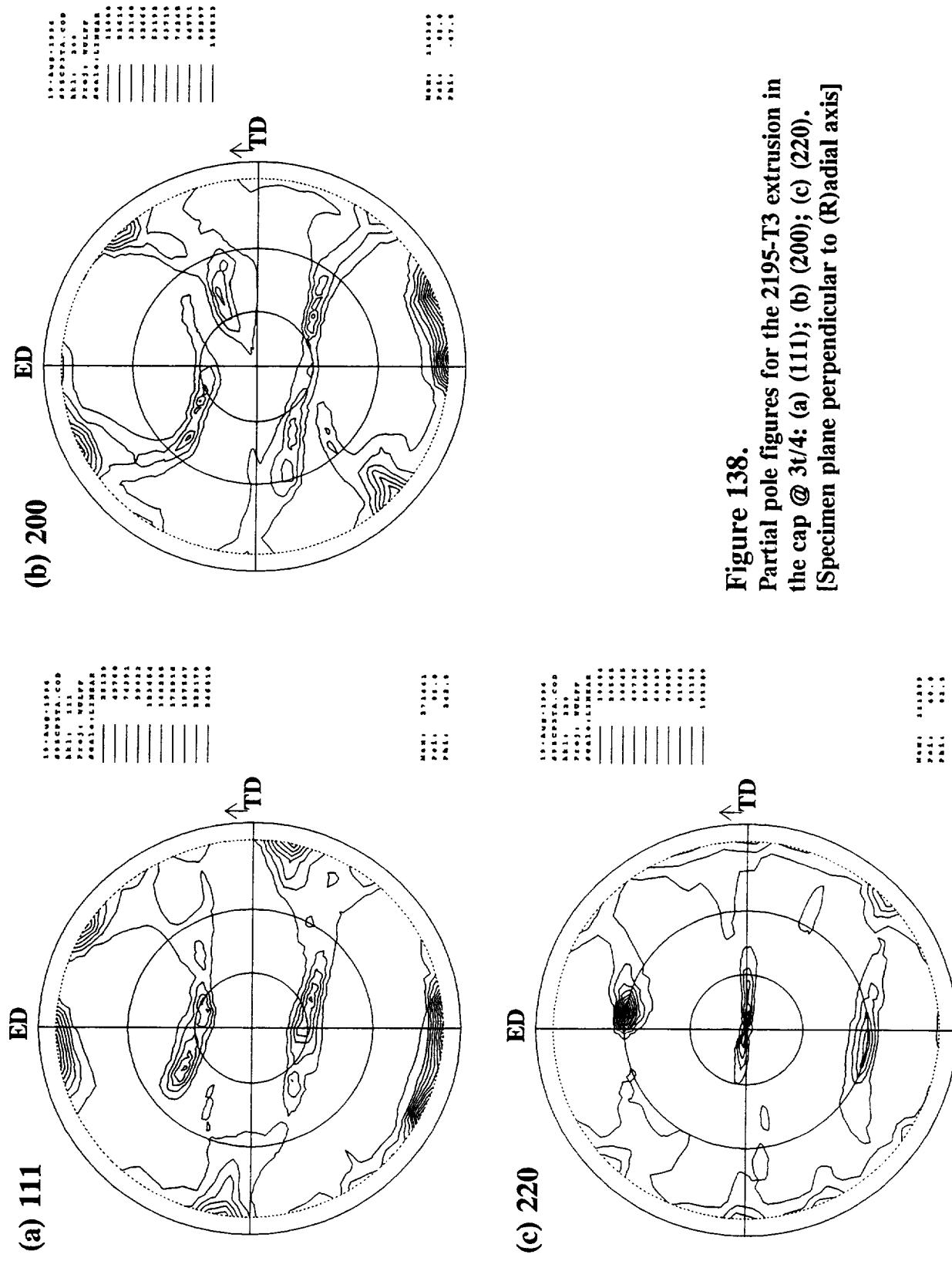
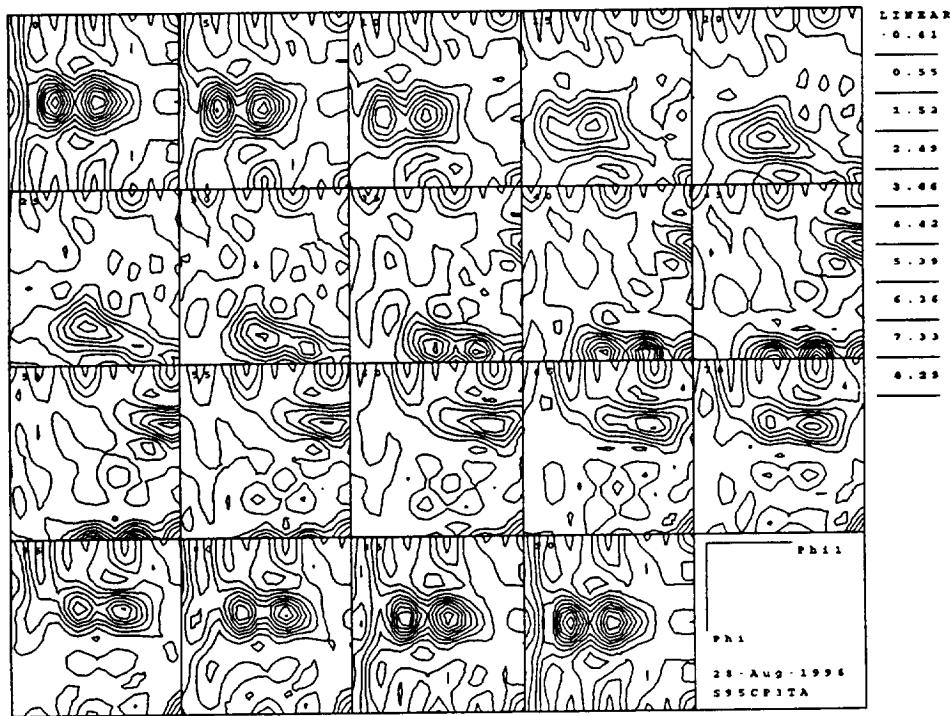


Figure 138.
Partial pole figures for the 2195-T3 extrusion in
the cap @ 3t/4: (a) (111); (b) (200); (c) (220).
[Specimen plane perpendicular to (R)adial axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

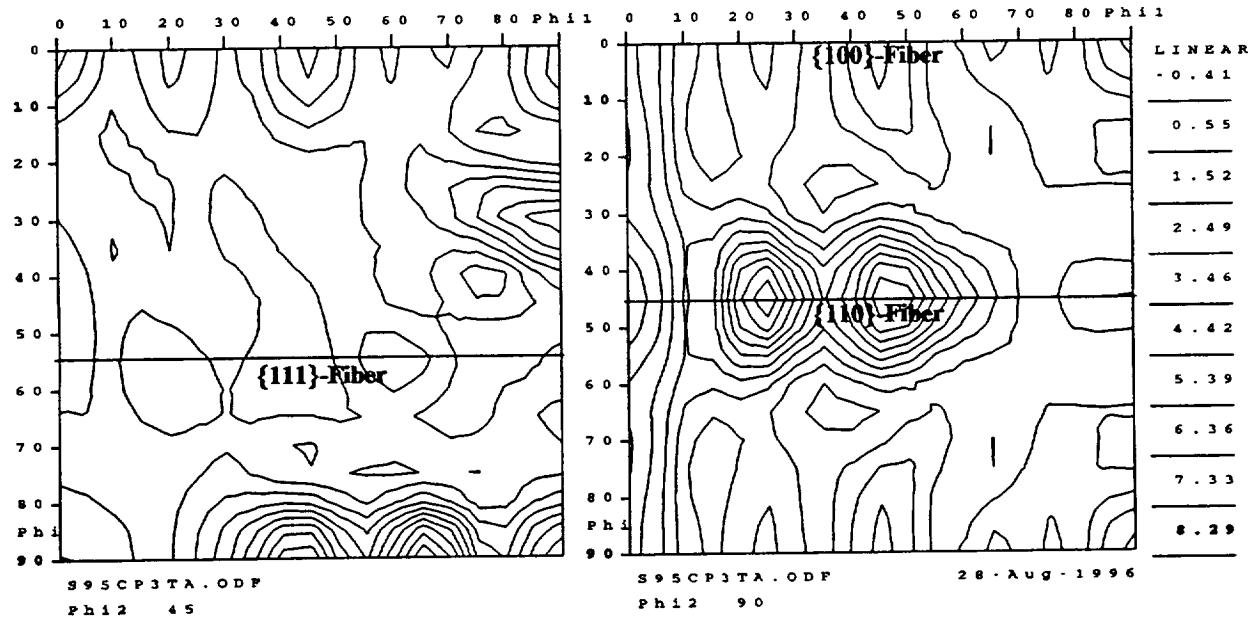


Figure 139. CODF sections for the 2195-T3 extrusion in the cap @ 3t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (R)adial axis]

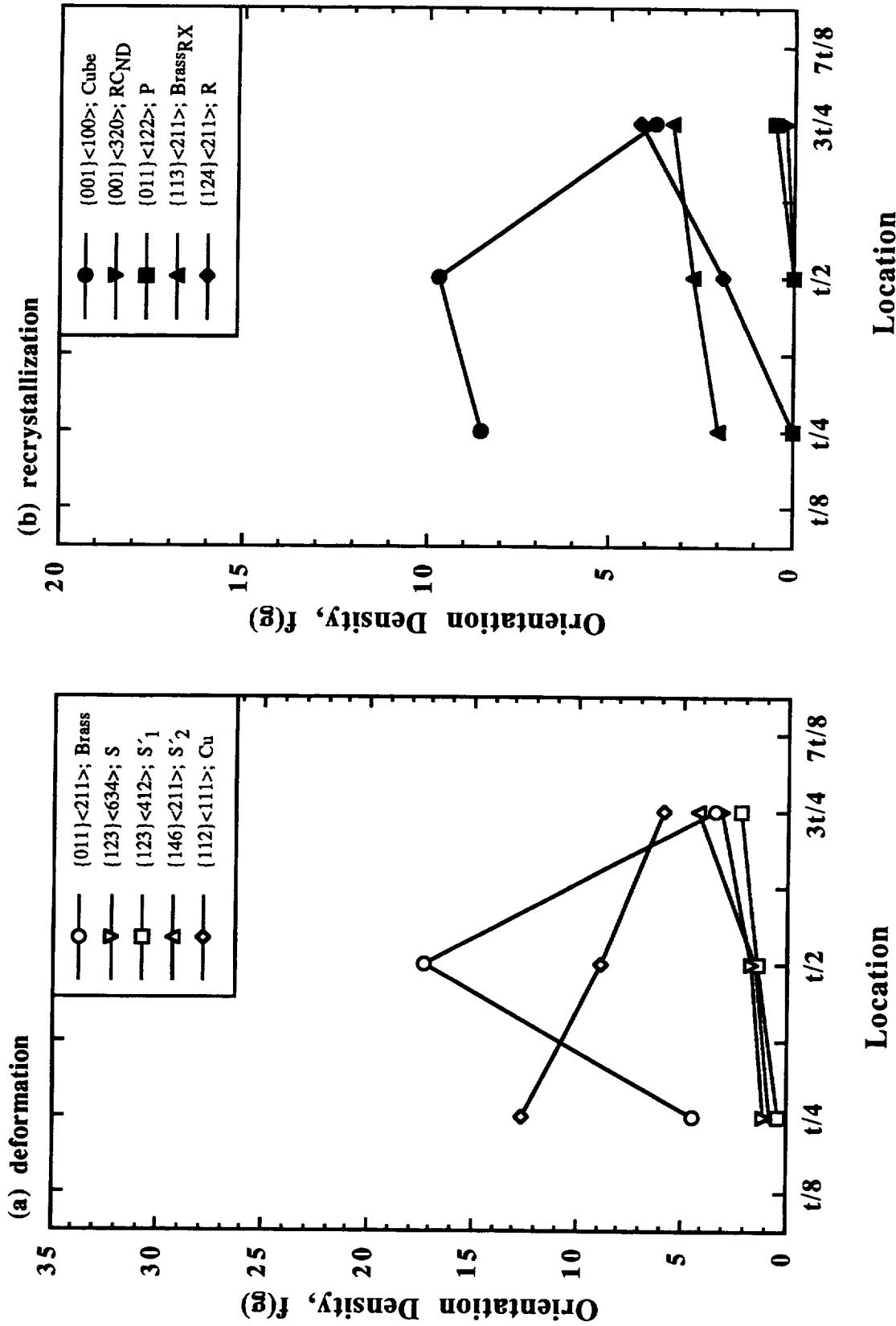


Figure 140. Orientation density, $f(g)$, as a function of location through the cross-section for the 2195-T3 extrusion in the cap region: (a) Deformation-related components; (b) Recrystallization-related components.

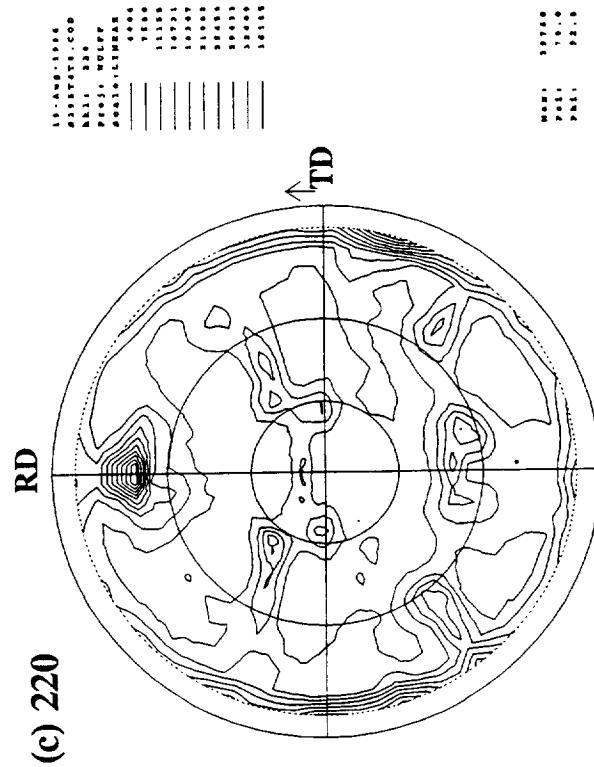
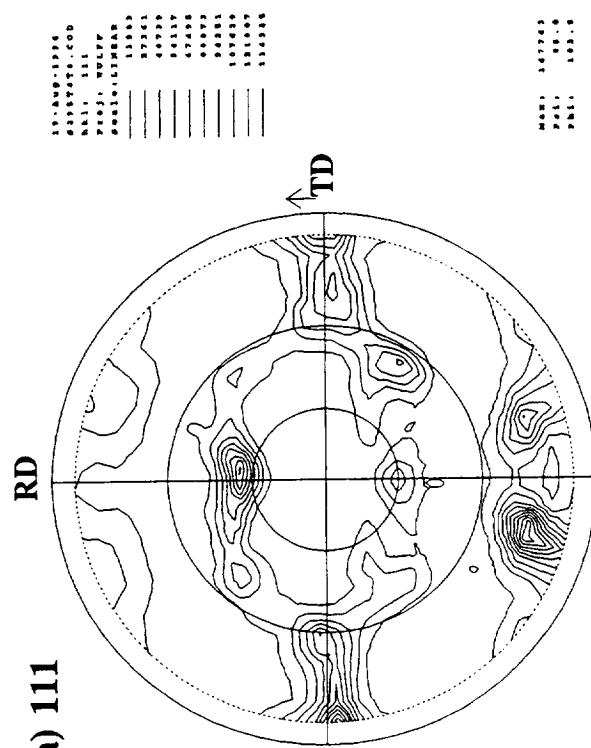
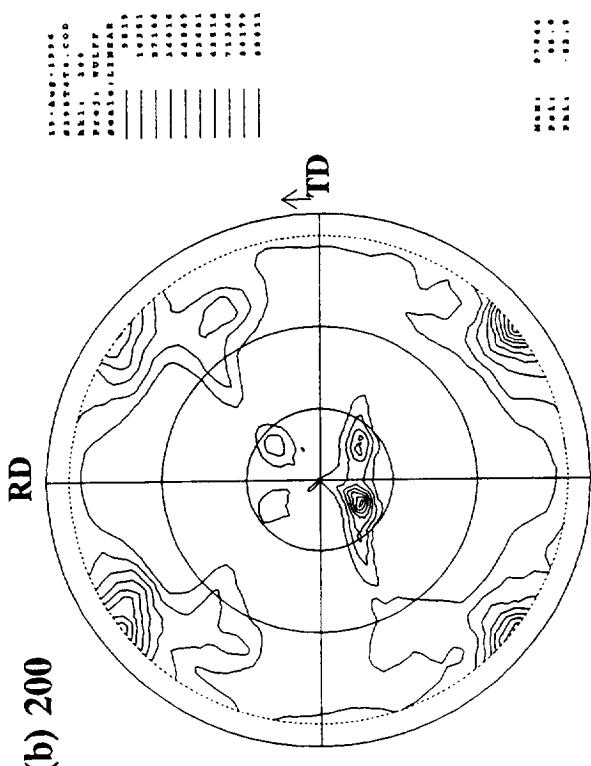
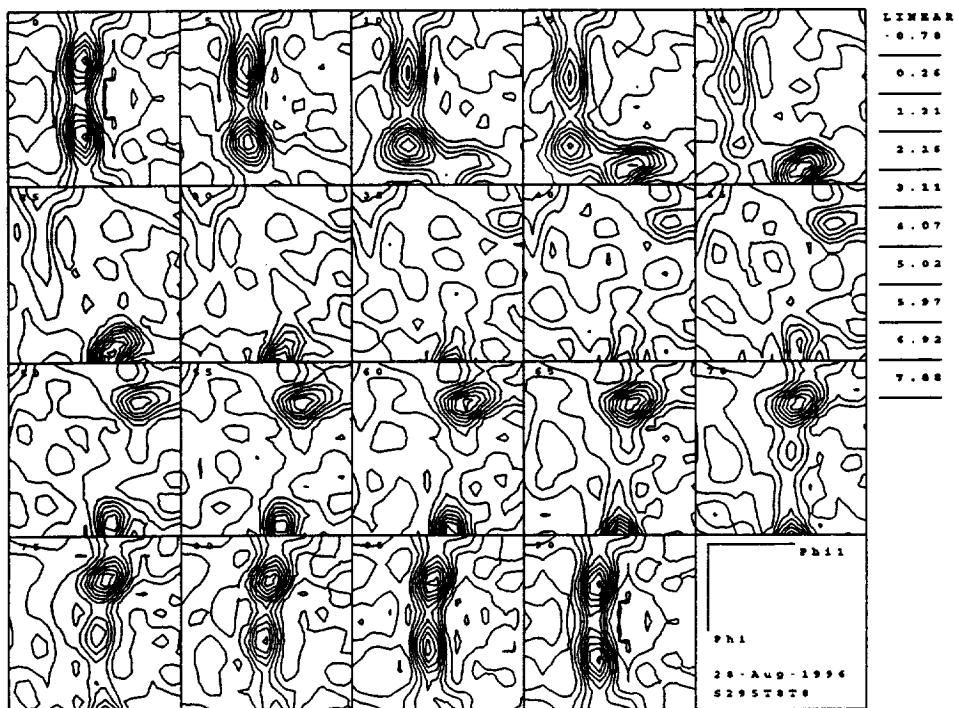


Figure 141.
Partial pole figures for 2195-T8 plate @ $t/8$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

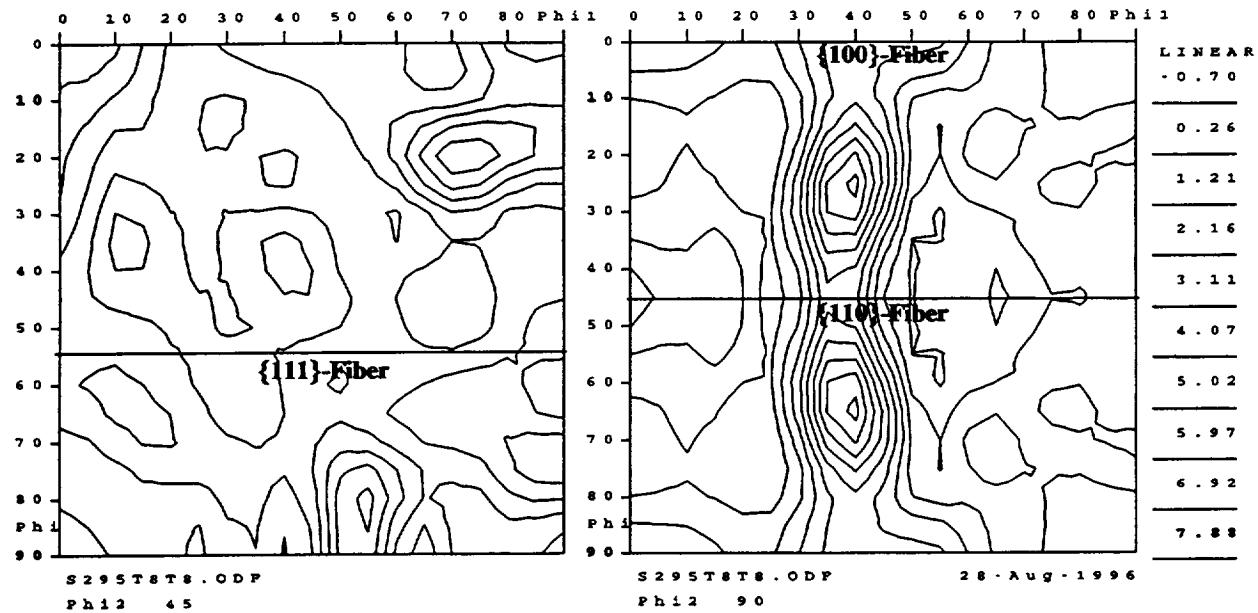


Figure 142. CODF sections for 2195-T8 plate @ t/8; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the {100}-fiber, {110}-fiber and {111}-fiber are shown.

[Specimen plane perpendicular to (S)hort-Transverse axis]

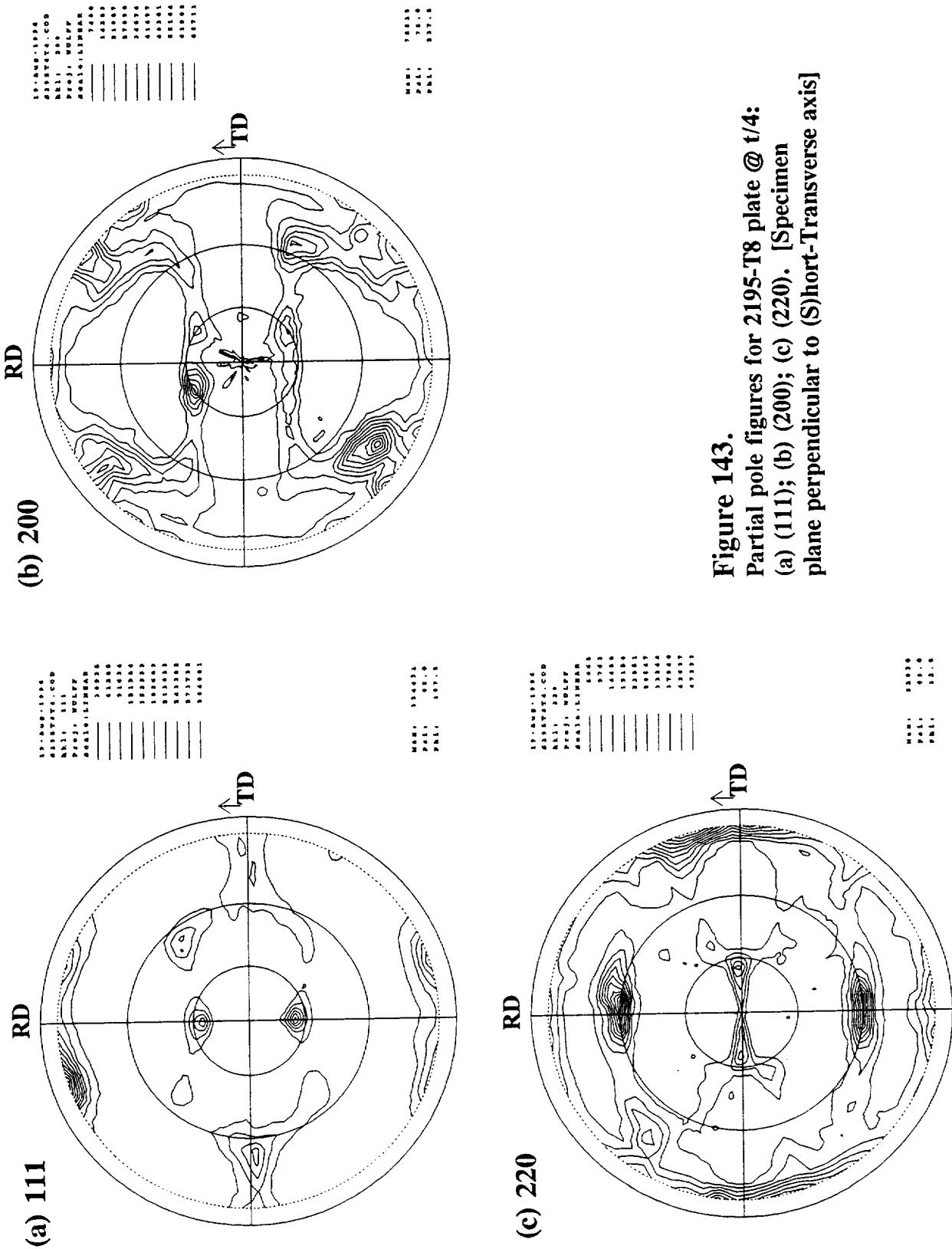
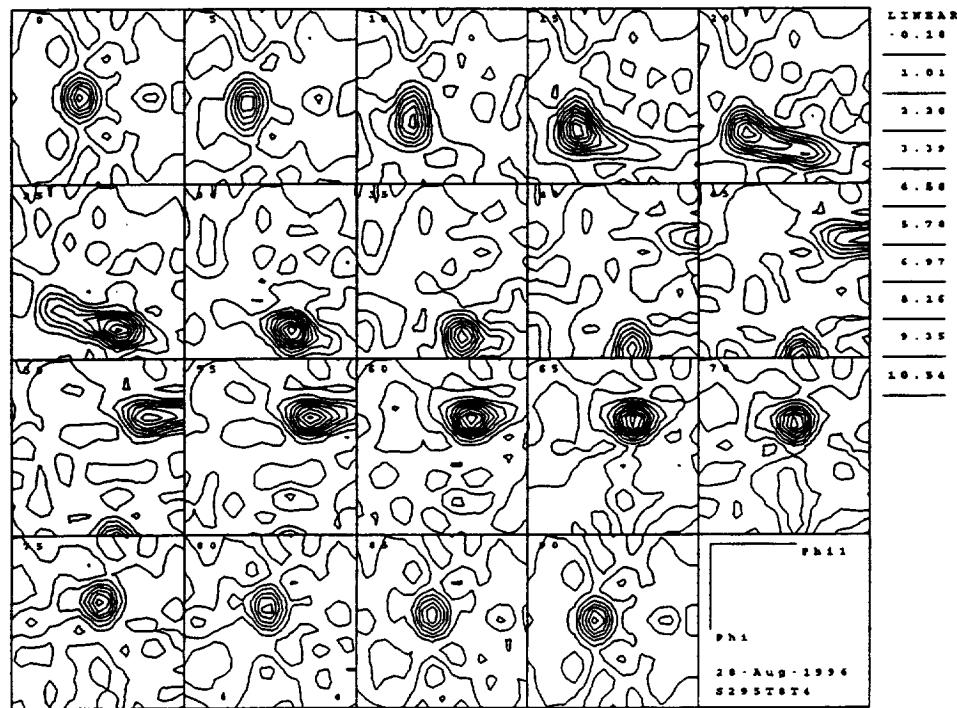


Figure 143.
Partial pole figures for 2195-T8 plate @ $t/4$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

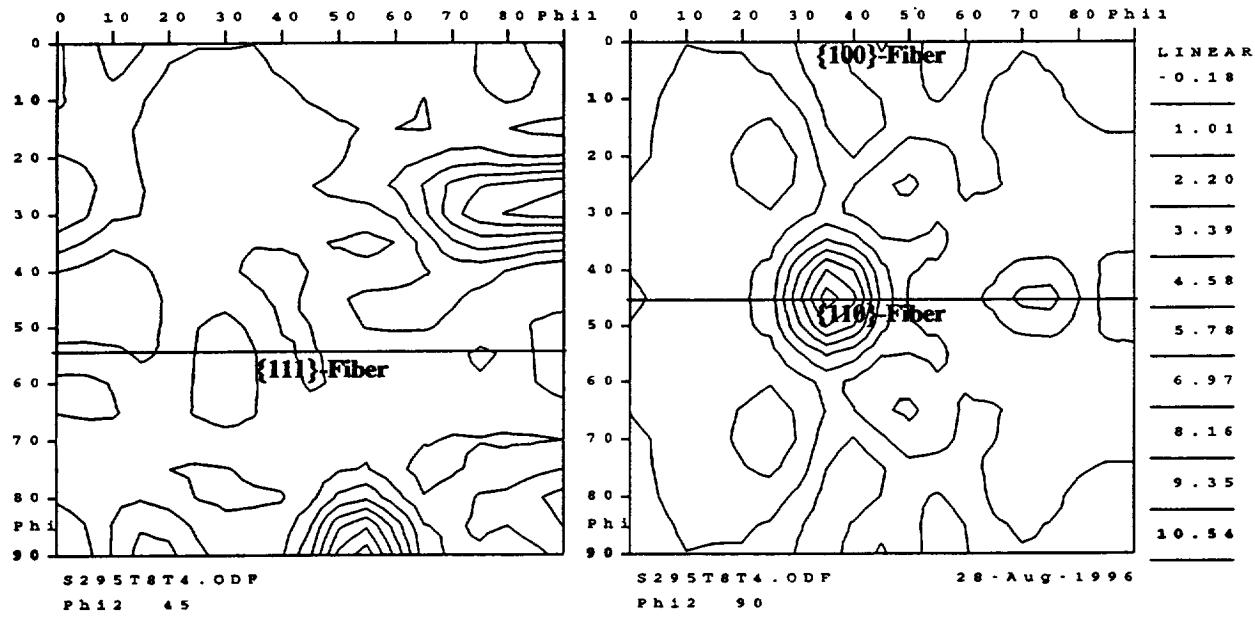


Figure 144. CODF sections for 2195-T8 plate @ t/4; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.
[Specimen plane perpendicular to (S)hort-Transverse axis]

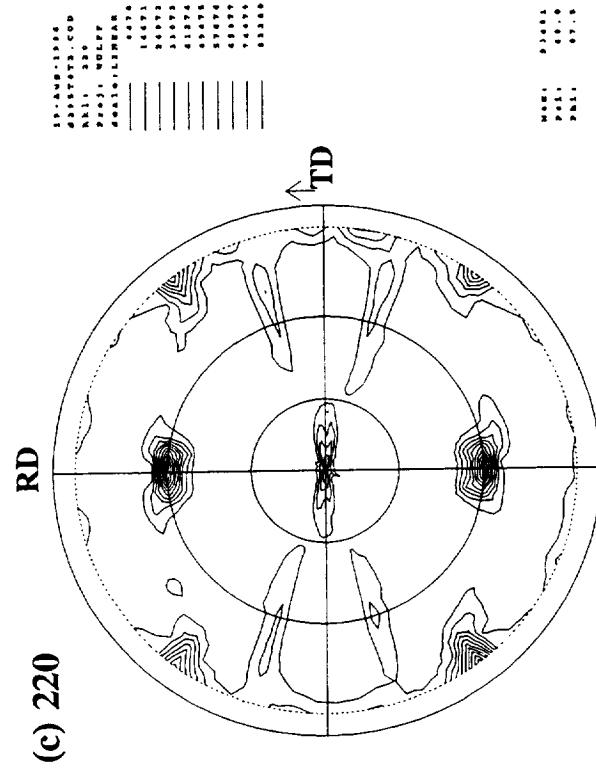
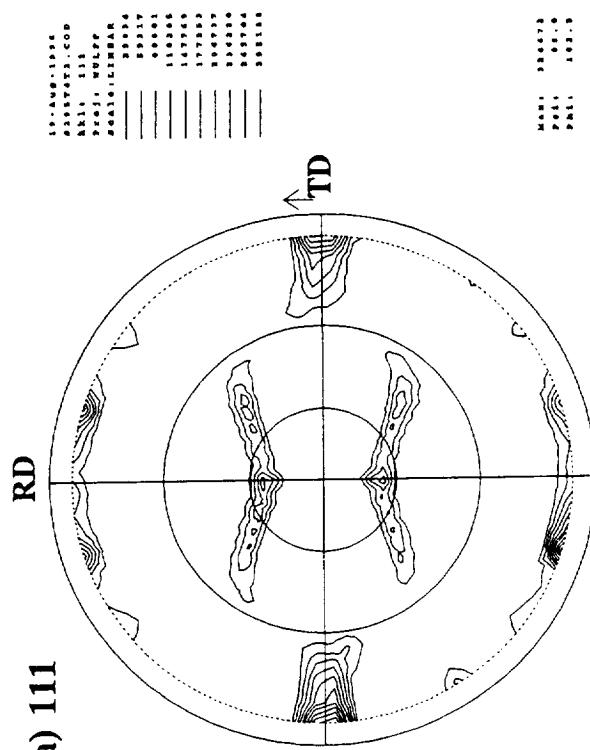
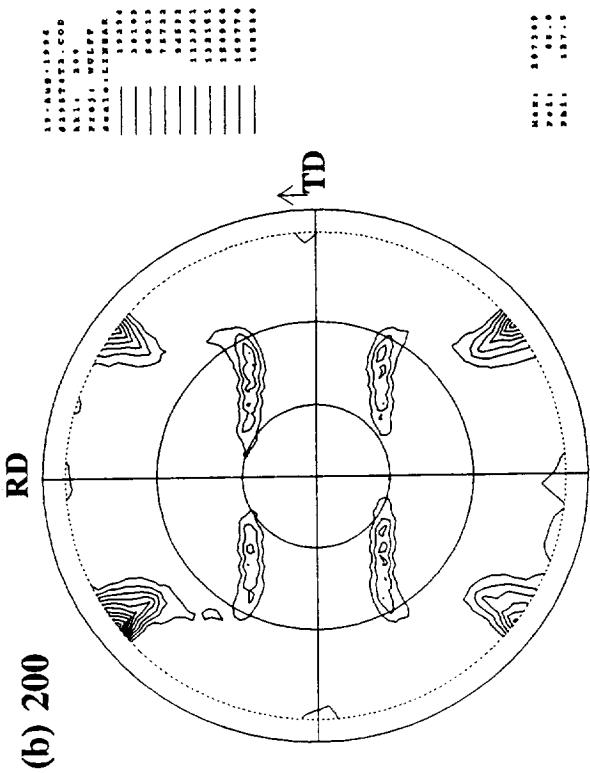
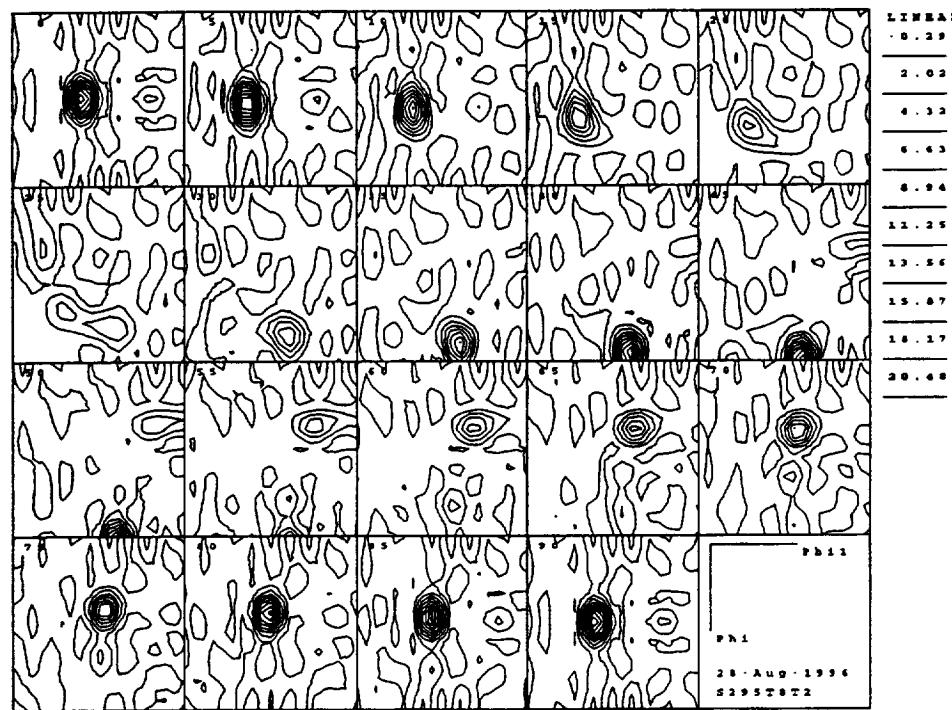


Figure 145.
Partial pole figures for 2195-T8 plate @ $t/2$:
(a) (111); (b) (200); (c) (220). [Specimen
plane perpendicular to (S)hort-Transverse axis]

(a) Sections: $\varphi_2 = 0 - 90^\circ$



(b) Sections: $\varphi_2 = 45^\circ; \varphi_2 = 90^\circ$

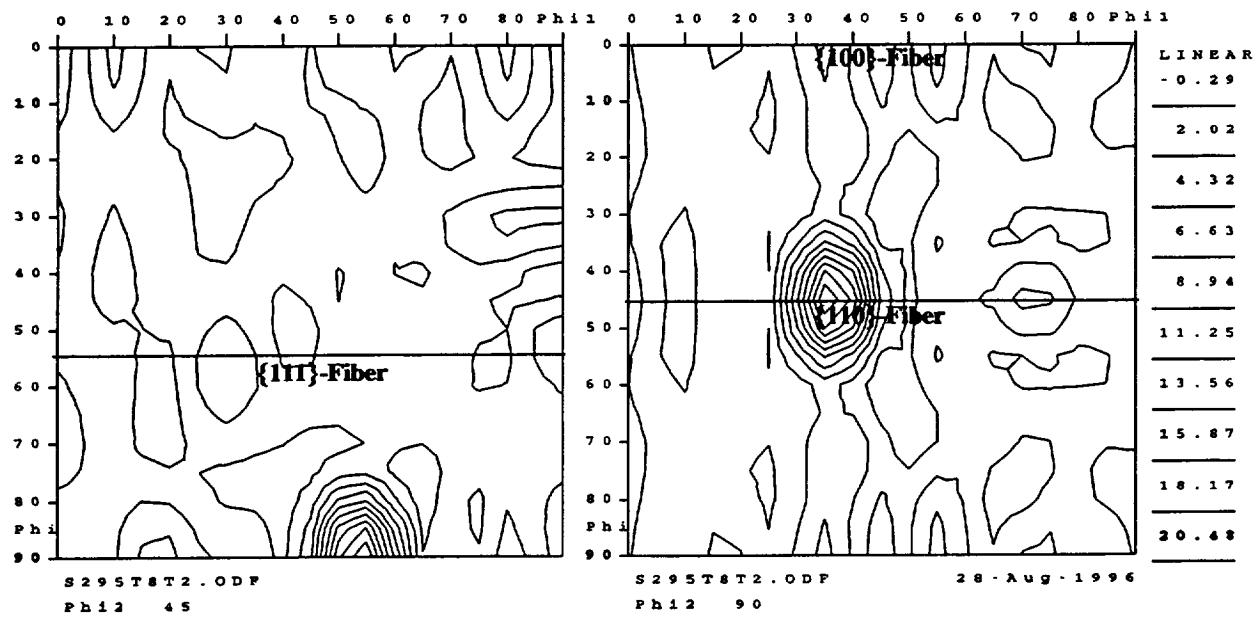


Figure 146. CODF sections for 2195-T8 plate @ t/2; (a), Complete sections: $\varphi_2 = 0, 5, 10 \dots 90^\circ$; and (b), enlarged $\varphi_2 = 45^\circ$ and $\varphi_2 = 90^\circ$ sections. The locations of the $\{100\}$ -fiber, $\{110\}$ -fiber and $\{111\}$ -fiber are shown.

[Specimen plane perpendicular to (S)hort-Transverse axis]

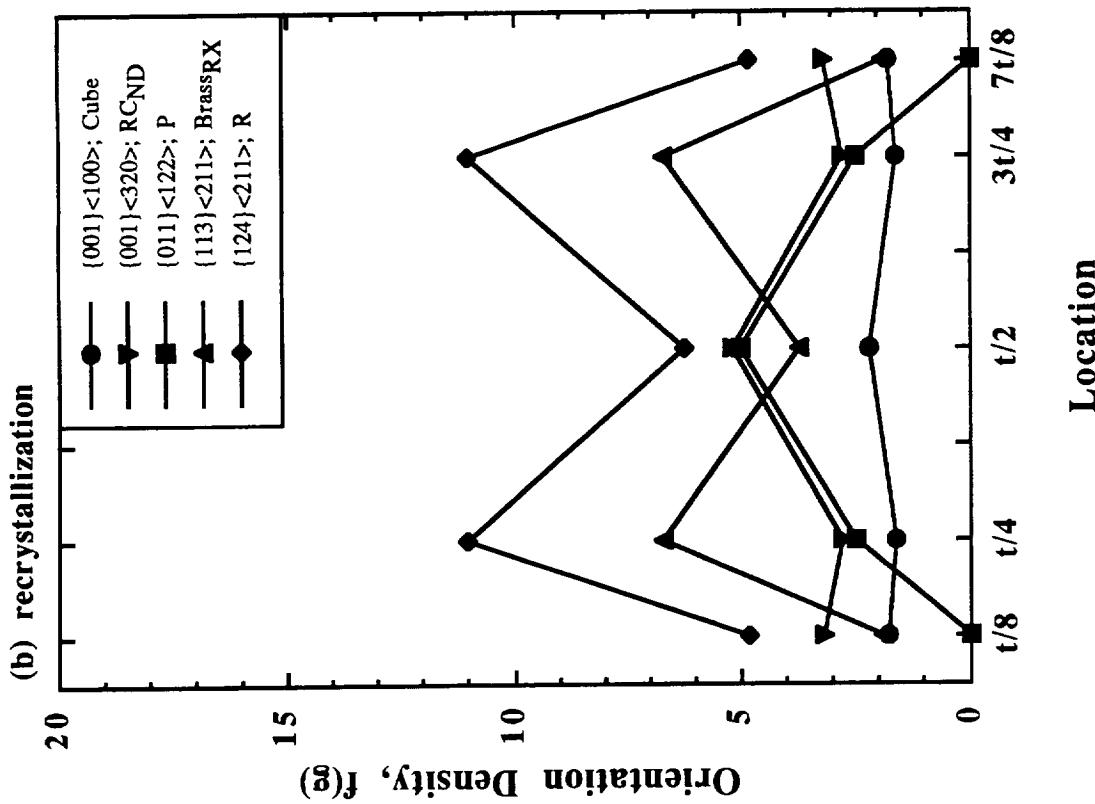
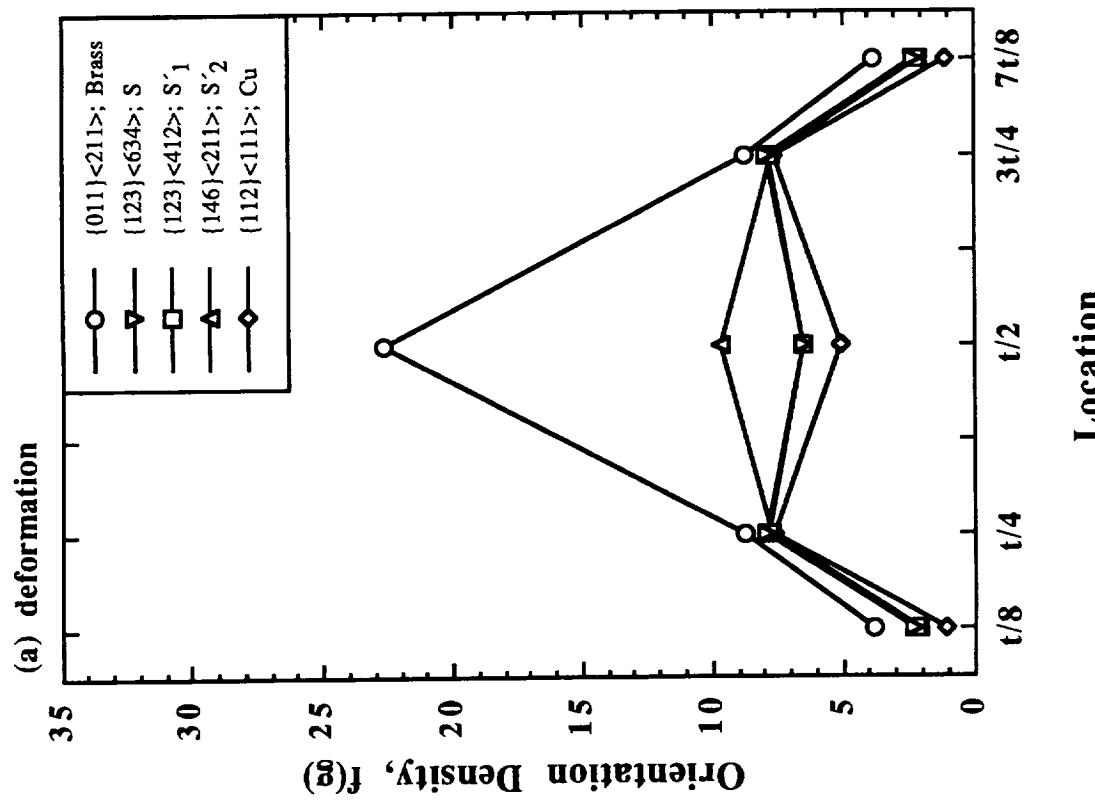


Figure 147. Orientation density, $f(g)$, as a function of location through the cross-section for the 2195-T8 plate:
(a) Deformation-related components; (b) Recrystallization-related components.

REPORT DOCUMENTATION PAGE

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13. ABSTRACT (Maximum 200 words) The effect of crystallographic texture on the mechanical properties of near-net-shape extrusions is of major interest if these products are to find application in launch vehicle or aircraft structures. The objective of this research was to produce a catalogue containing quantitative texture information for extruded product, sheet and plate. The material characterized was extracted from wide, integrally stiffened panels fabricated from the Al-Cu-Li alloys 1460, 2090, 2096 and 2195. The textural characteristics of sheet and plate products of the same alloys were determined for comparison purposes. The approach involved using X-ray diffraction to generate pole figures in combination with orientation distribution function analysis. The data were compiled as a function of location in the extruded cross-sections and the variation in the major deformation- and recrystallization-related texture components was identified.						
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